

Enabling Near-Field Communications: Beam Shaping, Optimization, and Channel/Data Estimation

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The University of Electro-Communications

- ❑ Founded in 1918 as the Technical Institute for Wireless Communications.
- ❑ Became national university in 1949.
- ❑ The only national university in Japan without a place name.
- ❑ 304 faculty members, 136 staffs, 3371 undergrads, and 1,430 graduates.
- ❑ Notable faculty members
 - Te Sun Han & Kingo Kobayashi
 - Kunihiko Fukushima
- ❑ Notable alumni
 - Ken Kutaragi (Father of PlayStation)



国立大学法人
電気通信大学
The University of Electro-Communications



Introduction of Our Research Center

☐ Advanced Wireless & Communications Research Center (AWCC)

- Japan's only national university research center specializing in wireless communications
- 3 dedicated professors, 6 concurrent professors
- Leading many national research projects



☐ Consortium for Wireless Innovation and Research EXchange

- Founded in 2023
- A platform for "industry-academia collaboration"
- To build up a strong network of researchers in Japan
- 8 Sponsors, 68 Members from 14 Organizations



Main Contributors of This Talk



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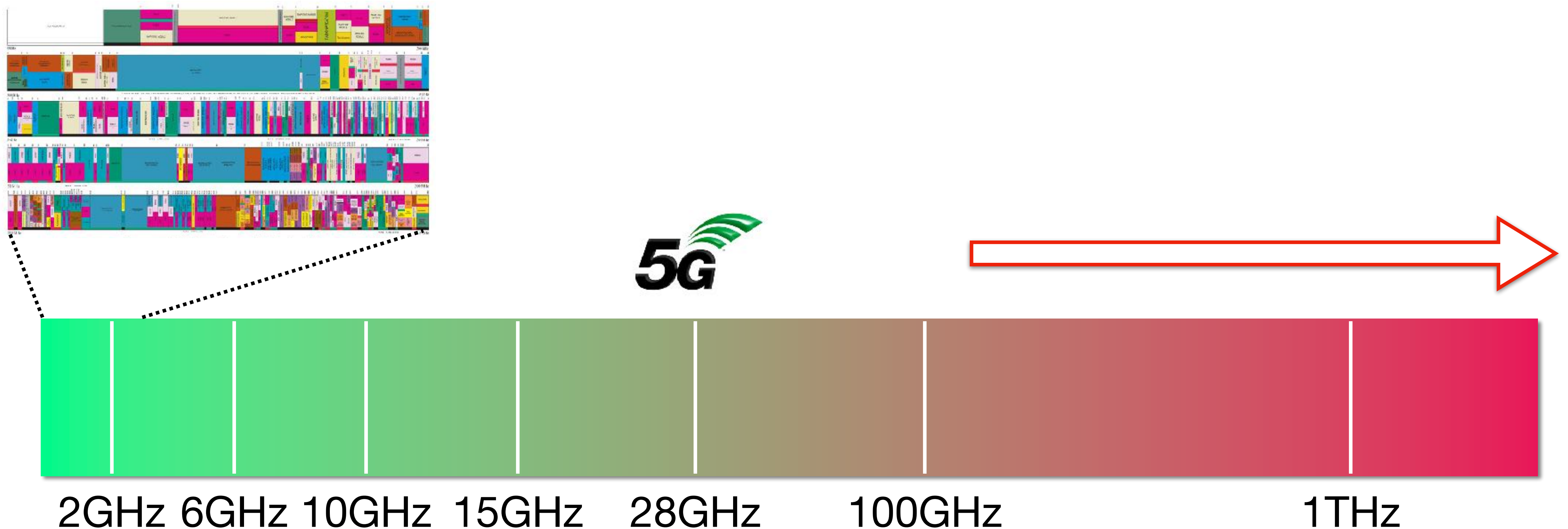


Szabolcs Malomsoky, Ph.D.
(Ericsson Research Japan)

Need for Higher-Frequency Bands

□ Leveraging higher-frequency bands is essential to further increase data rates.

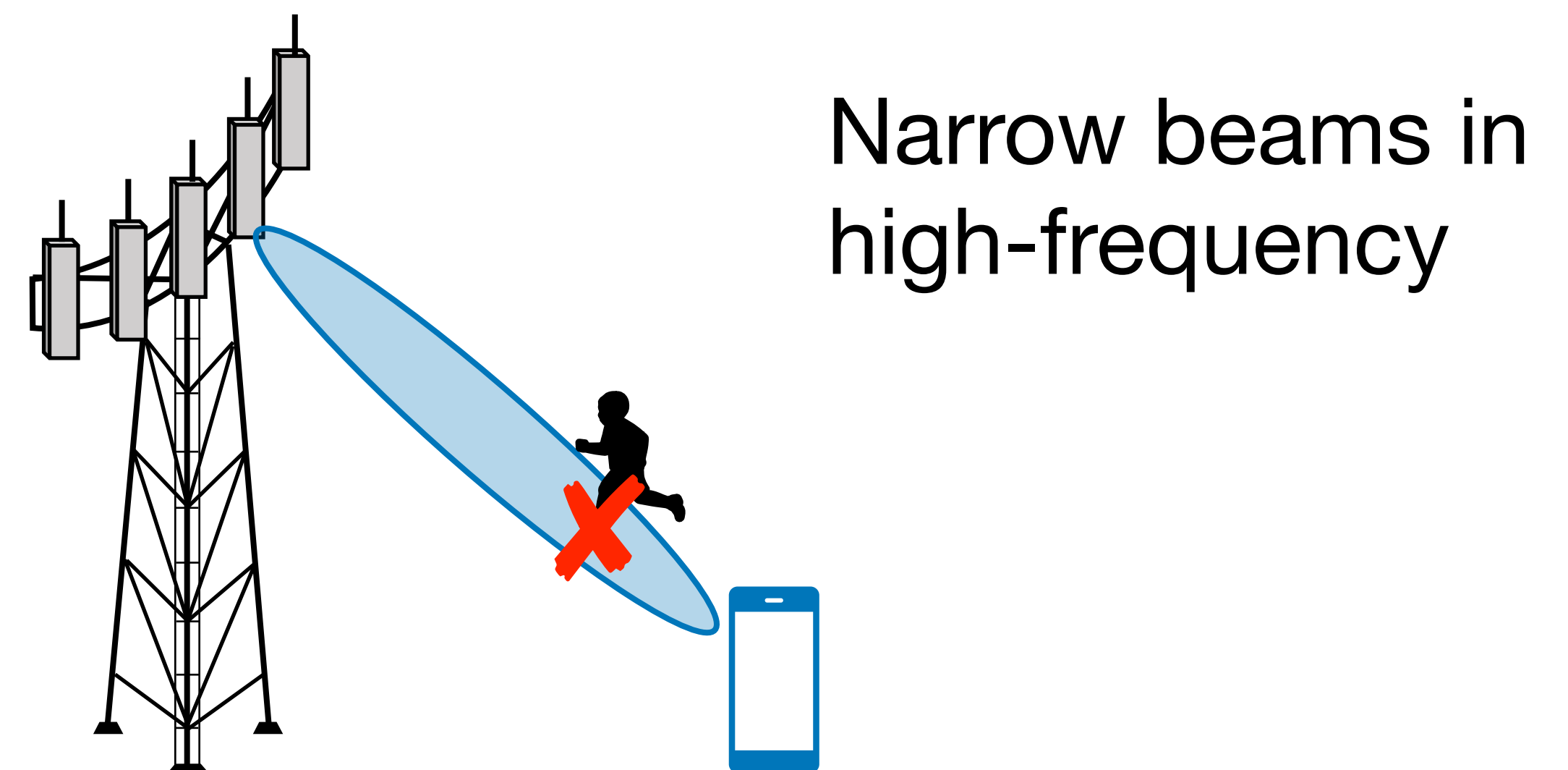
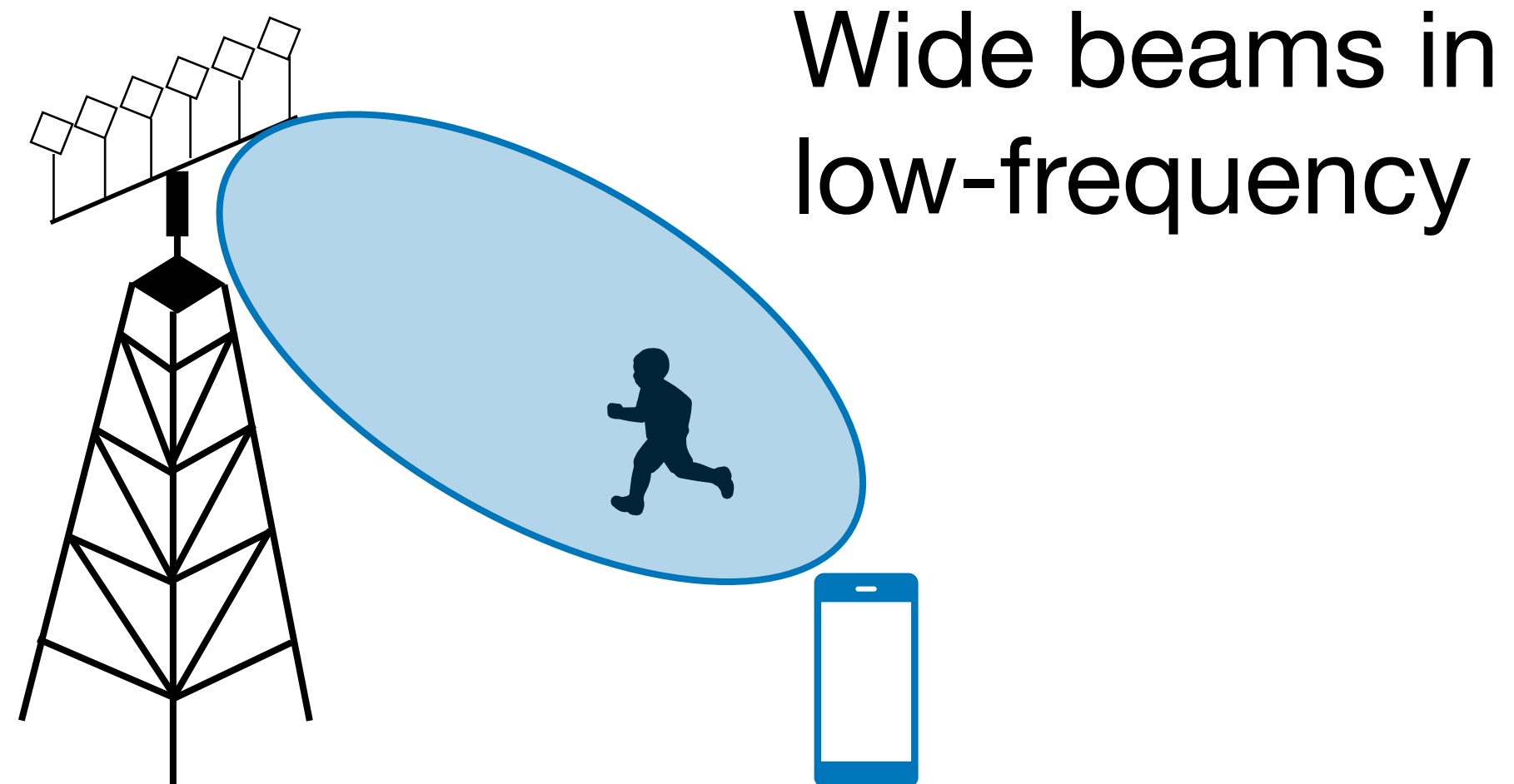
● **High directivity** is needed to compensate for severe path loss.



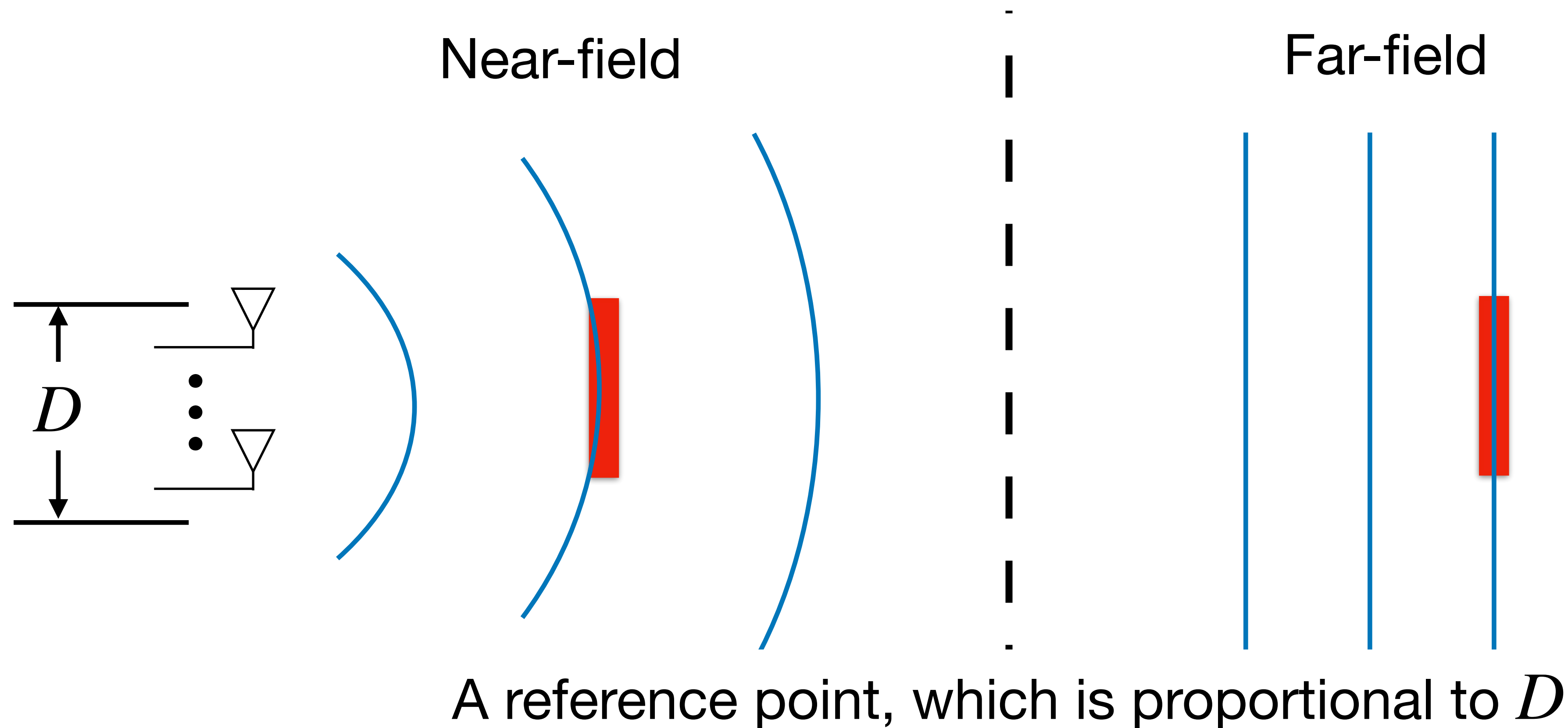
Channel Instability in High Frequency Bands

- High directivity → narrow beams
- High photon energy → strong reflection and/or absorption by materials
- Short wavelengths → significant diffraction even from small objects

Severe blockage losses by common objectives

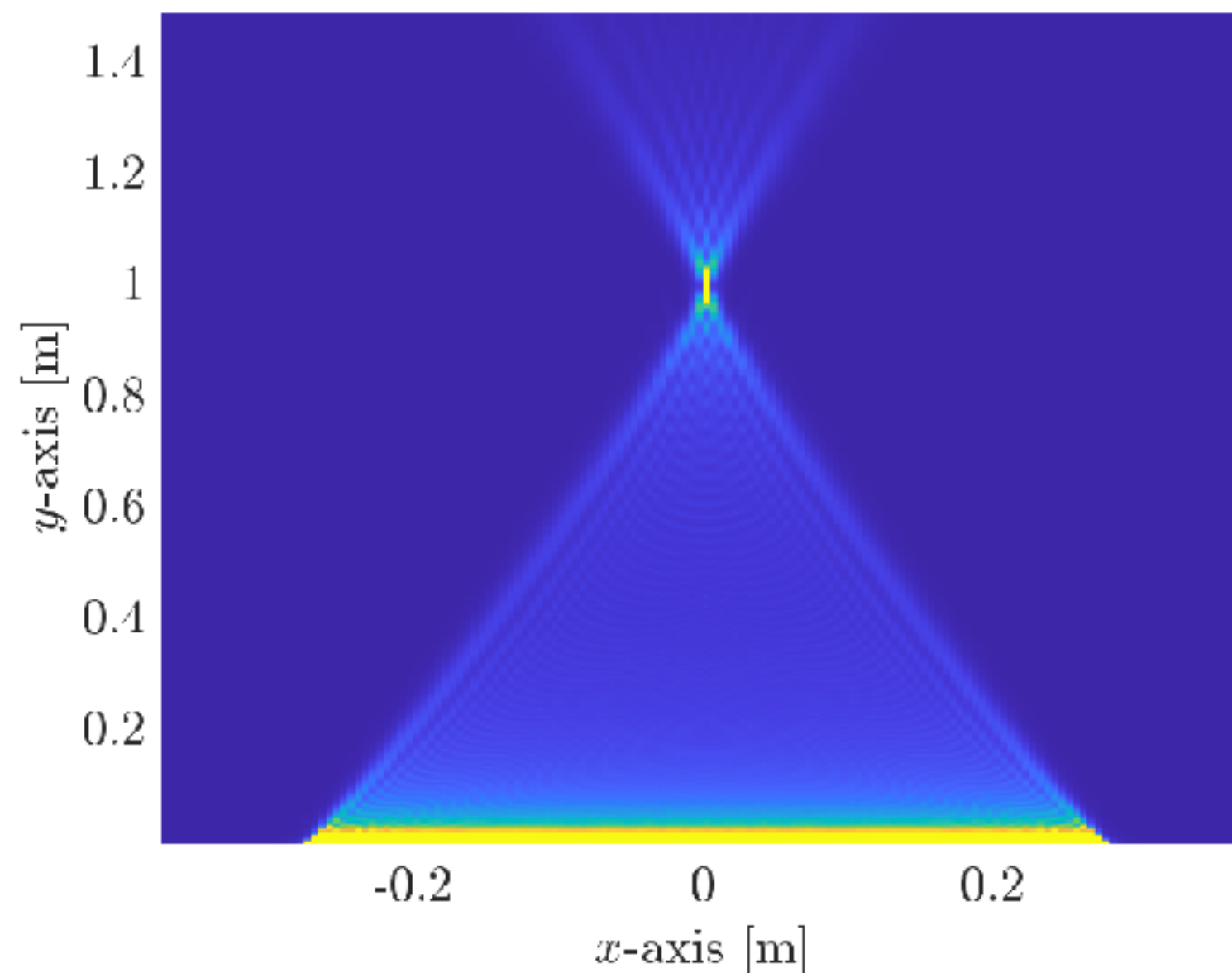


- **A large antenna aperture** for high directivity makes the signal's spherical wavefront non-negligible.
- This near-field effect must be considered in beam design.

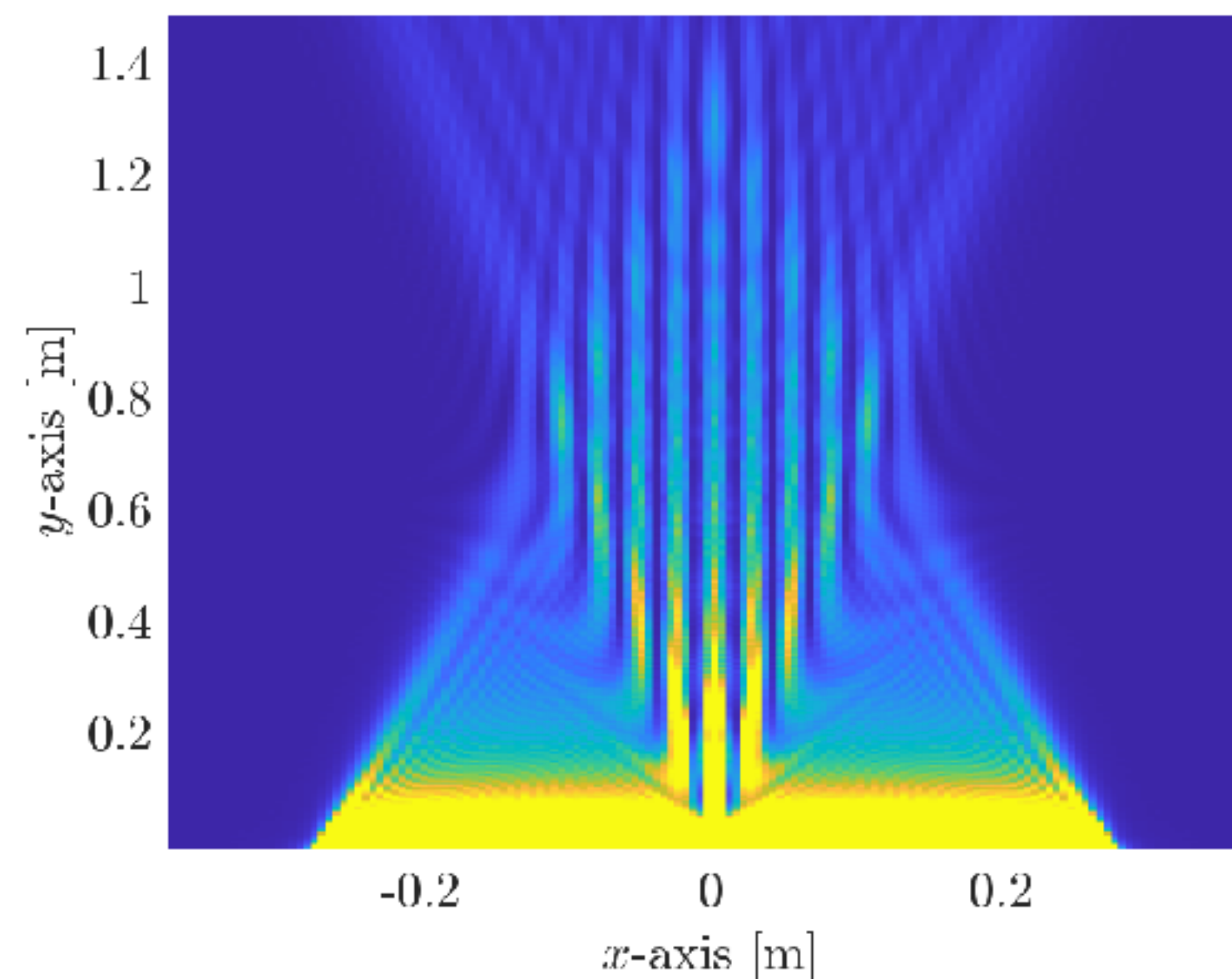


- Beam optimizations for the environment requires full CSI
 - Challenge: high-dimensional, near-field channels make CSI estimation hard
 - Any nice beam solely using *partial side information*?

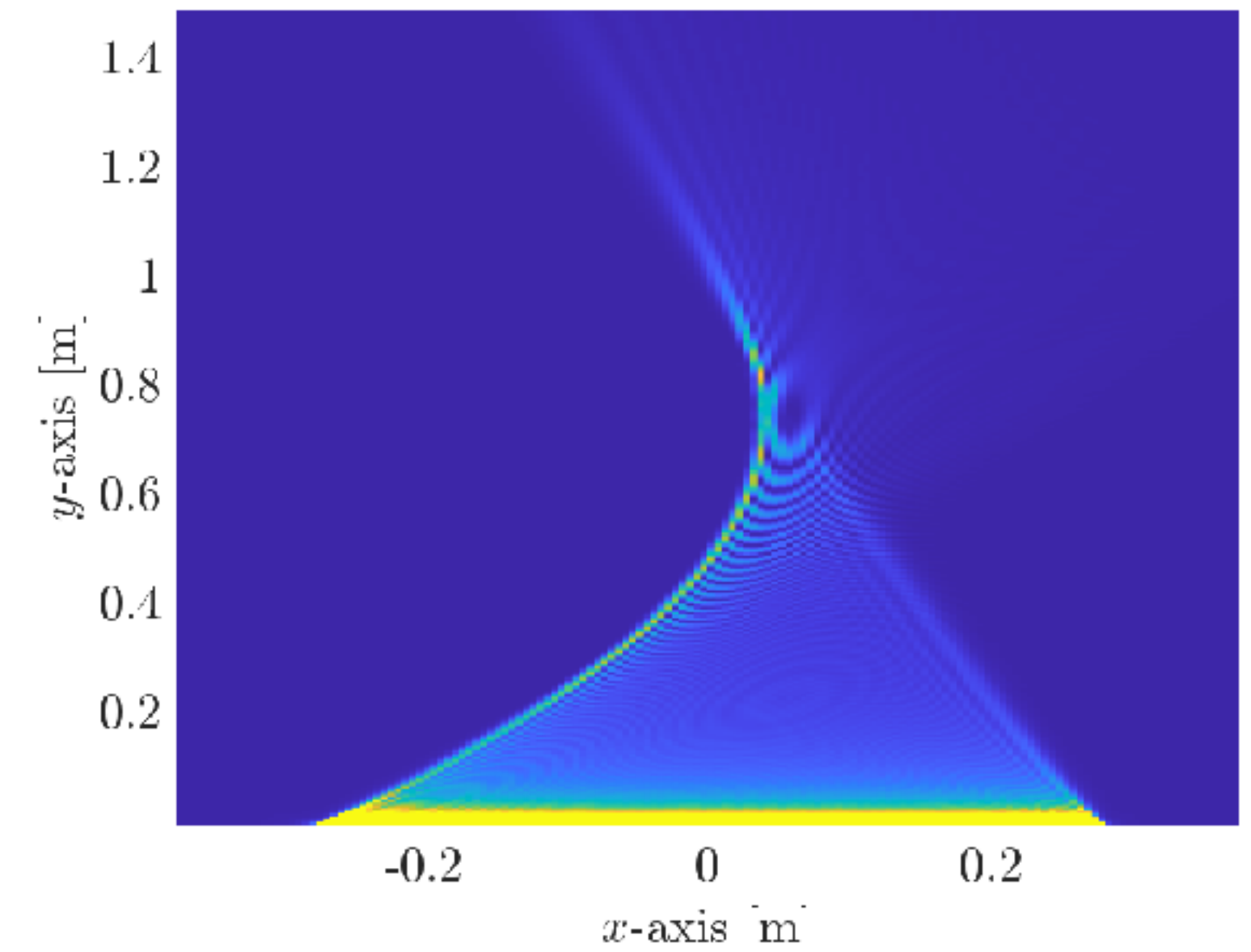
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 - Any nice beam solely using *partial side information*?



*Beam focusing
with UE's position*



*Bessel beam
with UE's angle*



*Curving beam
with UE's and blocker's positions*

- No beam is universally optimal [TWC'24]
 - Necessity of wavefront hopping via phased array
- Bessel beam steering [Bal'24]
 - Toward the desired azimuth and elevation
 - lacks a closed-form expression of phase distribution
- Curving beam steering [TWC'25]
 - Analyses on propagation and beam design for a known user position
 - No trajectory optimization to avoid obstacles

[TWC'24] V. Petrov et al., "Wavefront hopping: An enabler for reliable and secure near field terahertz communications in 6G and beyond," IEEE Wireless Commun., vol. 31, no. 1, pp. 48–55, Feb. 2024.

[Bal'24] A. Simoncic, and et al., "Near-field beam steering with planar antenna array," in Proc. 7th Int. BalkanCom, Jun. 2024, pp. 31–36

[TWC'25] S. Droulias, and et al., "Bending beams for 6G near-field communications," IEEE TWC., vol.24, no.2, pp. 1467--1480, Feb. 2025.

□ First part:

- Near-field beam generation using uniform linear array (ULA)
- Closed-form phase distributions of near-field beams
- Properties and conditions of Bessel beam generation



arXiv Paper

□ Second part:

- Full-digital extremely-large (XL-) MIMO systems
- Joint channel and data estimation for multiuser XL-MIMO



arXiv Paper

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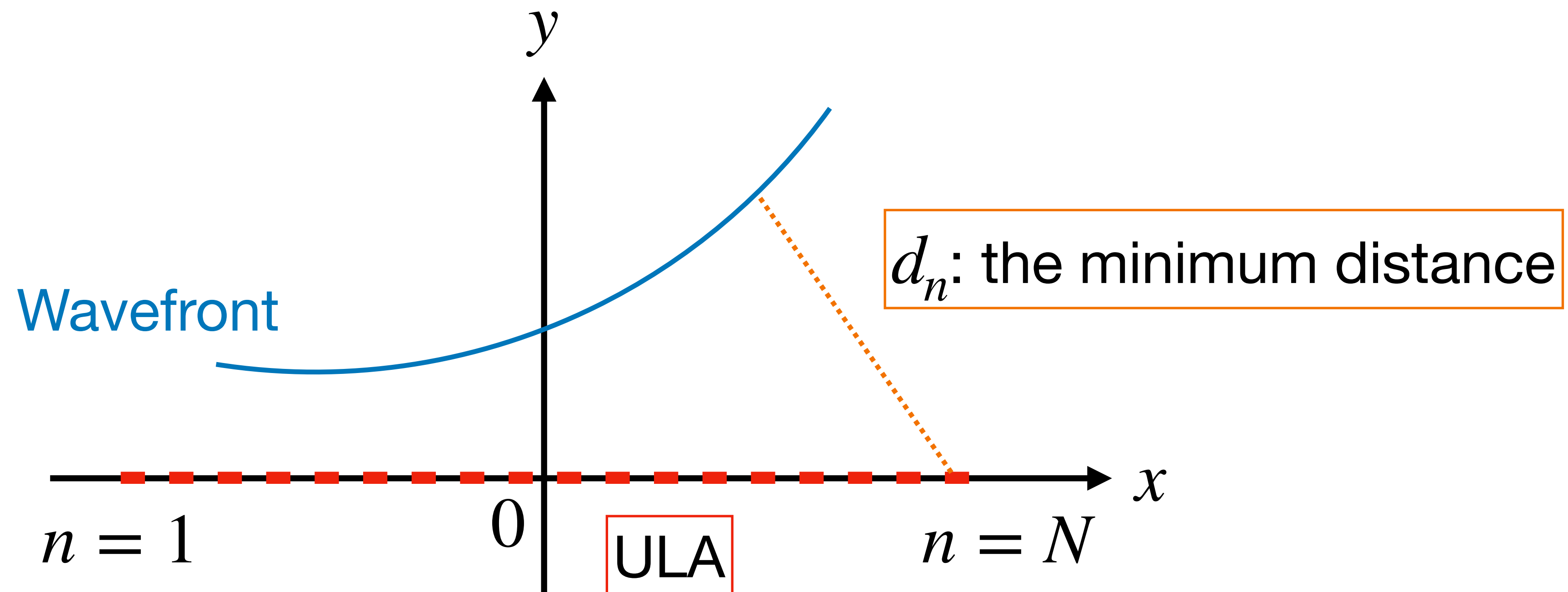
□ Second part:

- Full-digital extremely-large (XL-) MIMO systems
- Joint channel and data estimation for multiuser XL-MIMO



arXiv Paper

- Single propagation with a uniform linear array with N antenna elements
 - Manipulate the phases of phase-shifters ϕ_n
 - The phase can be decomposed into $\phi_n = kd_n$ where k is the wavenumber and d_n is the minimum distance between the n -th antenna element and the wavefront function.

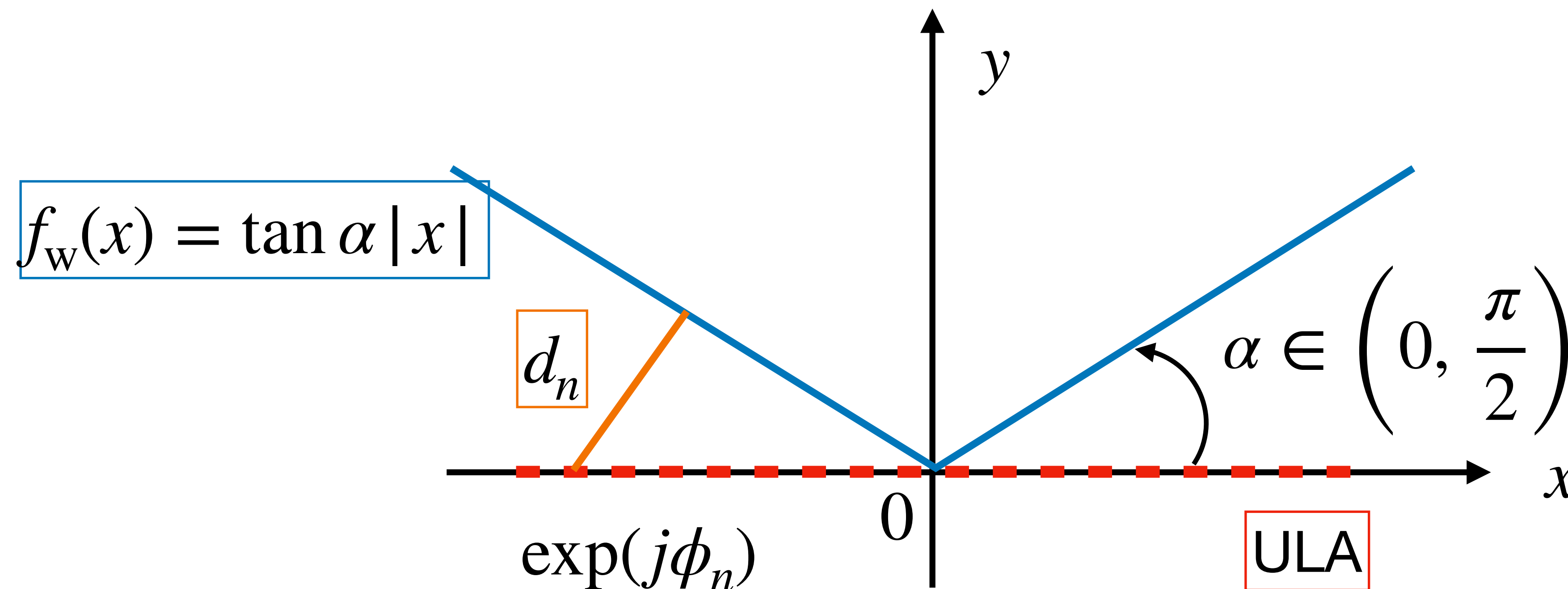


Wavefront Function of Bessel Beam

- A conical wavefront of an antenna array generates a Bessel beam [Phys'87]
- A conical wavefront is described by **an absolute function**

$$f_w(x) = \tan \alpha |x|$$

Hyper-parameter (c.t. beam-width)



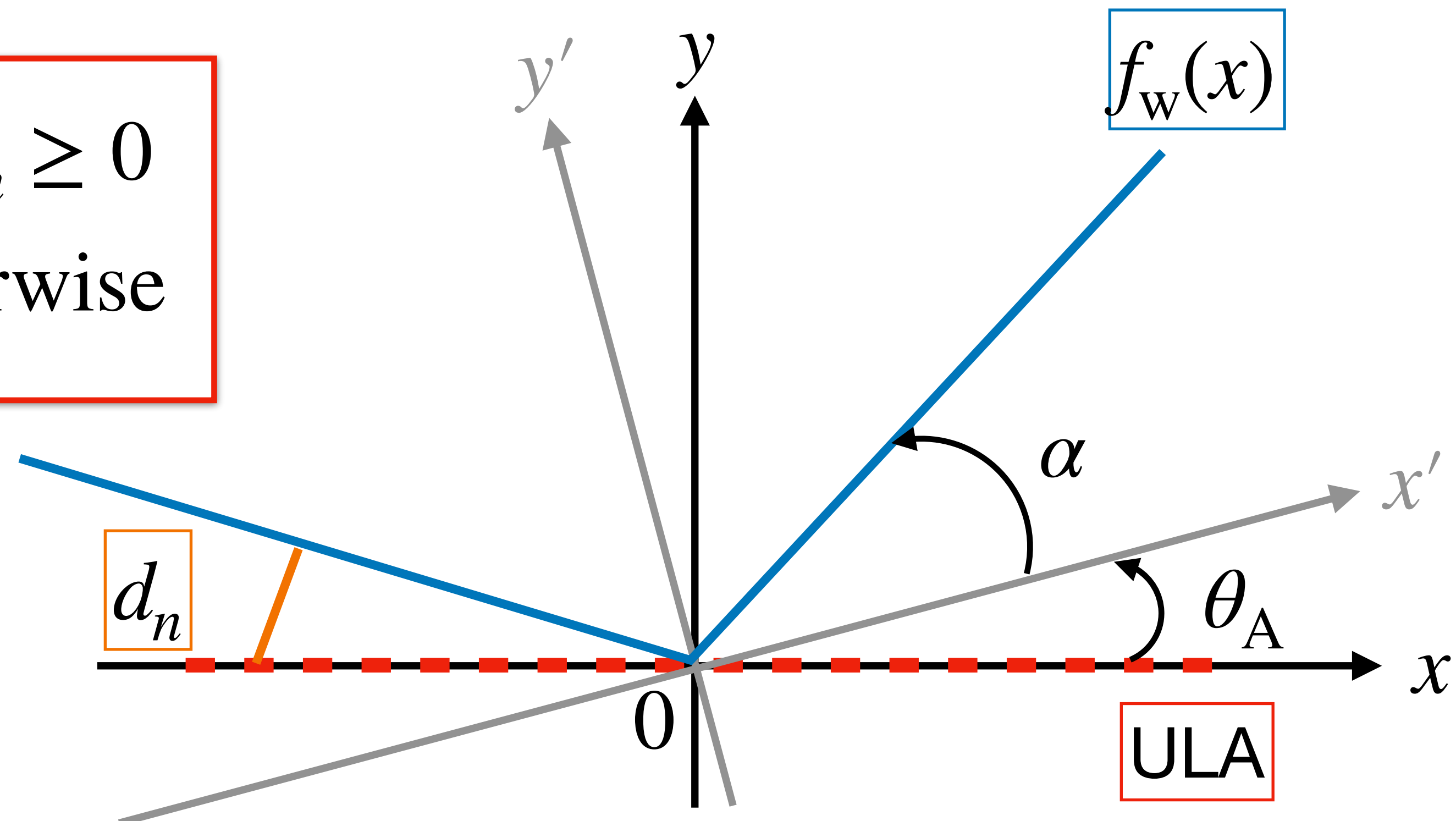
Closed Form Bessel Beam Steering

- Consider a rotated coordinate system (x', y') based on the desired angle θ_A
 - Define an absolute function based on the rotated coordinate system.

$$f_w(x) = \begin{cases} \tan(\alpha - \theta_A)x, & \text{if } x \geq 0 \\ -\tan(\alpha + \theta_A)x, & \text{otherwise} \end{cases}$$

$$\phi_n = \begin{cases} k |\sin(\alpha - \theta_A)| x_{t,n}, & \text{if } x_{t,n} \geq 0 \\ -k |\sin(\alpha + \theta_A)| x_{t,n}, & \text{otherwise} \end{cases}$$

$x_{t,n}$: the position of the n -th element

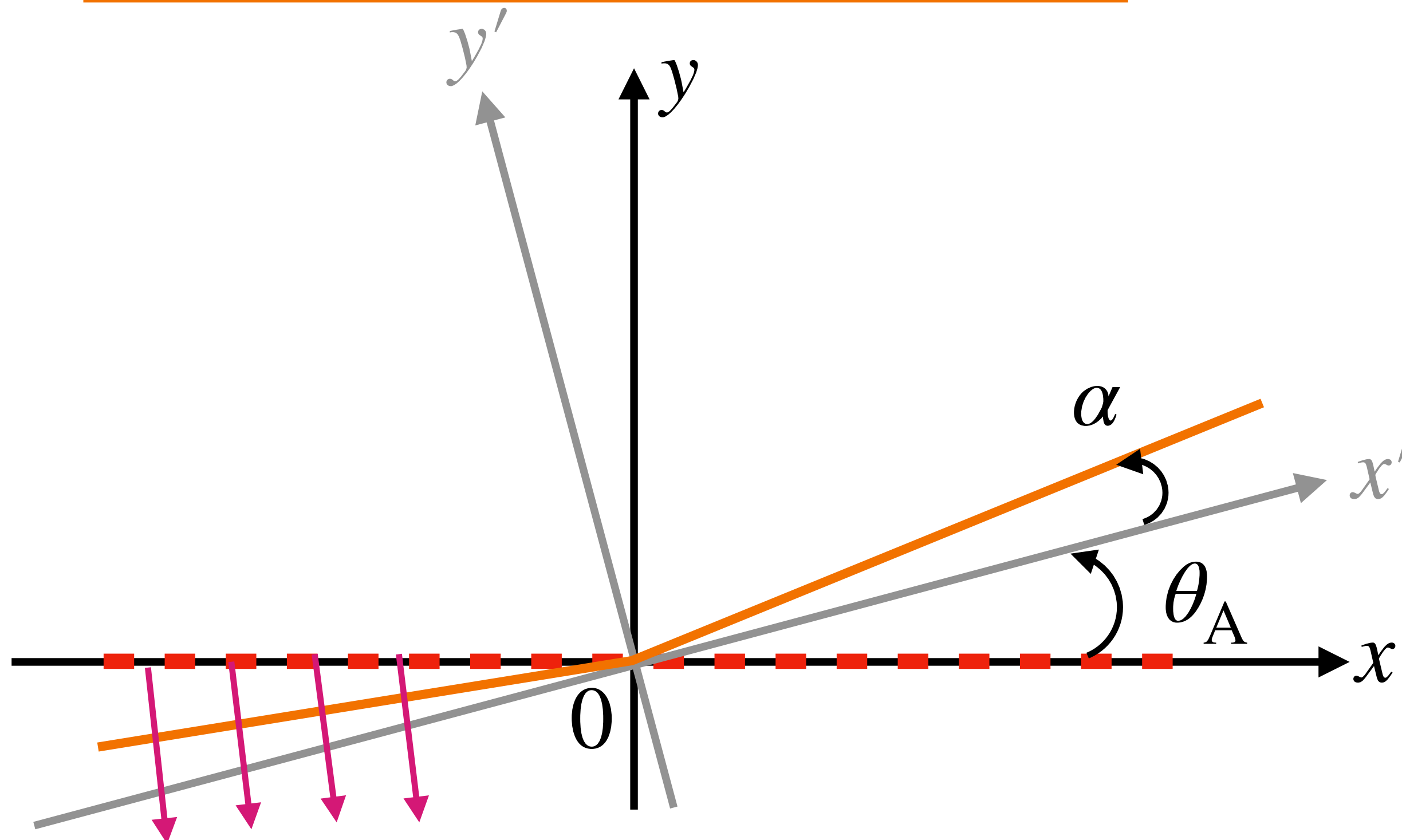


Necessary and Sufficient Condition for Steering

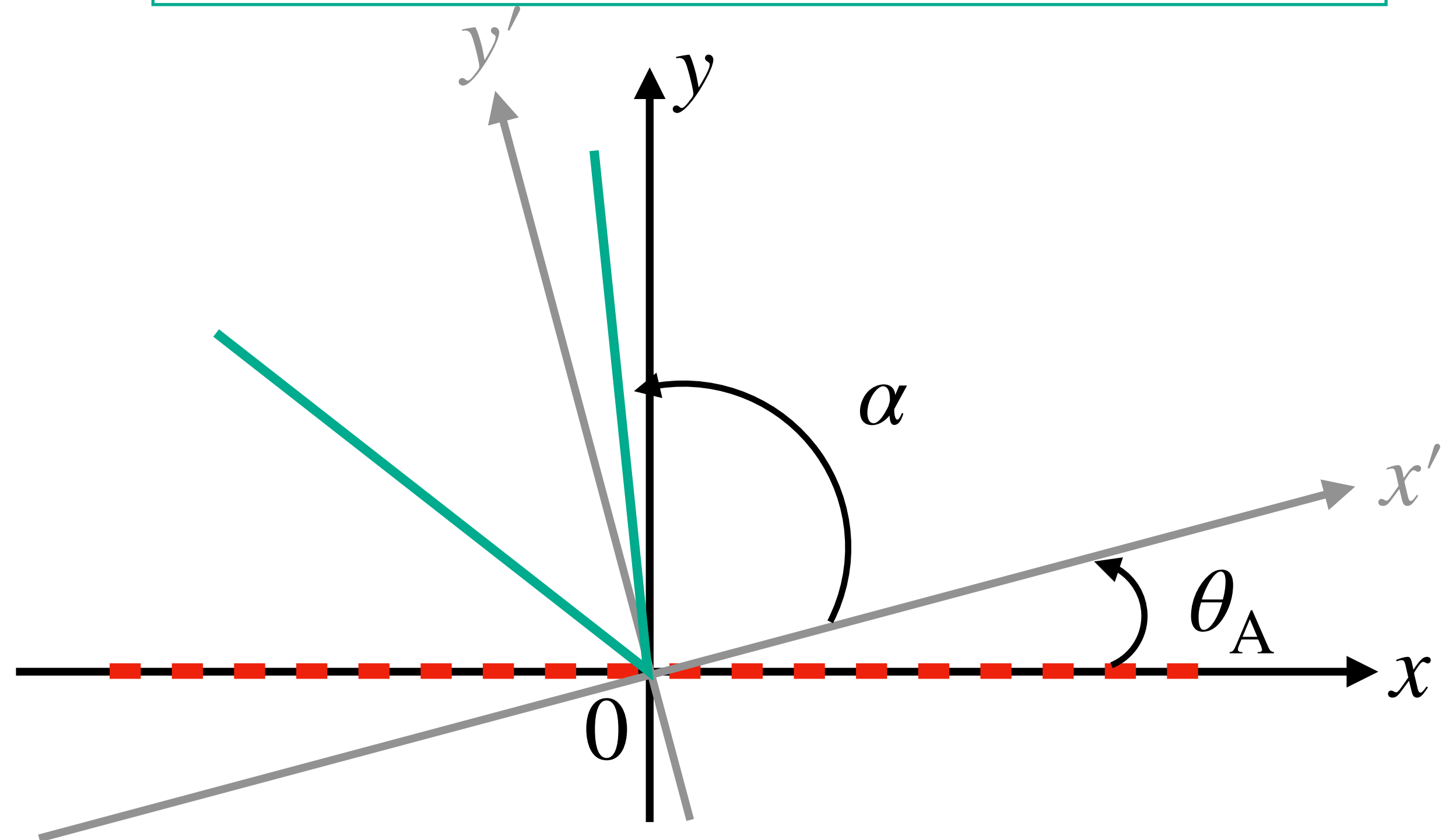
□ The parameter α must satisfy $|\theta_A| \leq \alpha < \frac{\pi}{2} - |\theta_A|$

● Only the desired directions given by $\theta_A \in (-\frac{\pi}{4}, \frac{\pi}{4})$ can be achieved.

$|\theta_A| > \alpha$: reverse propagation



$\alpha \geq \frac{\pi}{2} - |\theta_A|$: impossible wavefront



Maximum Propagation Distance

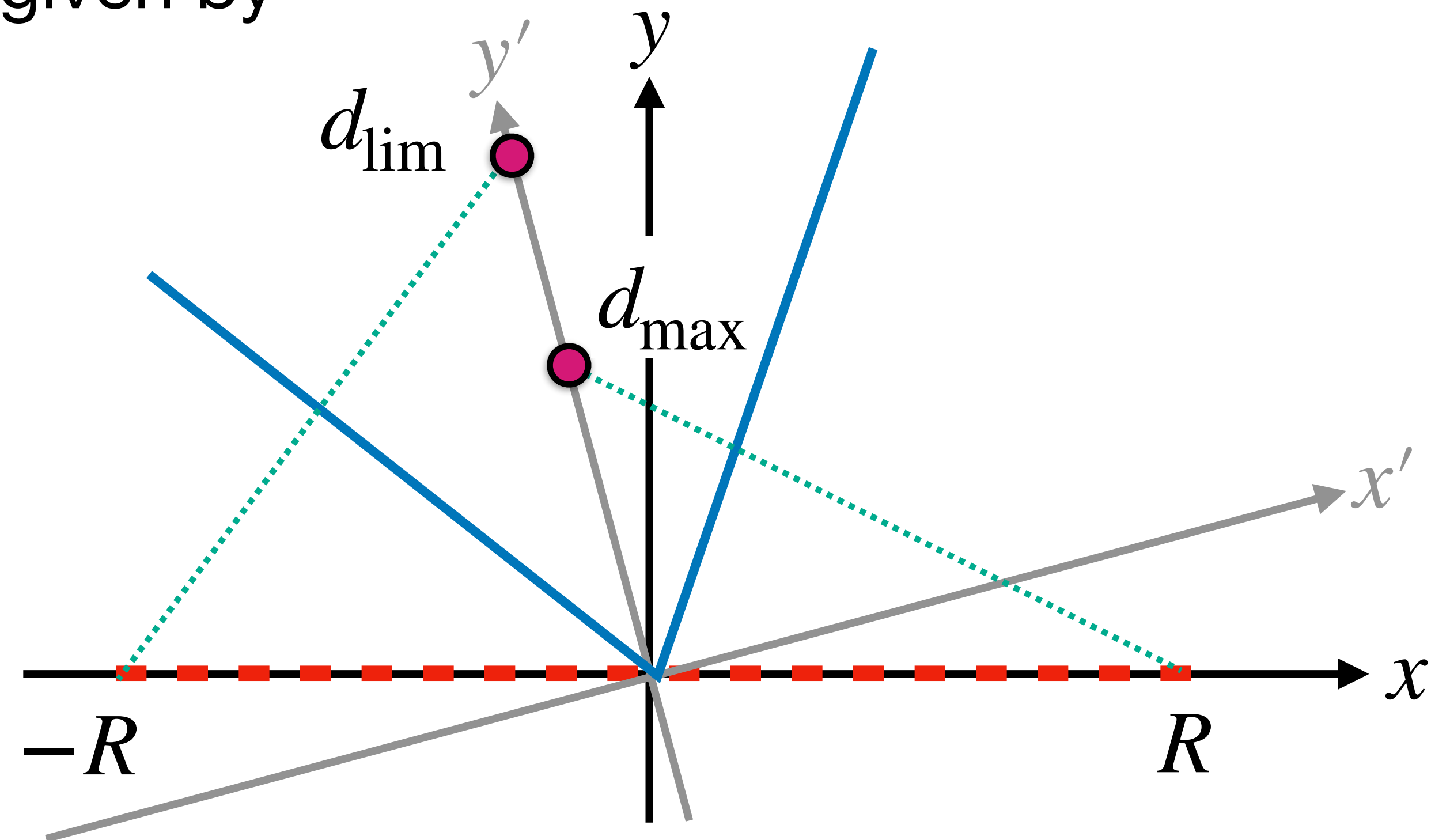
□ Based on geometric optics [SIAM'66],

● the maximum distance of the non-steering Bessel beam is given by $\frac{R}{\tan \alpha}$ [Phys'87].

● In the steering case, the distances are given by

$$d_{\max} = \frac{R}{\tan \alpha} \frac{\cos(\alpha + |\theta_A|)}{\cos \alpha} < \frac{R}{\tan \alpha}$$

$$d_{\lim} = \frac{R}{\tan \alpha} \frac{\cos(\alpha - |\theta_A|)}{\cos \alpha} > \frac{R}{\tan \alpha}$$



[SIAM'66] E. W. Marchand, "Electromagnetic theory and geometrical optics," SIAM Rev., vol.8, no.1, Jan. 1966.

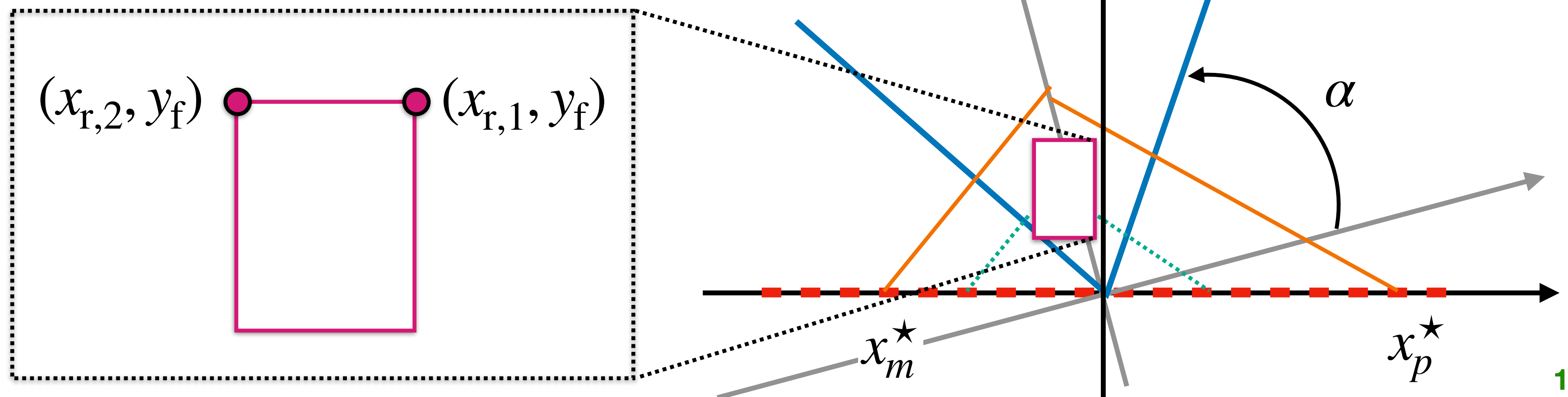
[Phys'87] J. Durnin et al., "Diffraction-free beams," Phys. Rev. Lett., vol.58, pp.1499-1501, Apr. 1987.

□ Consider a rectangular obstacle in the 2D-plane

● The rays from $x_{t,n} < x_p^\star$ are blocked ($x_{t,n} > 0$) / $x_{t,n} > x_m^\star$ are blocked ($x_{t,n} < 0$).

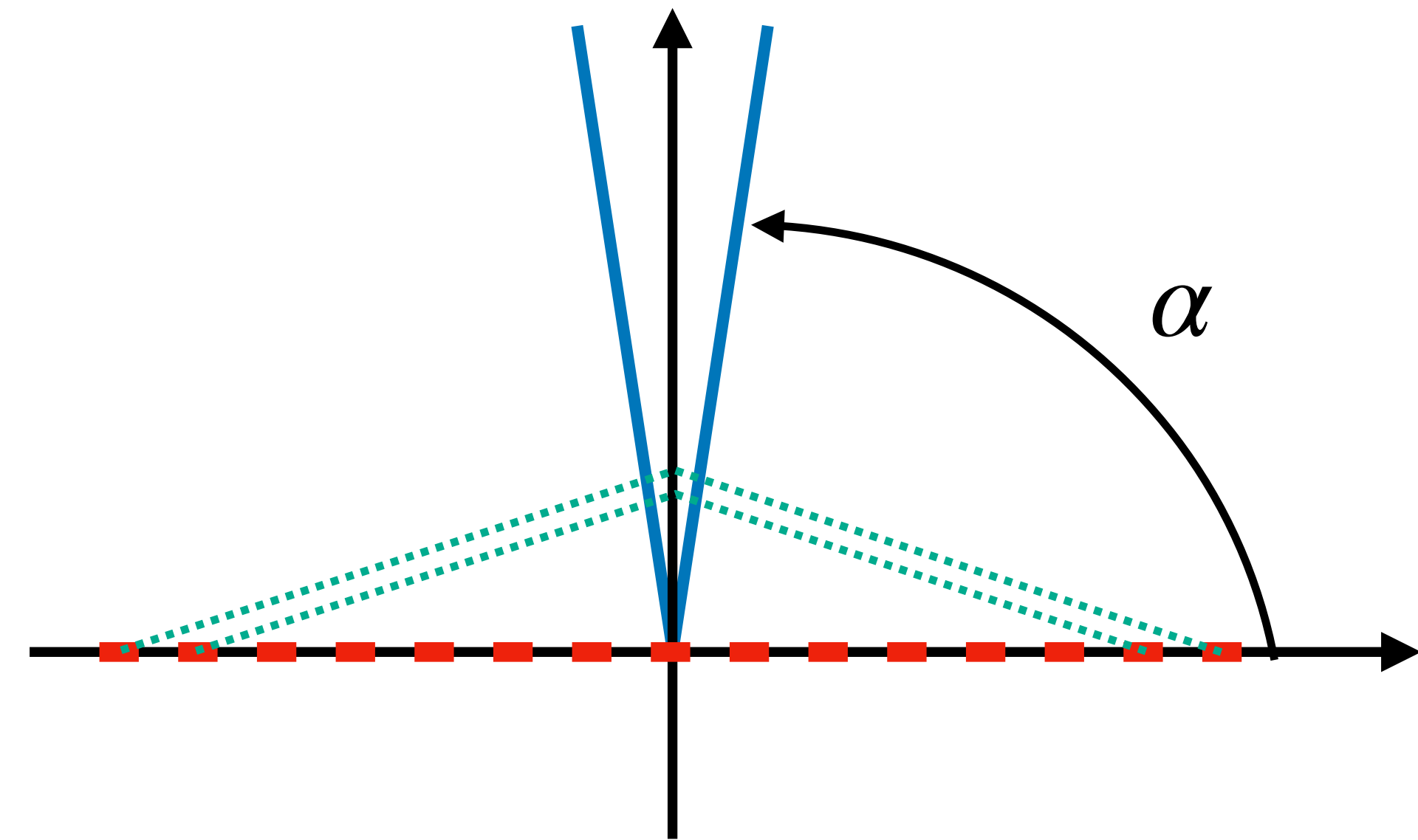
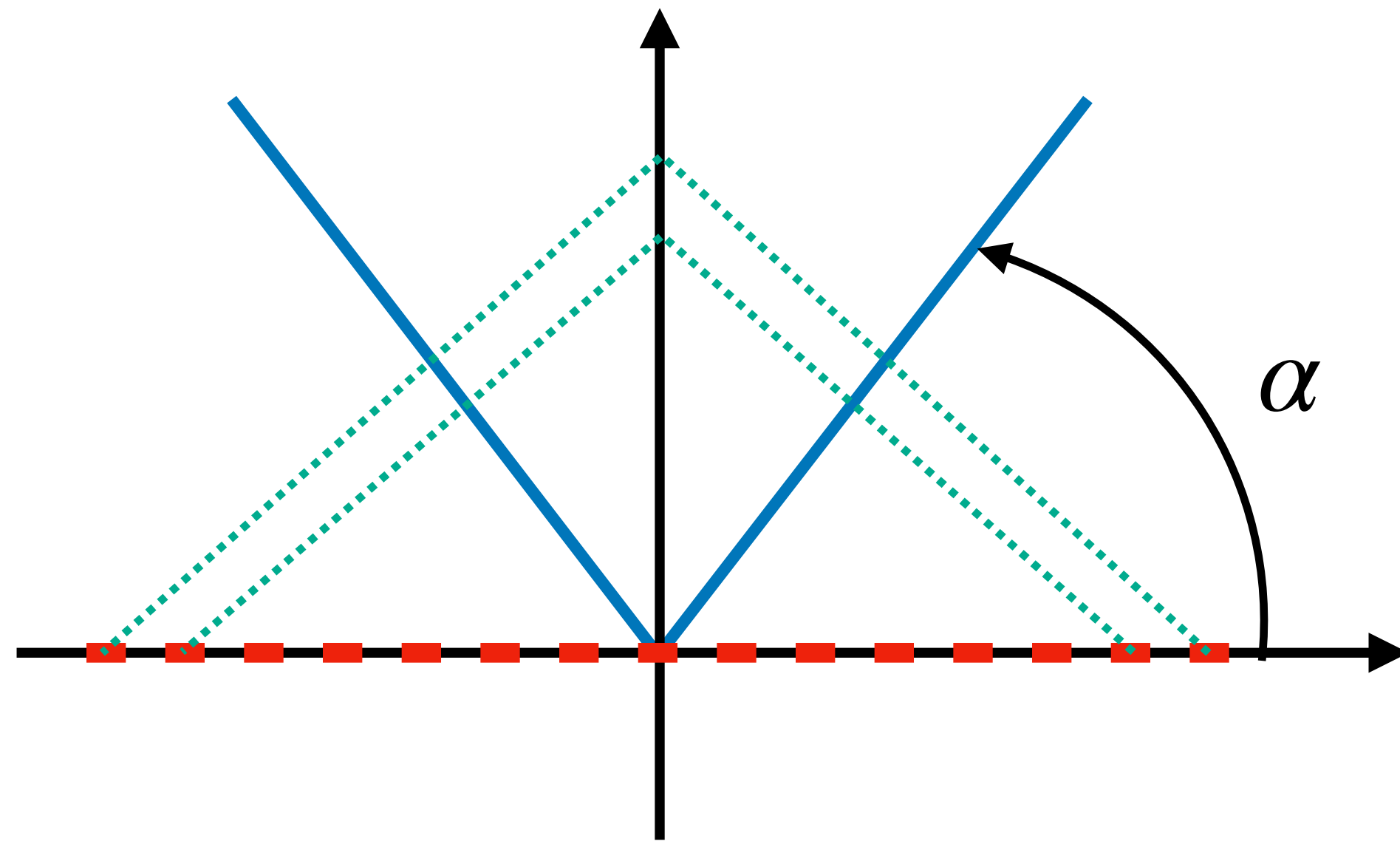
● $x_p^\star = \min_{x \in \mathcal{X}_p} x, \mathcal{X}_p \triangleq \{x \in \mathcal{X}_{\text{arr}} \mid x > x_{r,1} + \tan(\alpha - \theta_A)y_f\}$

● $x_m^\star = \min_{x \in \mathcal{X}_m} x, \mathcal{X}_m \triangleq \{x \in \mathcal{X}_{\text{arr}} \mid x < x_{r,2} - \tan(\alpha + \theta_A)y_f\}$



Maximum Distance vs Self-Healing Capability

- The smaller α leads to the longer maximum distance.
- The larger α leads to the higher self-healing capability.



- Any way to improve both the propagation and self-healing capabilities?
 - The possible approach is the adjustment of the antenna array.

□ Increasing the number of antennas to achieve the distance $d_{\max,d}$ with the fixed α

● From $\frac{R}{\tan \alpha} \frac{\cos(\alpha + |\theta_A|)}{\cos \alpha} \geq d_{\max,d}$, where $R = (N - 1)\Delta/2$

● the minimum number of antenna elements is $N = \left\lceil 2d_{\max,d} \frac{\sin \alpha}{\Delta \cos(\alpha + |\theta_A|)} + 1 \right\rceil$.
[\cdot]: a ceiling function

□ Increasing the antenna spacing to achieve the distance $d_{\max,d}$ with the fixed α

● $\Delta = 2d_{\max,d} \frac{\sin \alpha}{(N - 1)\cos(\alpha + |\theta_A|)}$

● However, **the sampling theorem in the spatial domain** should be satisfied.

Antenna Spacing Condition from Sampling Theorem

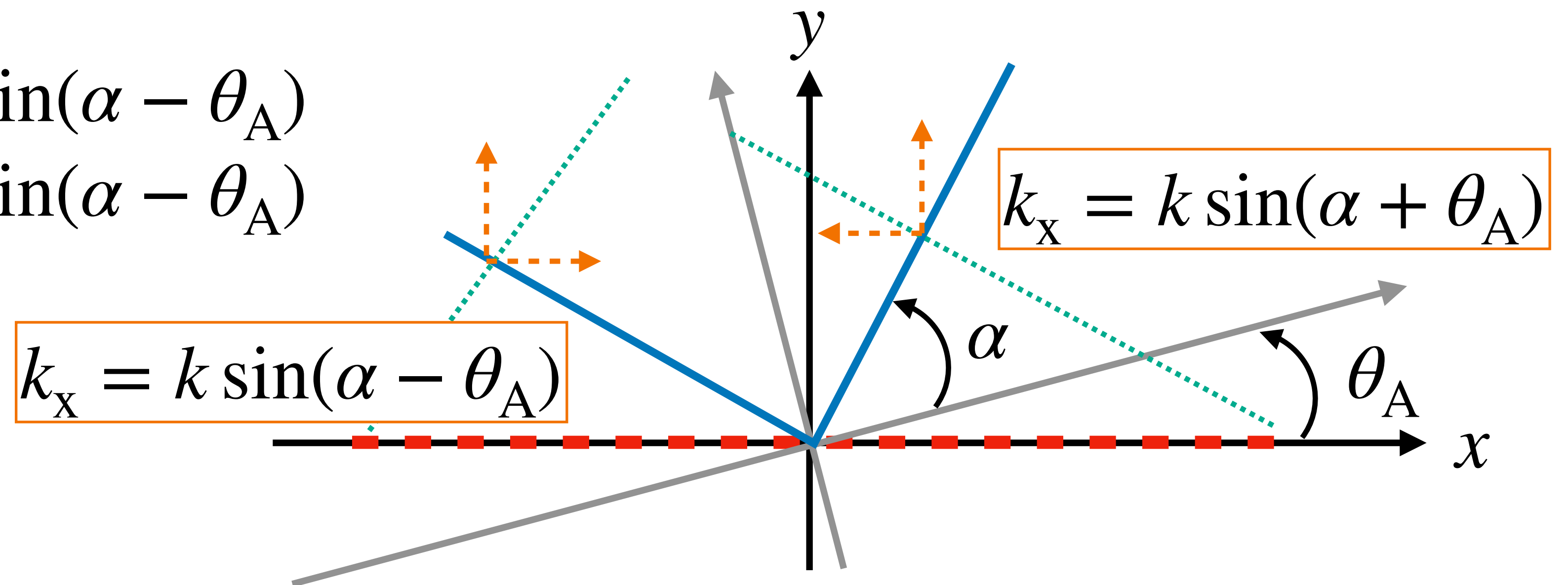
□ Since the ULA is located on the x -axis, the sampling theorem is $\Delta < \frac{\pi}{k_x}$ [TSP'22],

● $\Delta < \frac{\lambda}{2 \sin(\alpha + |\theta_A|)}$ should be satisfy to properly generate Bessel beams

● Under the necessary and sufficient condition, $\frac{1}{\sin(\alpha + |\theta_A|)} > 1$, which means **the ULA with the half-wavelength spacing can generate any Bessel beam.**

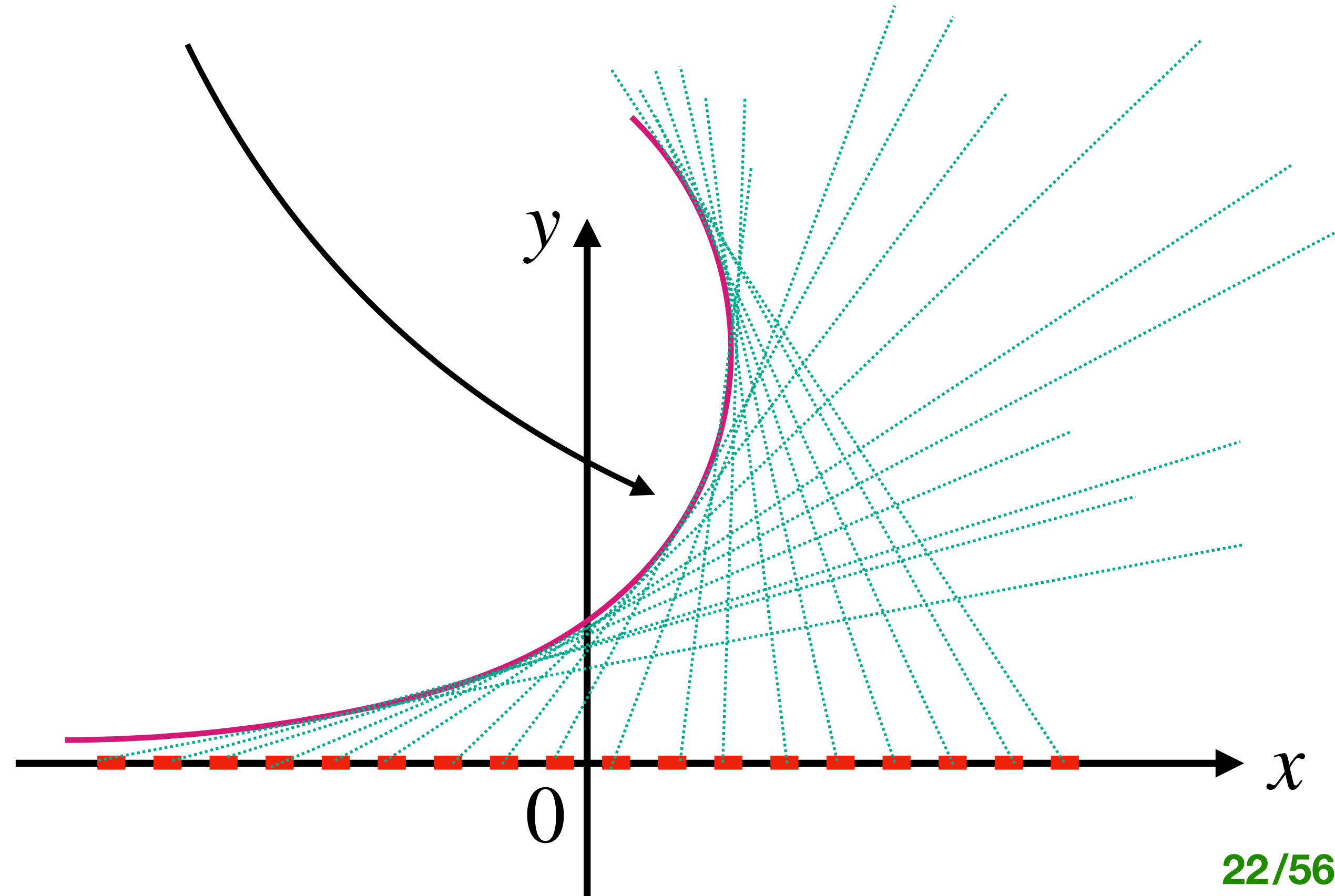
$$\theta_A > 0, \sin(\alpha + \theta_A) > \sin(\alpha - \theta_A)$$

$$\theta_A < 0, \sin(\alpha + \theta_A) < \sin(\alpha - \theta_A)$$



Curving Beams

- Consider design of curving beams. In ULA systems,
 - any trajectory described by convex or concave functions can be achieved.
 - only the parabolic trajectory is considered to simplify the discussion, where the trajectory function is given by $f_t(y) = \beta(y - p)^2 + q$.
 - the envelope forms a curving beam.



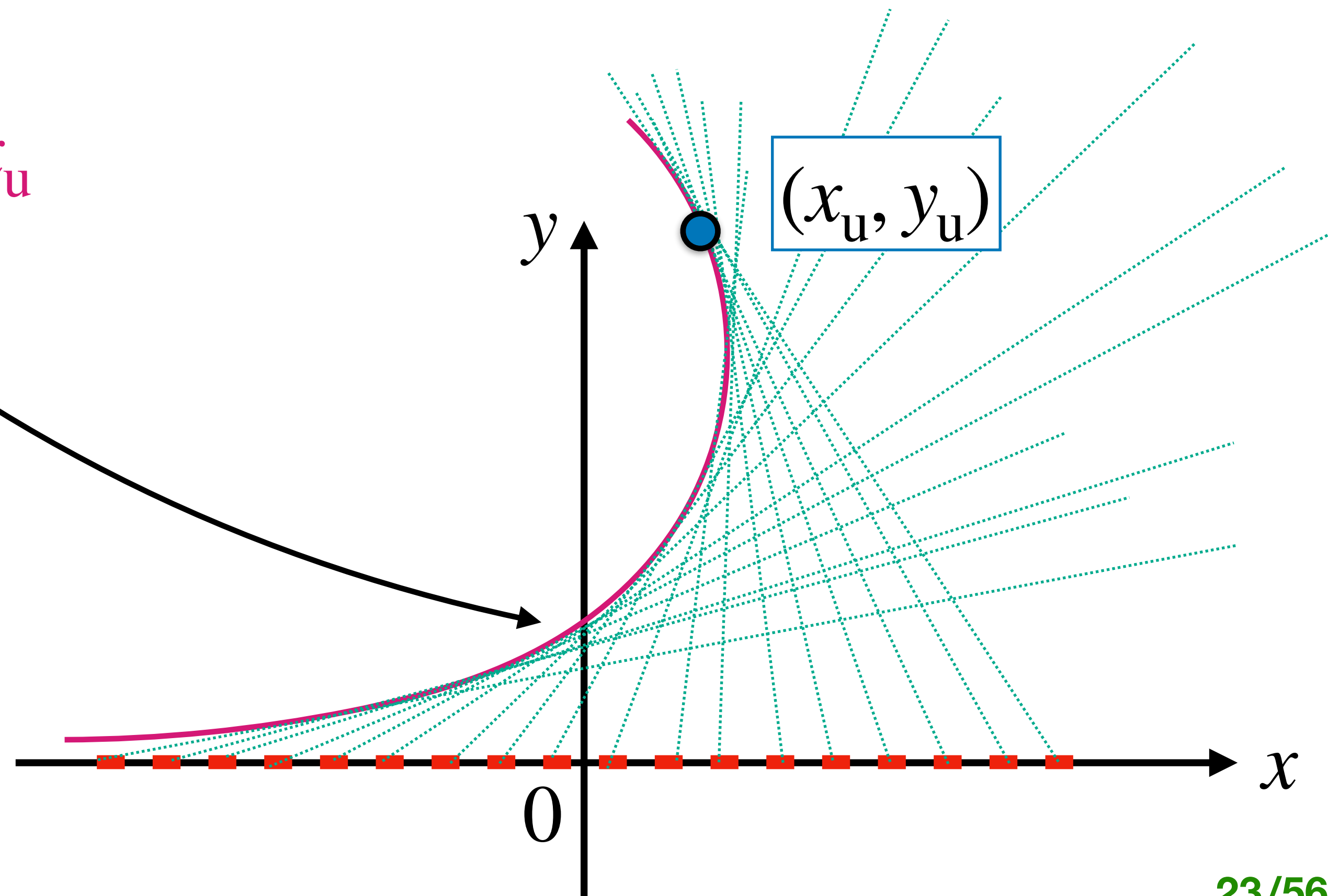
Parabolic Trajectory to a User

□ Consider a user, whose position is (x_u, y_u) .

● The parameters β, p, q should satisfy $x_u = \beta(y_u - p)^2 + q$, which leads to

$$q = x_u - \beta(y_u - p)^2 \text{ and}$$

$$f_t(y) = \beta(y^2 - y_u^2) - 2\beta p(y - y_u) + x_u$$



□ Based on the study of [TWC'25], the phase at the n -th element is given by

$$\phi_n = k \left\{ \frac{\log(\sqrt{c_1} - c_2)}{4|\beta|} - \left(p + \sqrt{\frac{\beta p^2 + q - x_{t,n}}{\beta}} \right) \frac{\sqrt{c_1}}{2} \right\}$$

where

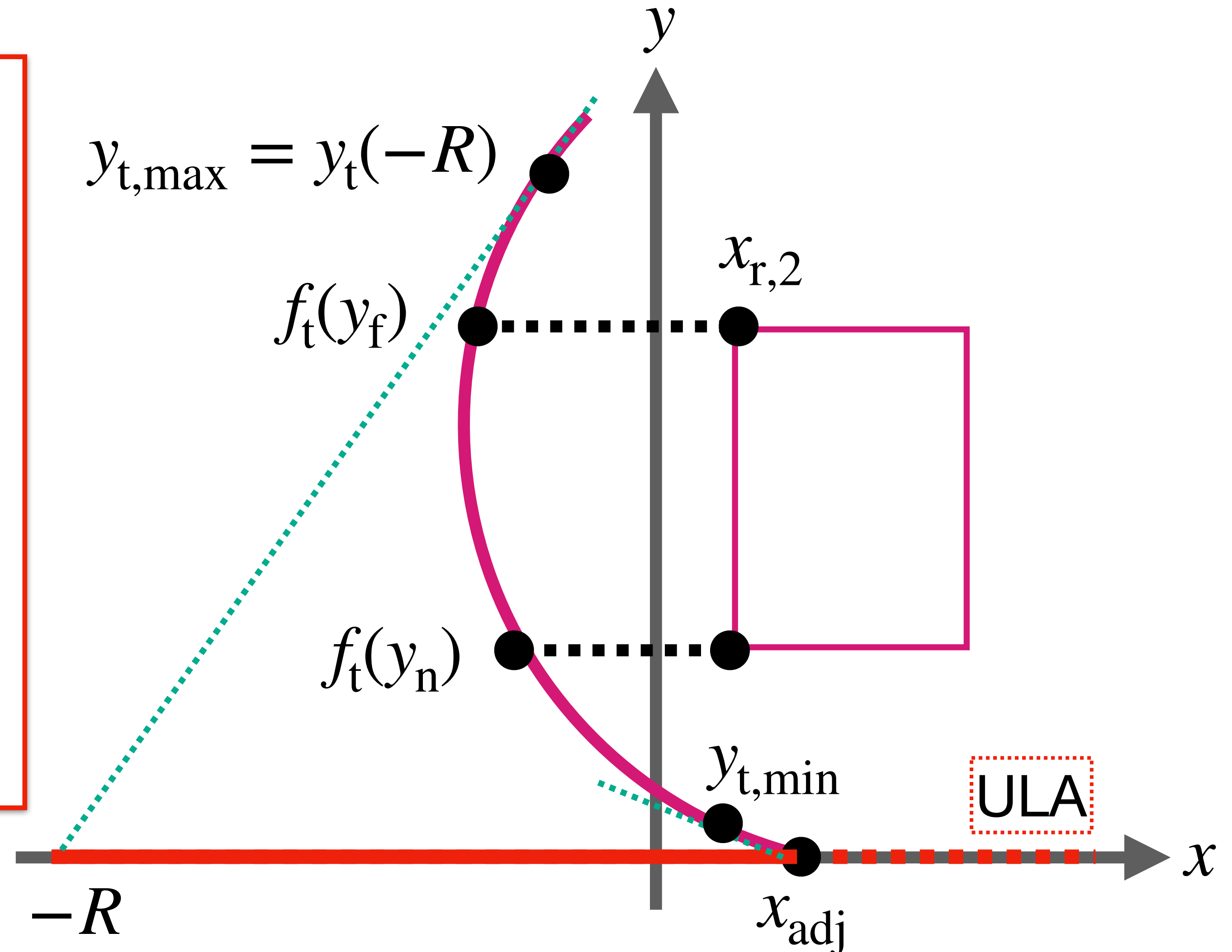
$$c_1 = 4\beta^2 p^2 + 4\beta(\beta p^2 + q - x_{t,n}) - 8\beta^2 p \sqrt{\frac{\beta p^2 + q - x_{t,n}}{\beta}} + 1$$

$$c_2 = \left(2\beta^2 p - 2\beta^2 \sqrt{\frac{\beta p^2 + q - x_{t,n}}{\beta}} \right) \frac{1}{|\beta|}$$

- From $q = x_u - \beta(y_u - p)^2$, **the design of curving beams is equivalent to the design of the parameters β and p .**

- Joint optimization of the parameters and the effective aperture of the ULA to avoid **the known obstacle**

Find $\beta > 0$, p , x_{adj}
 subject to $f_t(y_n) \leq x_{r,2}$
 $f_t(y_f) \leq x_{r,2}$
 $y_{t,\min} \leq y_u$
 $y_u \leq y_{t,\max}$
 $x_{\text{adj}} \in \mathcal{X}_{\text{arr}}$
 \mathcal{X}_{cal} : the set of antenna positions



- Based on the Lagrangian method,
the possible candidates of the closed-form solutions are given by

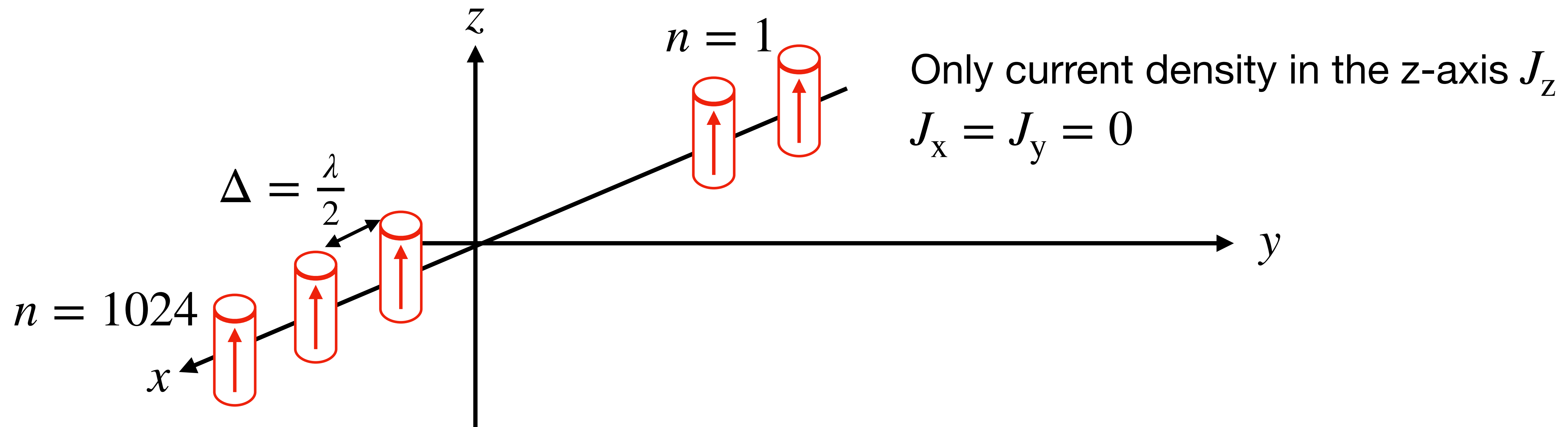
$$(\beta, \tilde{p}, x_{\text{adj}}) = \left\{ \begin{array}{l} \left(\frac{-(x_{r,2} - x_u)}{(y_f - y_u)(y_n - y_u)}, \frac{-(x_{r,2}y_f - x_u y_f + x_{r,2}y_n - x_u y_n)}{2(y_f - y_u)(y_n - y_u)}, \frac{x_{r,2}y_u^2 + x_u y_f y_n - x_{r,2}y_f y_u - x_{r,2}y_n y_u}{(y_f - y_u)(y_n - y_u)} \right) \\ \left(\frac{-(Ry_f - Ry_u + x_u y_f - x_{r,2}y_u)}{y_u(y_f - y_u)^2}, \frac{-(Ry_f^2 - Ry_u^2 + x_u y_f^2 - 2x_{r,2}y_u^2 + x_u y_u^2)}{2y_u(y_f - y_u)^2}, \frac{-(Ry_f^2 - x_{r,2}y_u^2 - Ry_f y_u + x_u y_f y_u)}{(y_f - y_u)^2} \right) \\ \left(\frac{-(Ry_n - Ry_u + x_u y_n - x_{r,2}y_u)}{y_u(y_n - y_u)^2}, \frac{-(Ry_n^2 - Ry_u^2 + x_u y_n^2 - 2x_{r,2}y_u^2 + x_u y_u^2)}{2y_u(y_n - y_u)^2}, \frac{-(Ry_n^2 - x_{r,2}y_u^2 - Ry_n y_u + x_u y_n y_u)}{(y_n - y_u)^2} \right) \\ \dots \\ \left(\frac{Ry_f - Ry_u - x_u y_f + x_{r,2}y_u}{y_f y_u (y_f - y_u)}, \frac{Ry_f^2 - Ry_u^2 - x_u y_f^2 + x_{r,2}y_u^2}{2y_f y_u (y_f - y_u)}, R \right) \\ \left(\frac{Ry_n - Ry_u - x_u y_n + x_{r,2}y_u}{y_n y_u (y_n - y_u)}, \frac{Ry_n^2 - Ry_u^2 - x_u y_n^2 + x_{r,2}y_u^2}{2y_n y_u (y_n - y_u)}, R \right) \\ \left(\frac{-(Ry_f - Ry_u + x_u y_f - x_{r,2}y_u)}{y_u(y_f - y_u)^2}, \frac{-(Ry_f^2 - Ry_u^2 + x_u y_f^2 - 2x_{r,2}y_u^2 + x_u y_u^2)}{2y_u(y_f - y_u)^2}, R \right) \\ \left(\frac{-(Ry_n - Ry_u + x_u y_n - x_{r,2}y_u)}{y_u(y_n - y_u)^2}, \frac{-(Ry_n^2 - Ry_u^2 + x_u y_n^2 - 2x_{r,2}y_u^2 + x_u y_u^2)}{2y_u(y_n - y_u)^2}, R \right) \\ \left(\frac{Ry_f - Ry_u - x_u y_f + x_{r,2}y_u}{y_u(y_f - y_u)^2}, \frac{-(Ry_u^2 - Ry_f^2 + x_u y_f^2 - 2x_{r,2}y_u^2 + x_u y_u^2)}{2y_u(y_f - y_u)^2}, R \right) \\ \left(\frac{Ry_n - Ry_u - x_u y_n + x_{r,2}y_u}{y_u(y_n - y_u)^2}, \frac{-(Ry_u^2 - Ry_n^2 + x_u y_n^2 - 2x_{r,2}y_u^2 + x_u y_u^2)}{2y_u(y_n - y_u)^2}, R \right) \end{array} \right. \quad \tilde{p} = \beta p$$

↓ Full exploitation of a ULA

The trajectories with negative curvatures can be designed in the same manner.

General Setup For Numerical Results

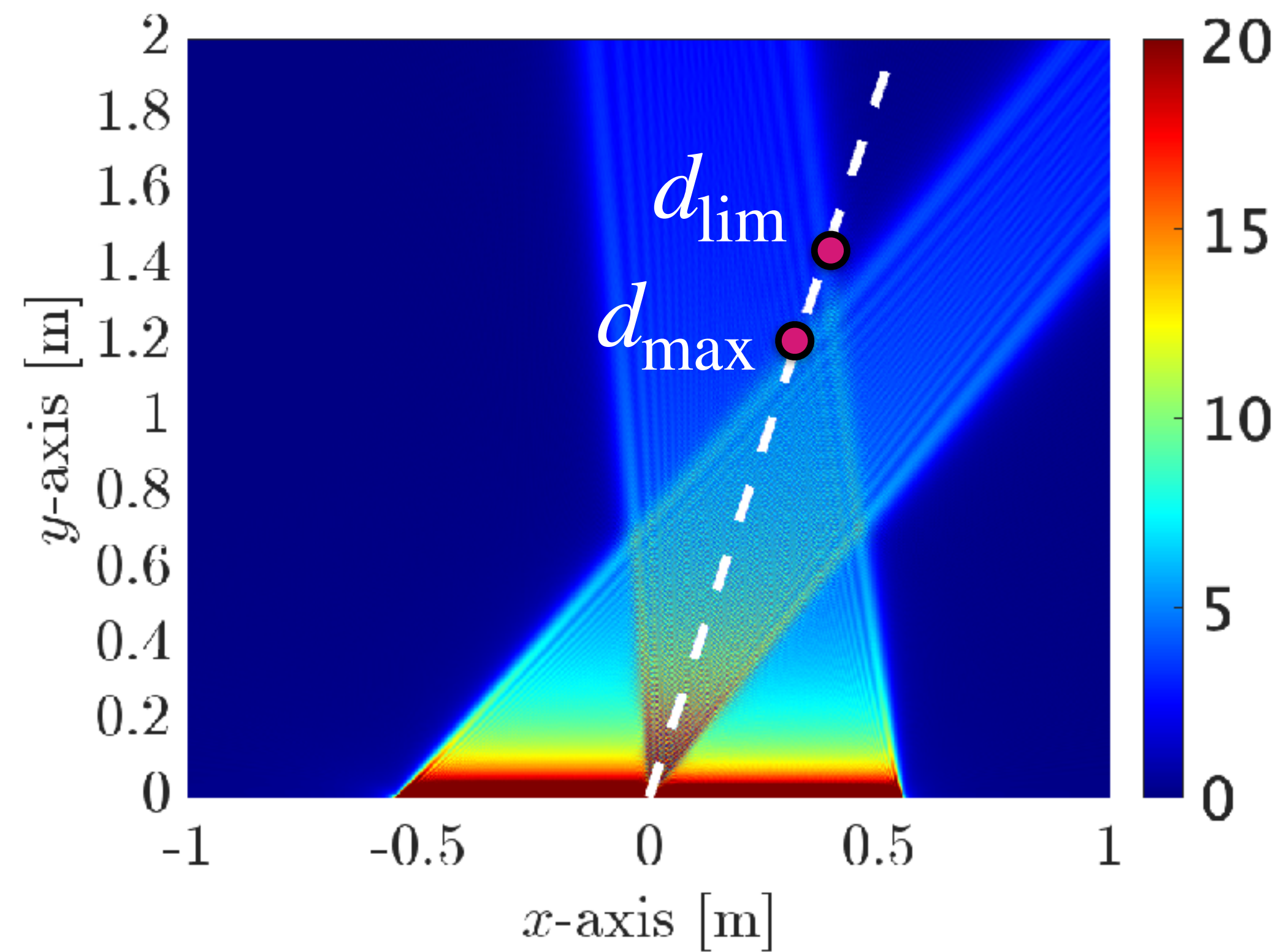
- Consider the 3D coordinate system
 - The ULA is modeled as the set of ideal dipole sources.
 - The central frequency is set to 140 [GHz]
 - Electric fields in the xy -plane are calculated by EM simulations.



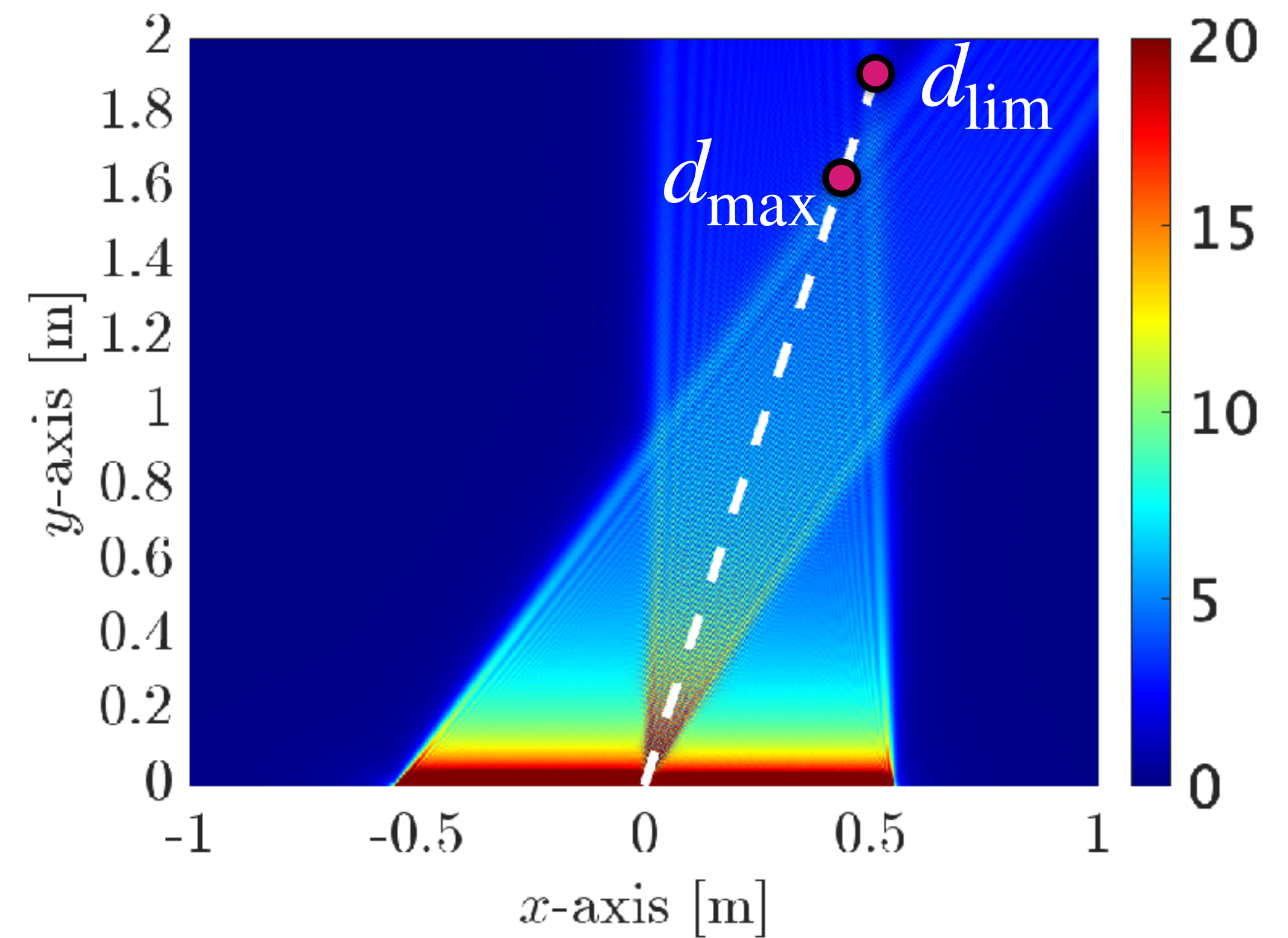
Steering Bessel Beams

- The desired angle is set to $\theta_A = 15$ [deg].
- A smaller α achieves a longer propagation distance.

Magnitude of the electric field in the xy -plane [kV/m]



$\alpha = 20$ [deg]

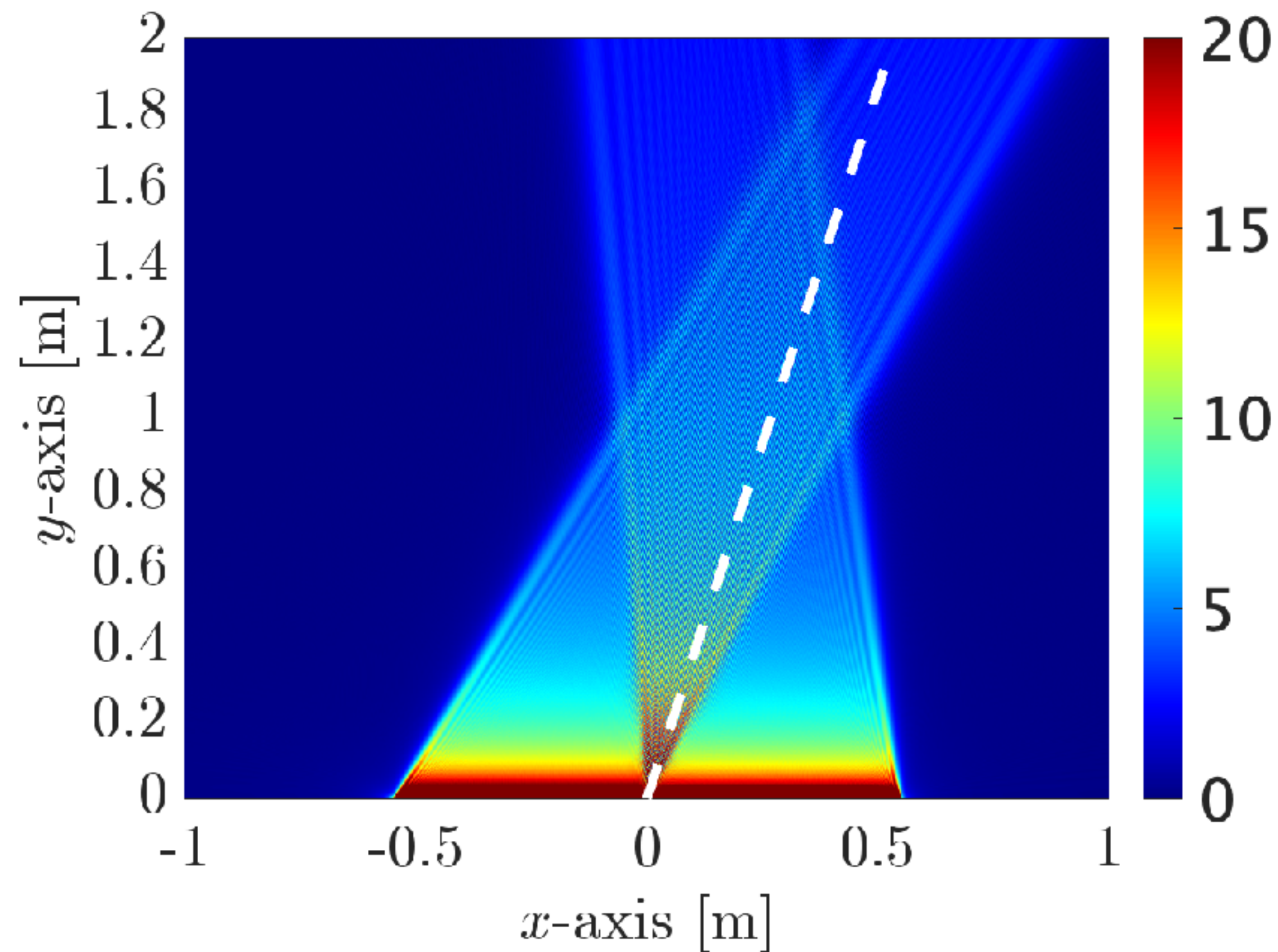


$\alpha = 15$ [deg]

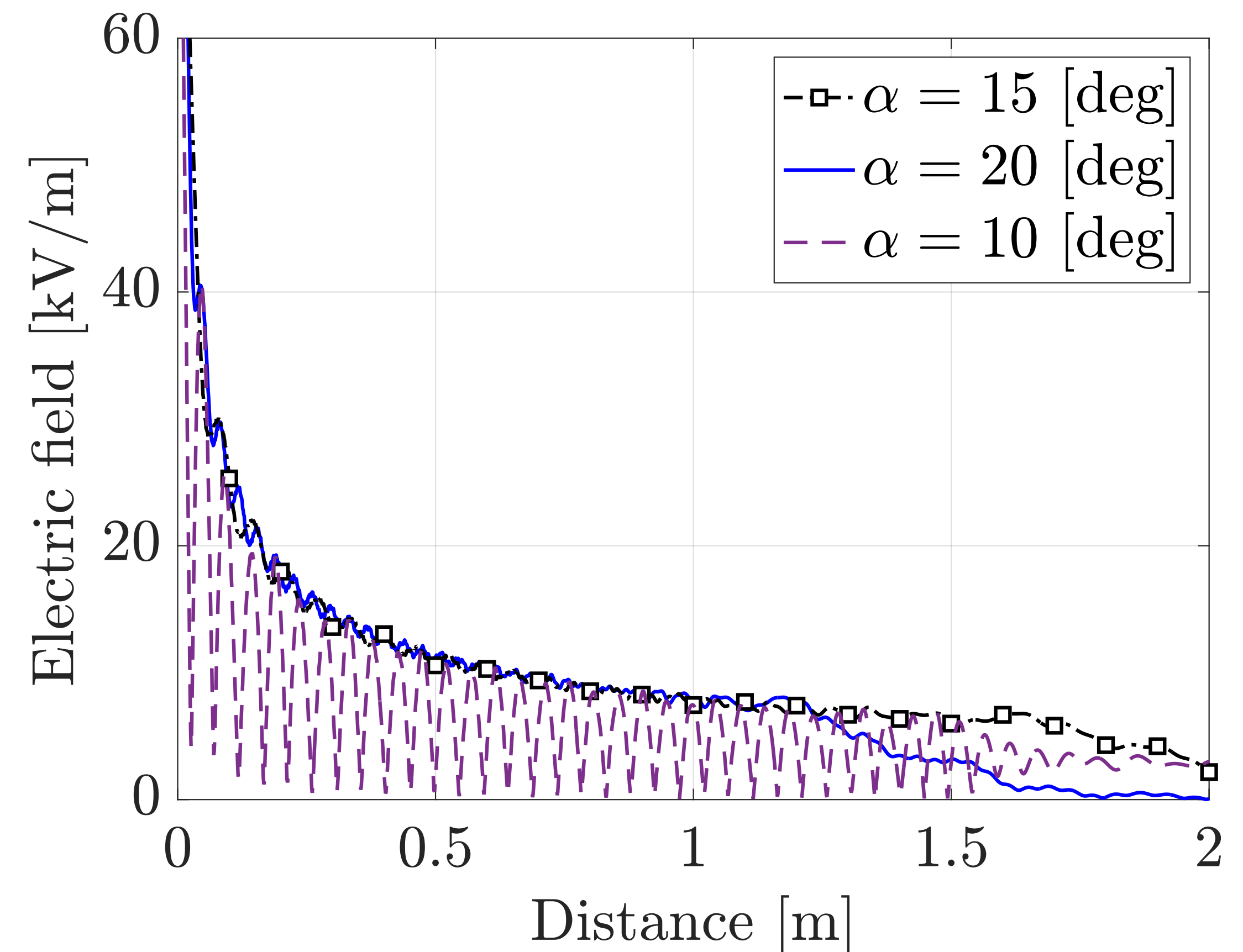
Non-diffraction Propagation of Bessel Beams

□ If $\alpha < |\theta_A|$, *quasi-non-diffraction propagation cannot be achieved.*

$\alpha = 10$ [deg] ($< \theta_A = 15$ [deg])



E-field along the desired direction



Sampling Theorem for Bessel Beams

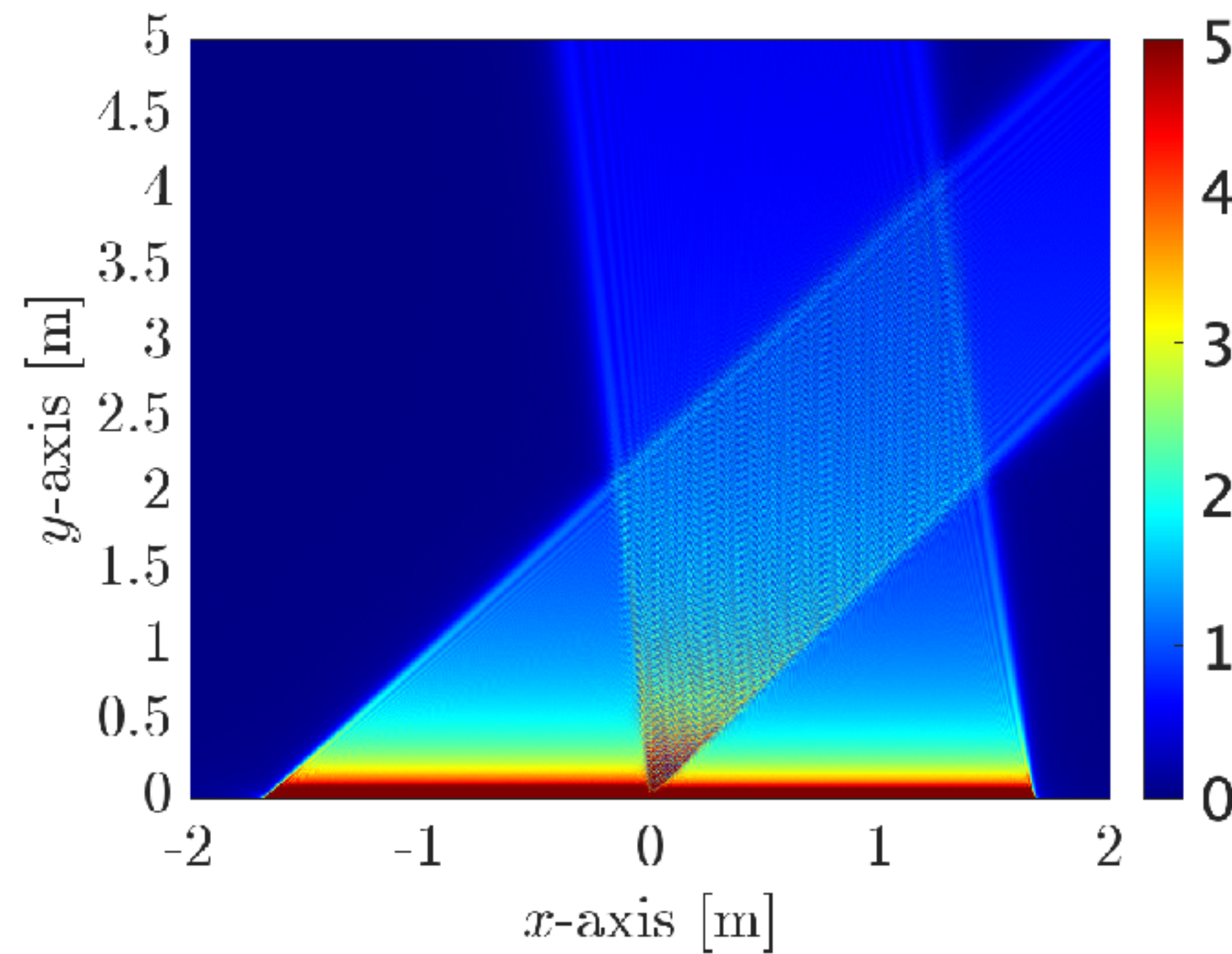
□ The desired distance is set to $d_{\max,d} = 4$ [m] with $\theta_A = 15$ and $\alpha = 20$ [deg].

● $\Delta < \frac{\lambda}{2 \sin(\alpha + |\theta_A|)} = 0.0018666\dots$ should be satisfied.

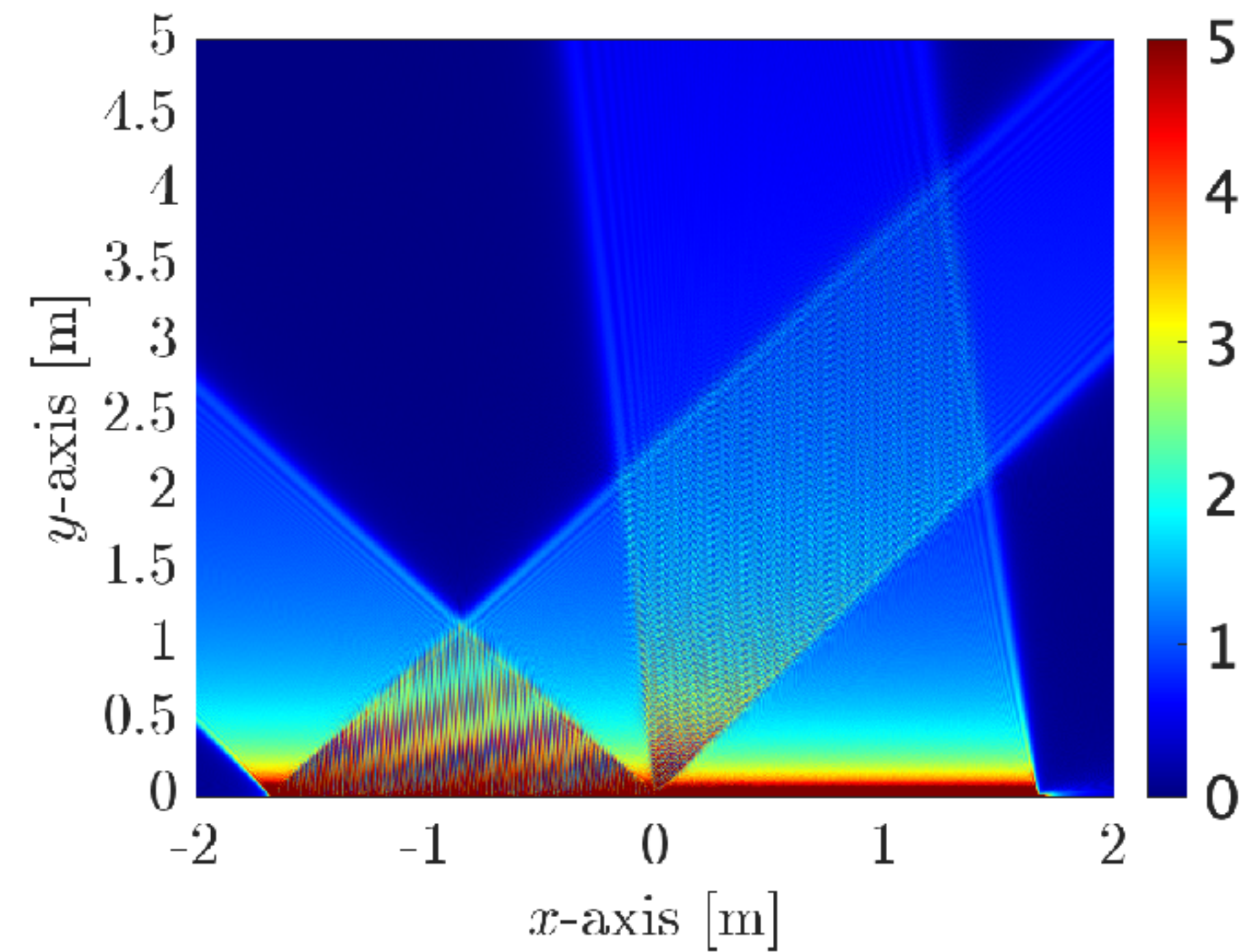
□ Grating lobes appear (right figure)

□ Under the condition, the unintended beam does not interfere with the desired beam.

$$N = 3121, \Delta = \frac{\pi}{2}$$



$$N = 1797, \Delta = 0.00186$$

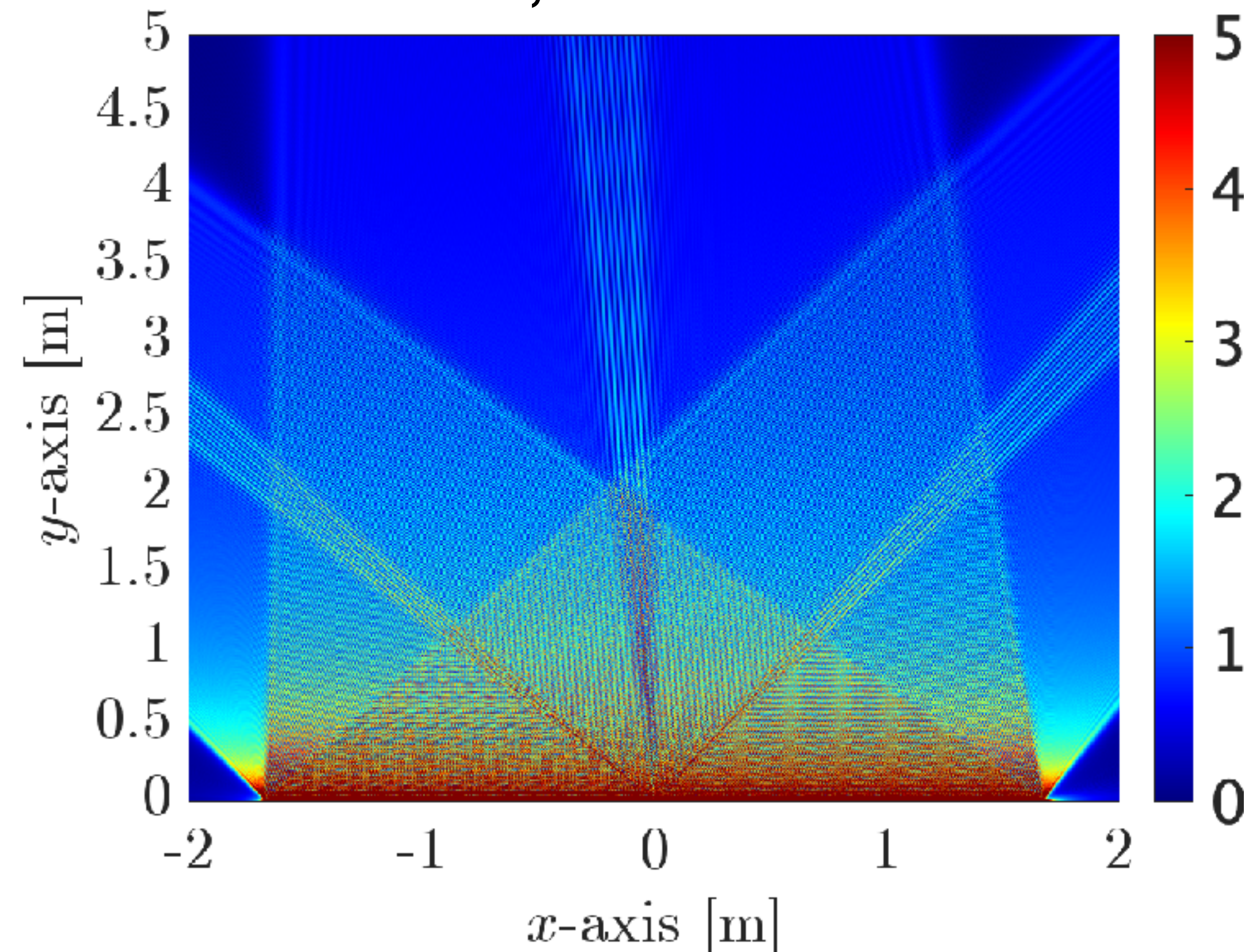


□ The desired distance is set to $d_{\max,d} = 4$ [m] with $\theta_A = 15$ and $\alpha = 20$ [deg].

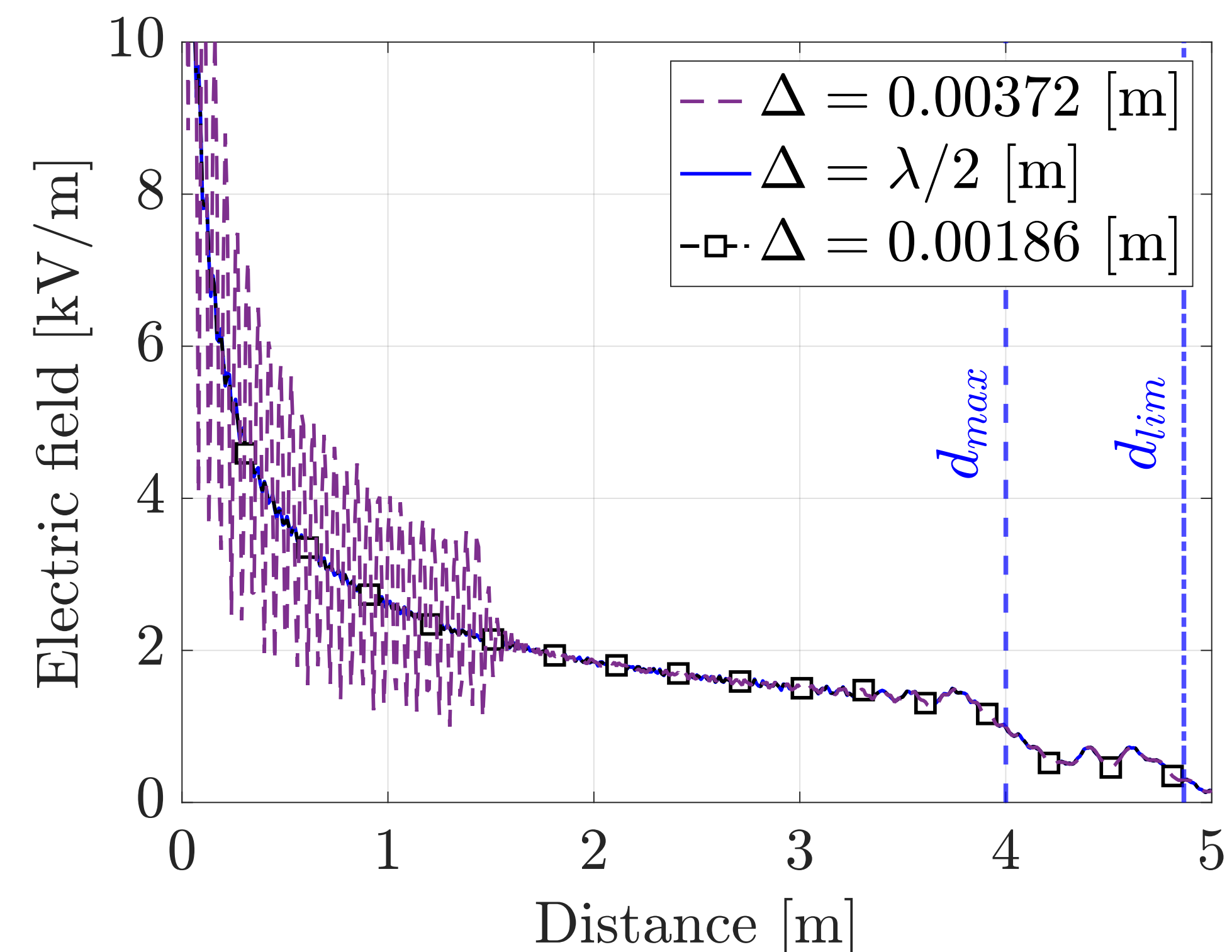
● $\Delta < \frac{\lambda}{2 \sin(\alpha + |\theta_A|)} = 0.0018666\dots$ should be satisfied.

● *Quasi-non-diffraction propagation cannot be achieved.*

$N = 899, \Delta = 0.00372$

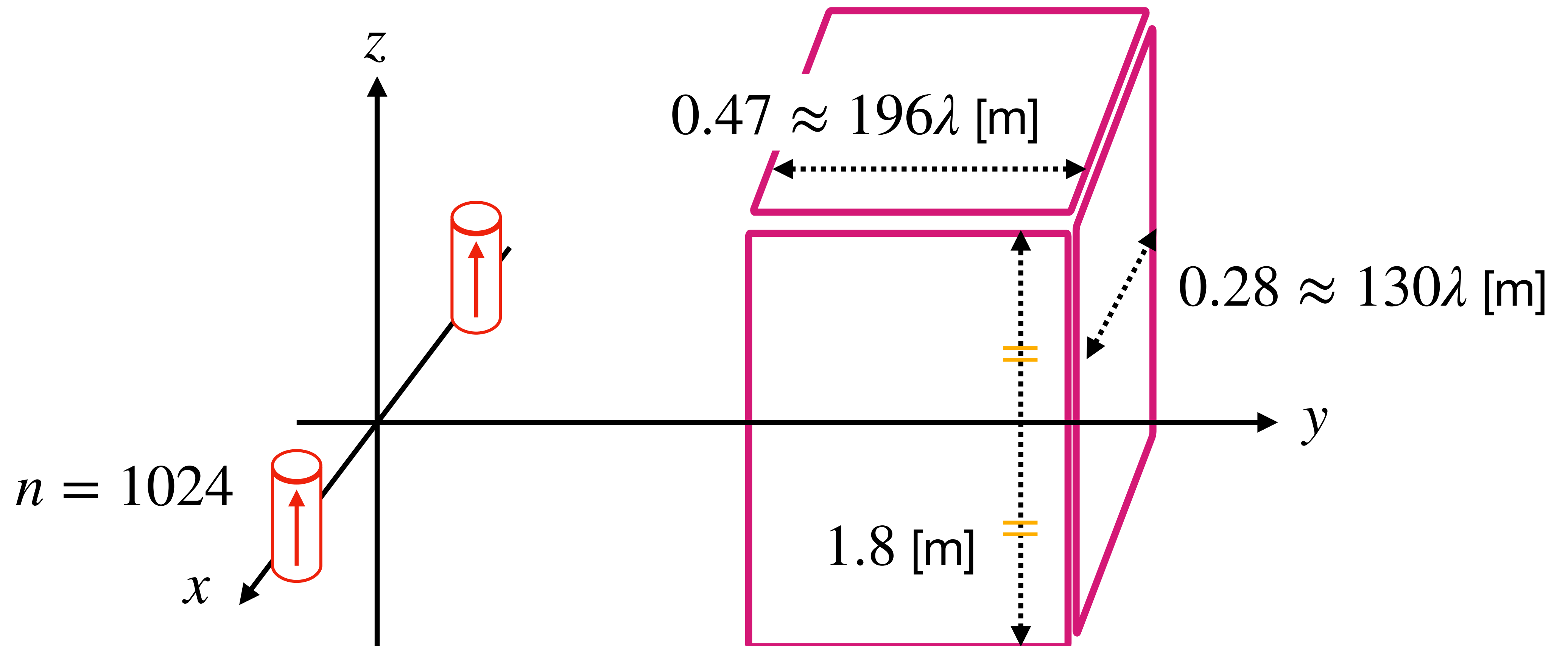


E-field along the desired direction



Numerical Results with Blockages

- The obstacle is modeled by a cuboid considering a human body.
- Assume a perfect electric conductor.
- The uniform theory of diffraction is used to evaluate the blockage effects.

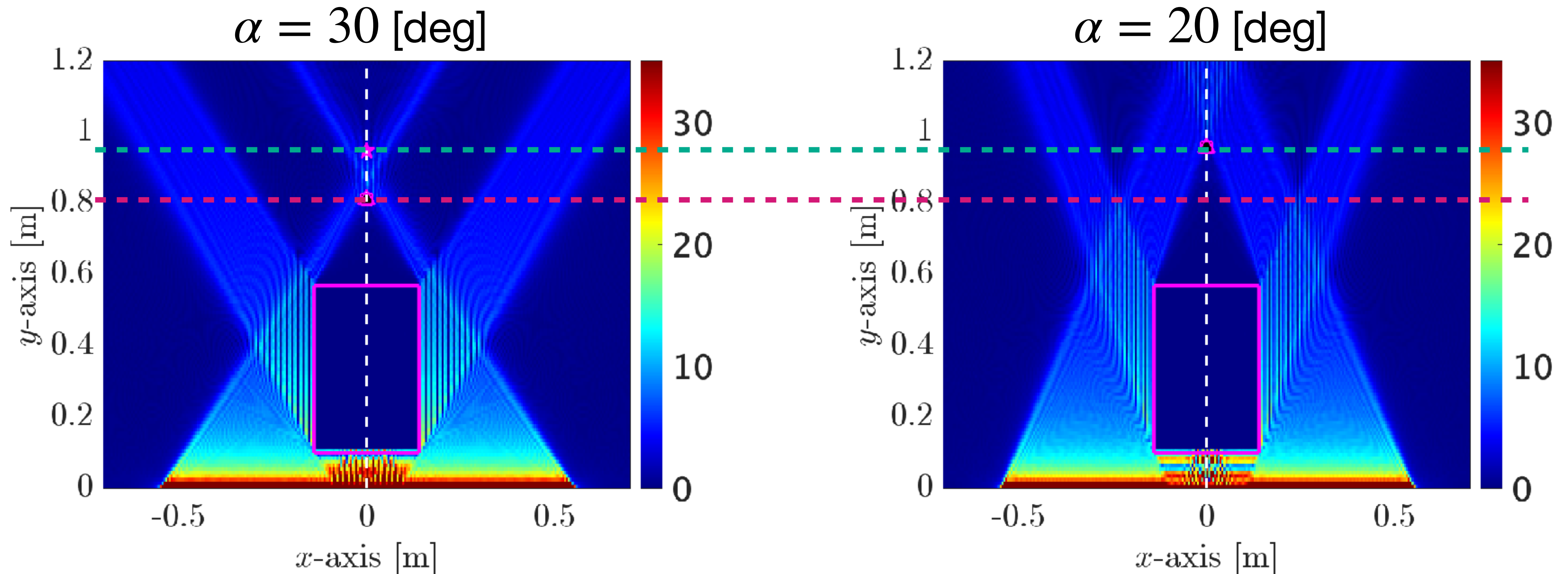


Self-Healing Capability of Bessel Beams

□ Consider non-steering cases.

● The larger α leads to the higher self-healing capability but shorter distance.

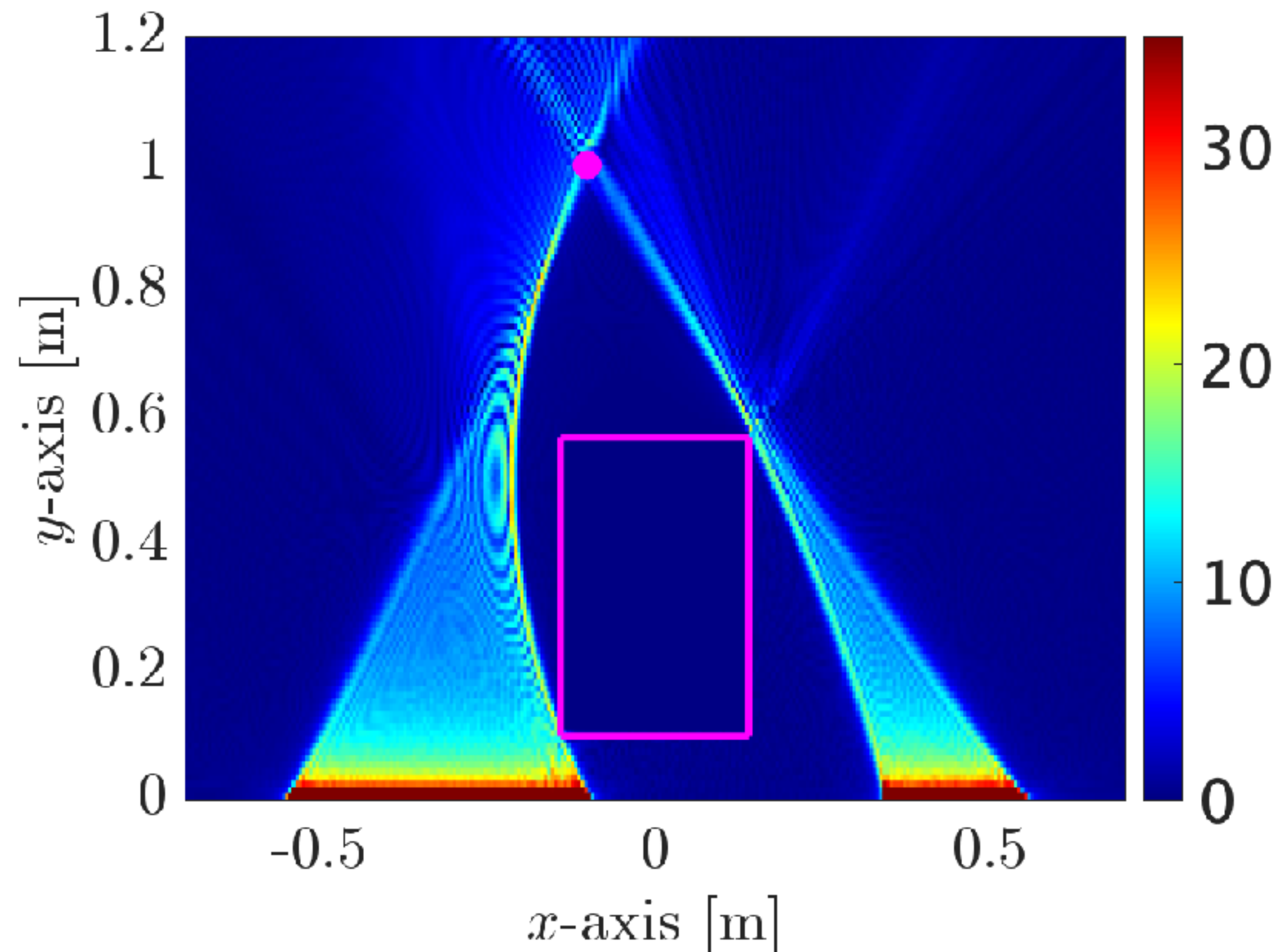
● The smaller α leads to the longer distance but lower self-healing capability.



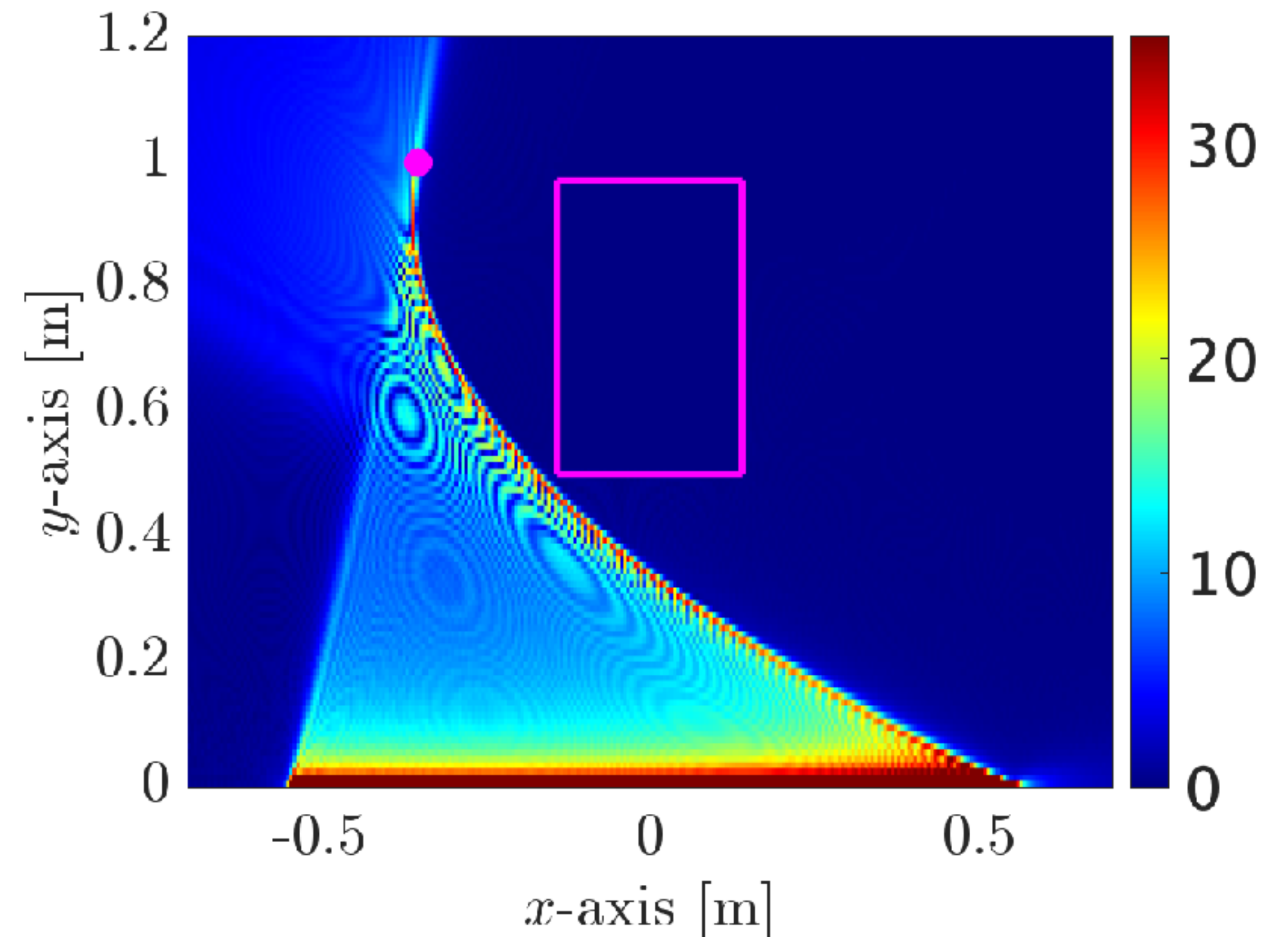
Blockage Avoidance of Curving Beams

- The proposed design achieves the parabolic trajectories based on the user position while avoiding one obstacle.

$$(x_u, y_u) = (-0.1, 1)$$



$$(x_u, y_u) = (-0.35, 1)$$



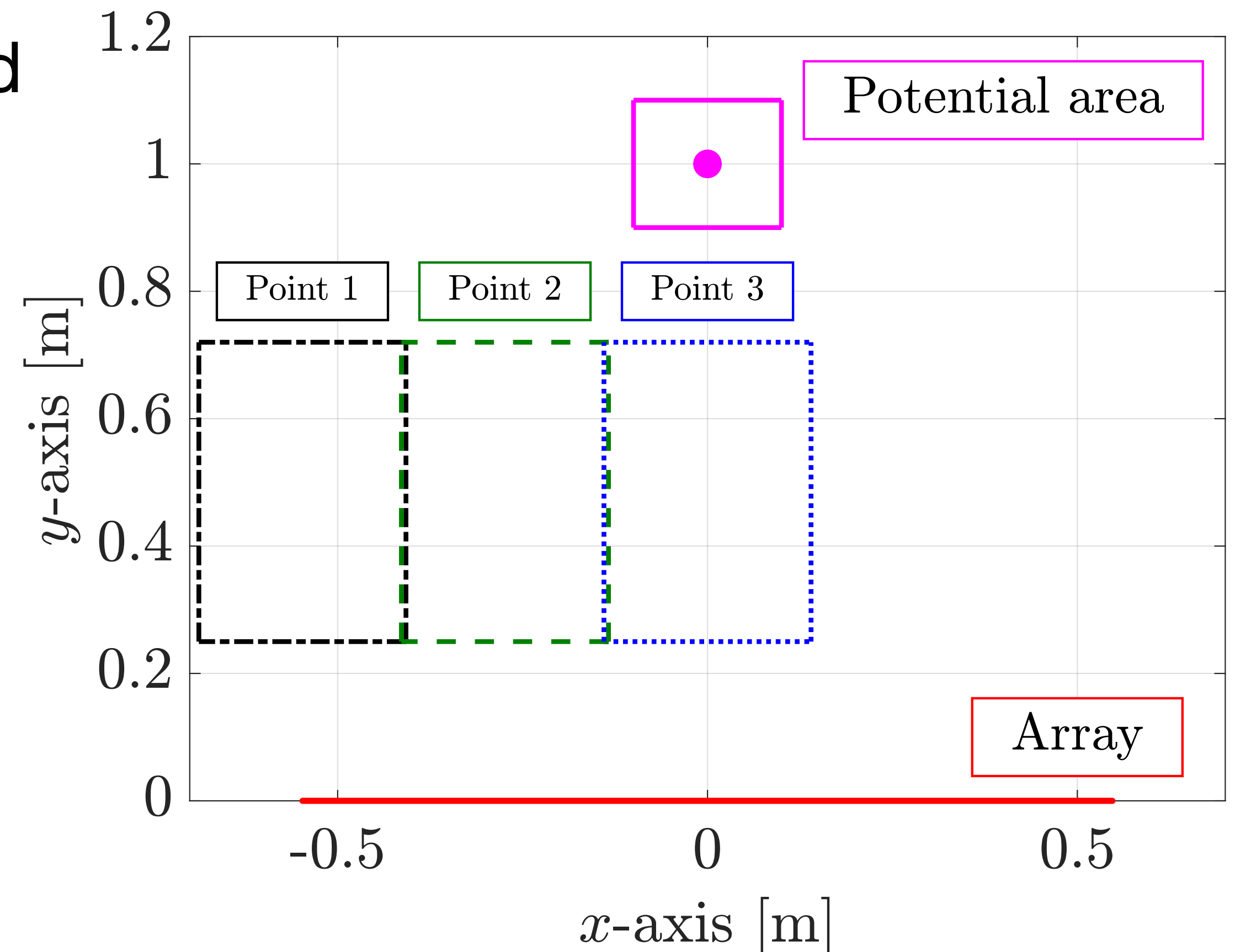
- The phase distribution of the other well-know beams;
- Gaussian beam: $\phi_n = -k \sin \theta_A x_{t,n}$
- Beamfocusing: $\phi_n = kr_n$ (r_n is the distance between the user and antenna)

Information used to generate beams with a ULA

	Gaussian beam	Beamfocusing	Bessel beam	Curving beam
User position		✓		✓
Azimuth angle	✓	-	✓	-
Obstacle position			△	✓

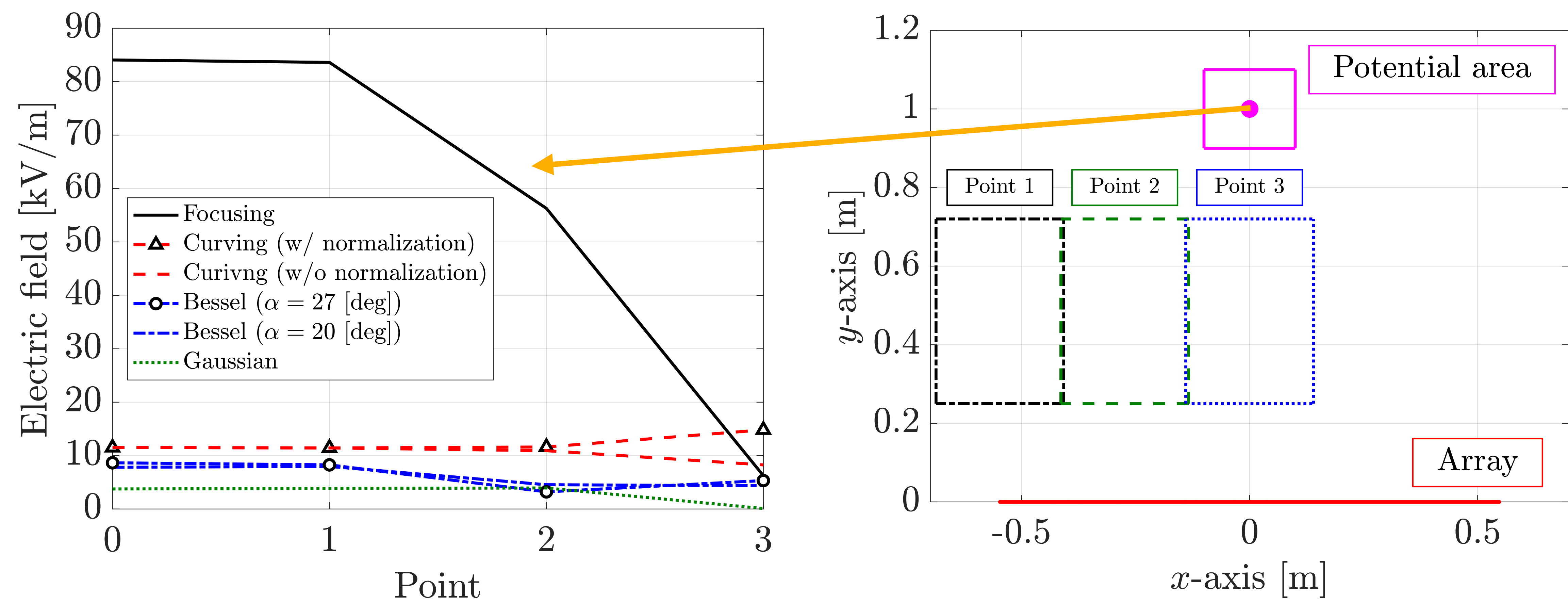
Communication Scenario

- The user position is set to $(x_u, y_u) = (0, 1)$.
- The potential area of the user in the presence of *positioning errors* is given by $x_u \in [-0.1, 0.1]$ and $y_u \in [0.9, 1.1]$
- Four points of the obstacle are considered
- Point 0 means no obstacle.



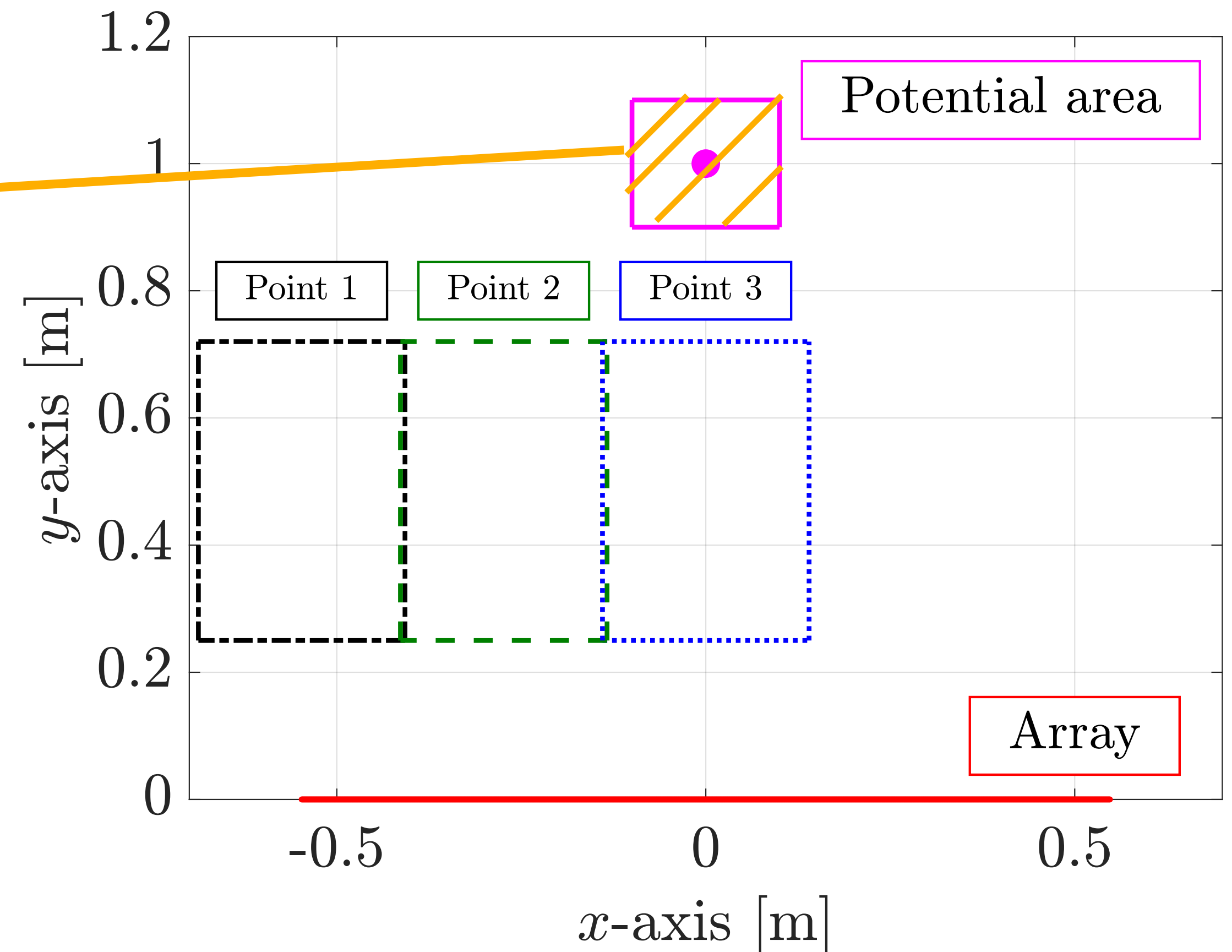
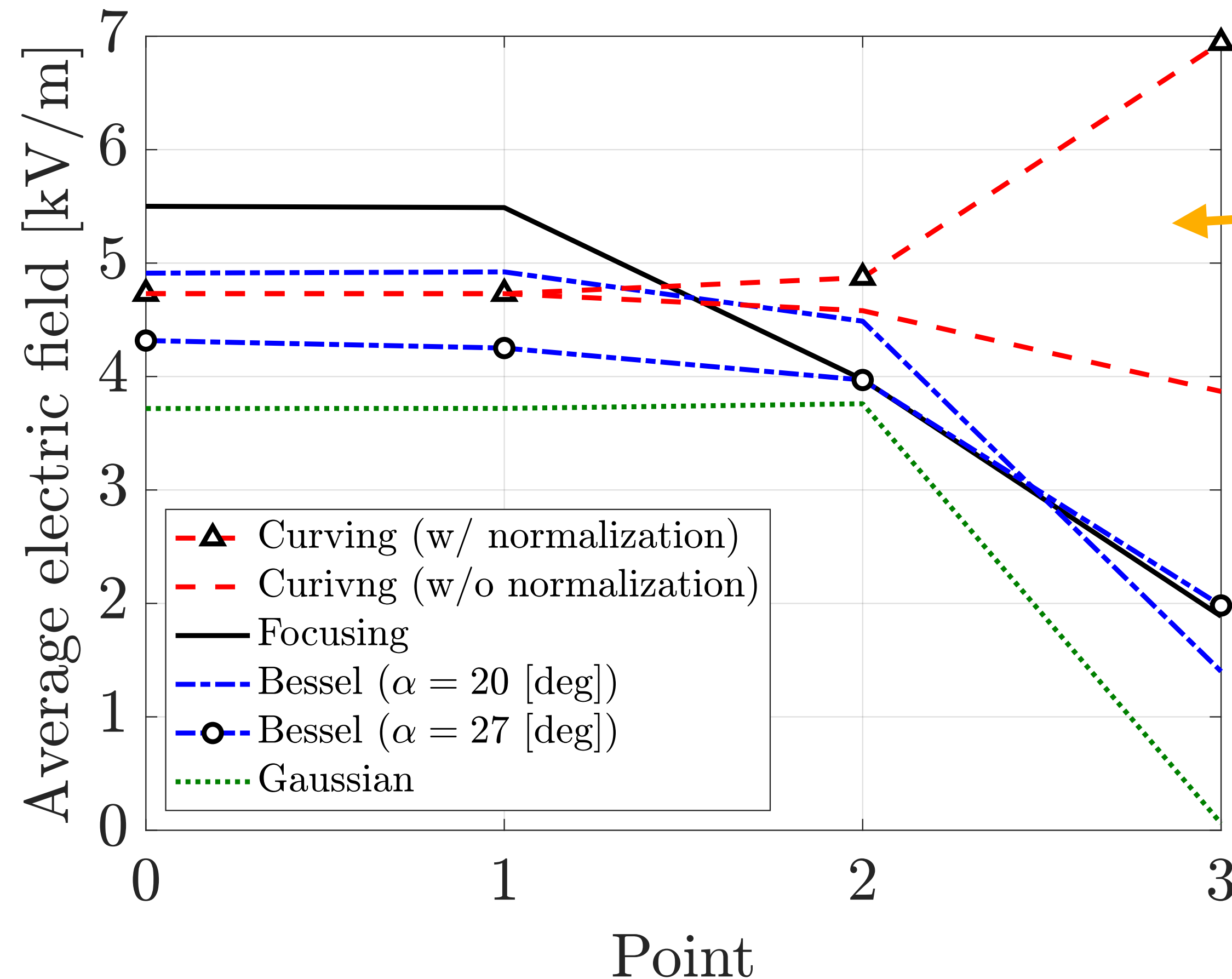
Amplitude of the Electric Field at the User Position

- The beamfocusing achieves the strongest intensity.
- Bessel and curving beams mitigate the blockage effects



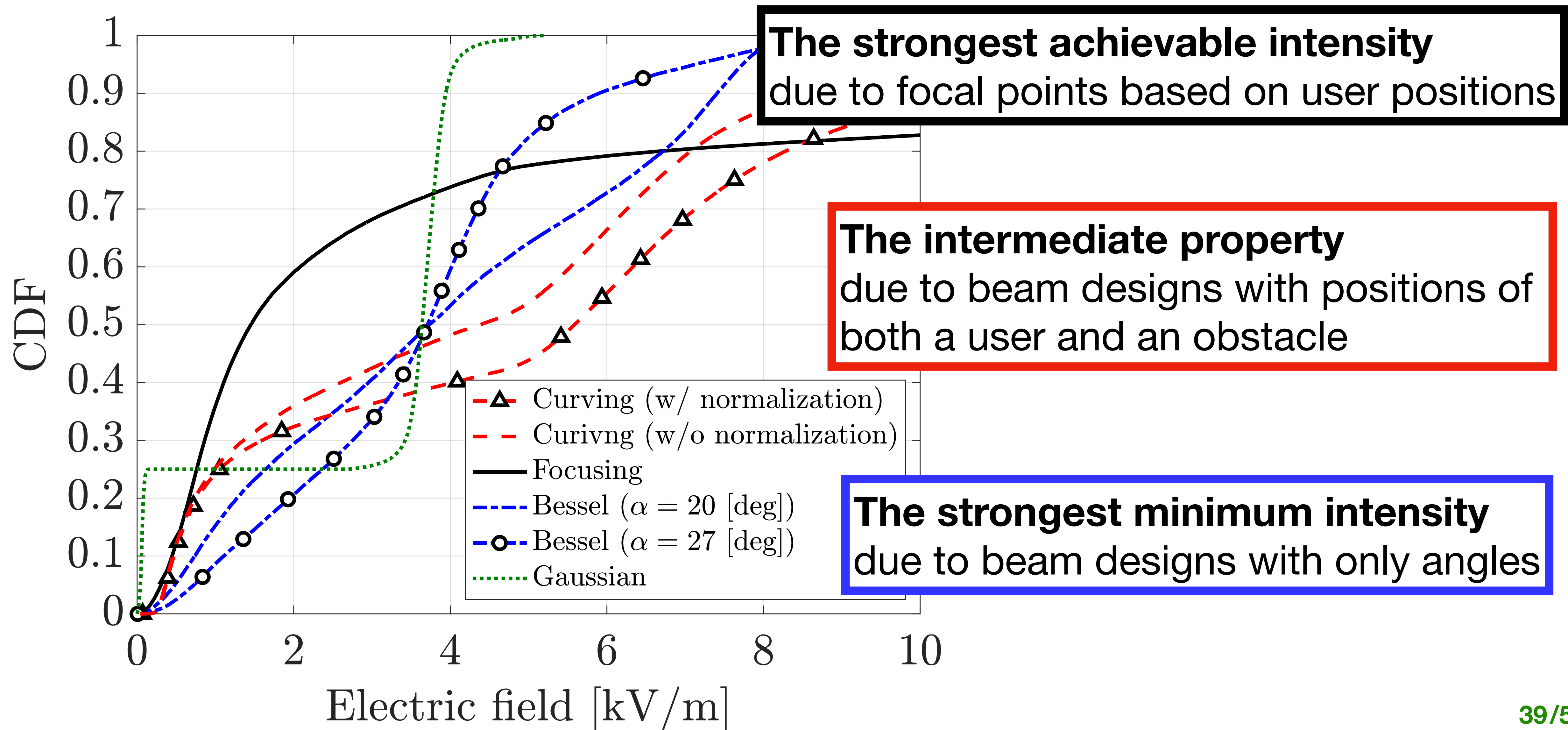
Amplitude of the Electric Field With Positioning Errors

- For beamfocusing, the average intensity is much lower than the maximum one.
- The proper choice of α of Bessel beams depends on the blockage effects.



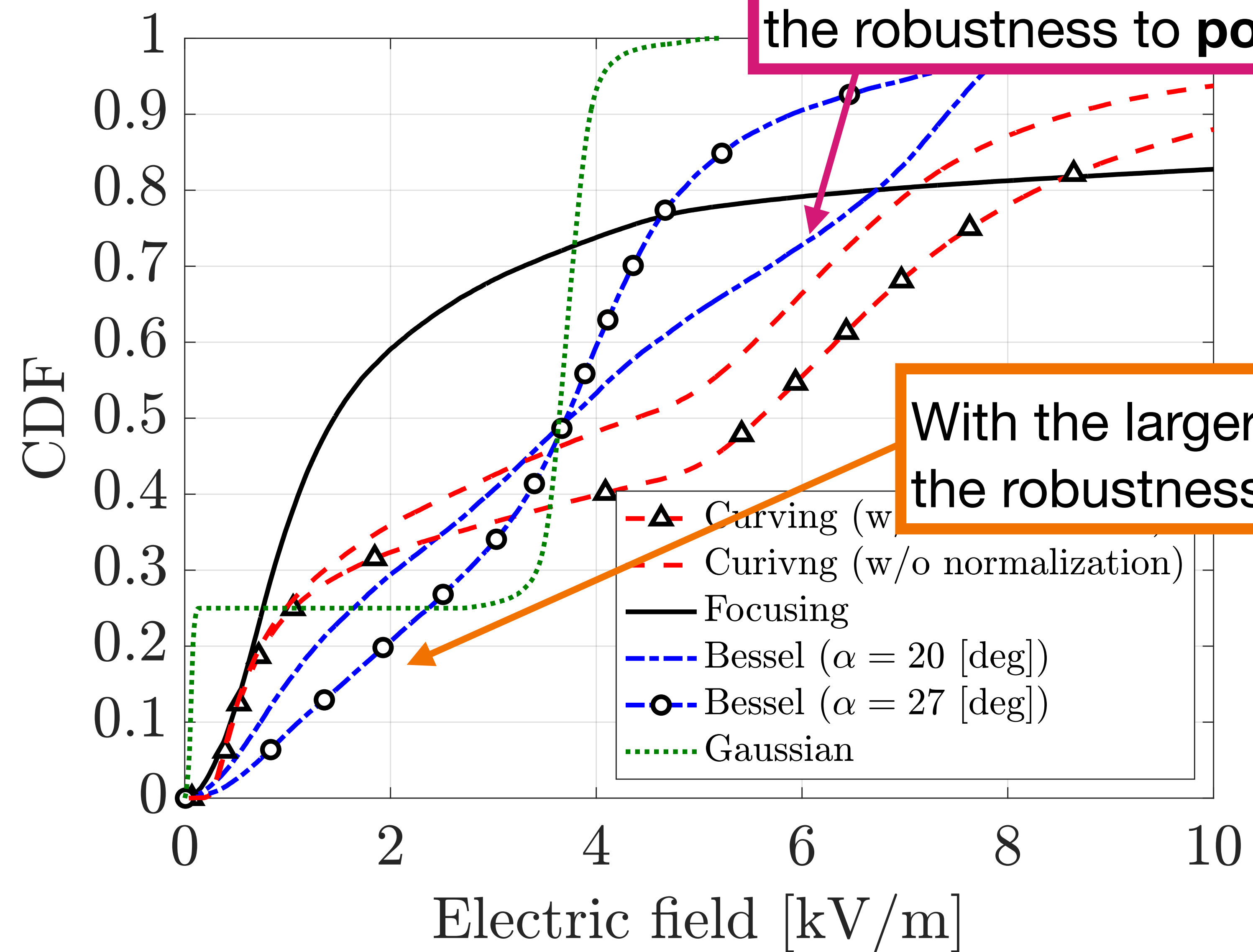
CDF of Amplitude of the Electric Field

□ Consider all the situations with positing errors.



CDF of Amplitude of the Electric Field

□ Focus on Bessel beams



With the smaller α (= 20 [deg]),
the robustness to **position errors** is improved.

With the larger α (= 27 [deg]),
the robustness **against blockages** is improved.

□ First part:

- Near-field beam generation using uniform linear array (ULA)
- Closed-form phase distributions of near-field beams
- Properties and conditions of Bessel beam generation



arXiv Paper

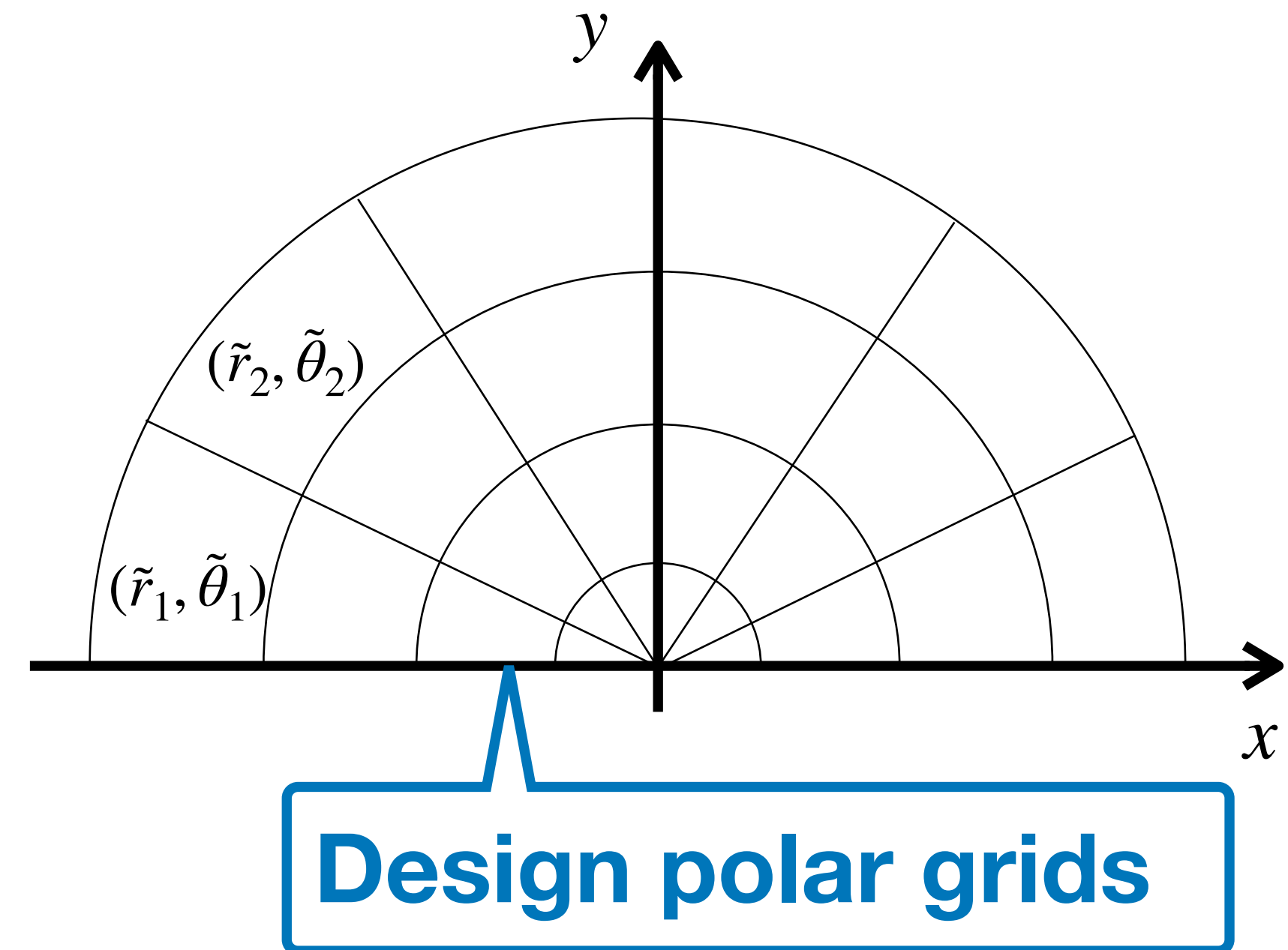
□ Second part:

- **Full-digital extremely-large (XL-) MIMO systems**
- **Joint channel and data estimation for multiuser XL-MIMO**



arXiv Paper

- **P-SOMP** [TC'22]
 - Consider near-field channel sparsity using **polar (angle-distance) grids**
 - Assume orthogonal pilot (leads to large pilot overhead in XL-MIMO)
- **2D-CoSaMP** [TC'24], **2-Stage-2D-SOMP** [SP'24]
 - Use non-orthogonal pilots to reduce pilot overhead
 - **Data detection performance is limited** compared to perfect CSI due to non-orthogonality of pilots



[TC'22] M. Cui and L. Dai, IEEE Trans. Commun., 2022.

[SP'24] K. Arai, et.al., in Proc. IEEE SPAWC, 2024.

[TC'24] X. Xie, et.al., IEEE Trans. Commun., 2024.

□ Purpose of this study

- Accurate data detection and near-field channel estimation for multiuser XL-MIMO systems with small pilot overhead

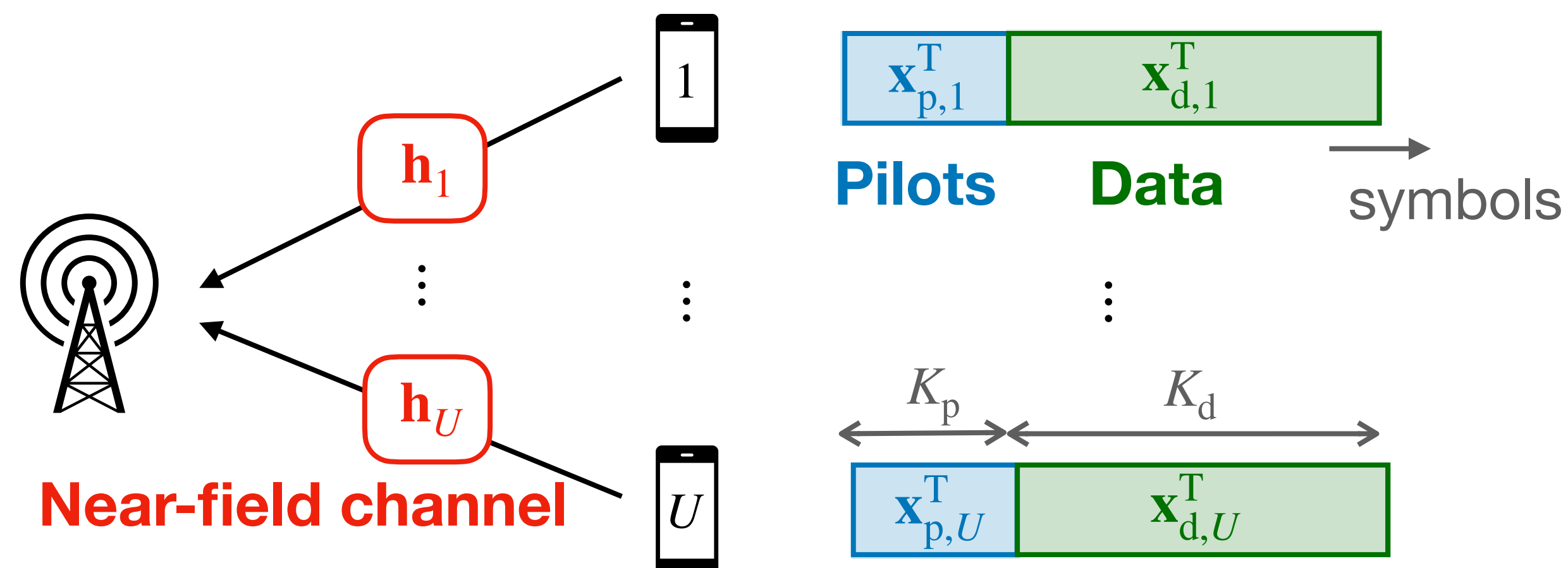
□ Contribution

- **JCDE (Joint channel and data estimation) algorithm** based on EP and EM
 - ▶ leverages polar sparsity by Bayesian inference with deterministic approach
 - ▶ leverages channel correlation by sub-array-wise LMMSE-based filter

EP : Expectation propagation

EM : Expectation maximization

System Model (Uplink Multiuser XL-MIMO)



Num. of antennas : N

Num. of UEs : U

Length of pilots : K_p

Length of data : K_d

Received signal : \mathbf{Y} Channel : \mathbf{H} Tx signals : $\mathbf{X} = [\mathbf{X}_p, \mathbf{X}_d]$

$$\begin{array}{c}
 \begin{array}{|c|c|}
 \hline
 \mathbf{Y}_p & \mathbf{Y}_d \\
 \hline
 \end{array}
 \end{array}
 =
 \begin{array}{c}
 \begin{array}{|c|c|c|c|}
 \hline
 \mathbf{h}_1 & \mathbf{h}_2 & \dots & \mathbf{h}_U \\
 \hline
 \end{array}
 \end{array}
 \begin{array}{c}
 \begin{array}{|c|c|}
 \hline
 \mathbf{x}_{p,1}^T & \mathbf{x}_{d,1}^T \\
 \mathbf{x}_{p,2}^T & \mathbf{x}_{d,2}^T \\
 \vdots & \vdots \\
 \mathbf{x}_{p,U}^T & \mathbf{x}_{d,U}^T \\
 \hline
 \end{array}
 \end{array}
 + \mathbf{N} \text{ (Noise)}$$

The dimensions of the matrices are indicated by arrows: \mathbf{Y} is $N \times (K_p + K_d)$, \mathbf{H} is $N \times U$, and \mathbf{X} is $(K_p + K_d) \times U$.

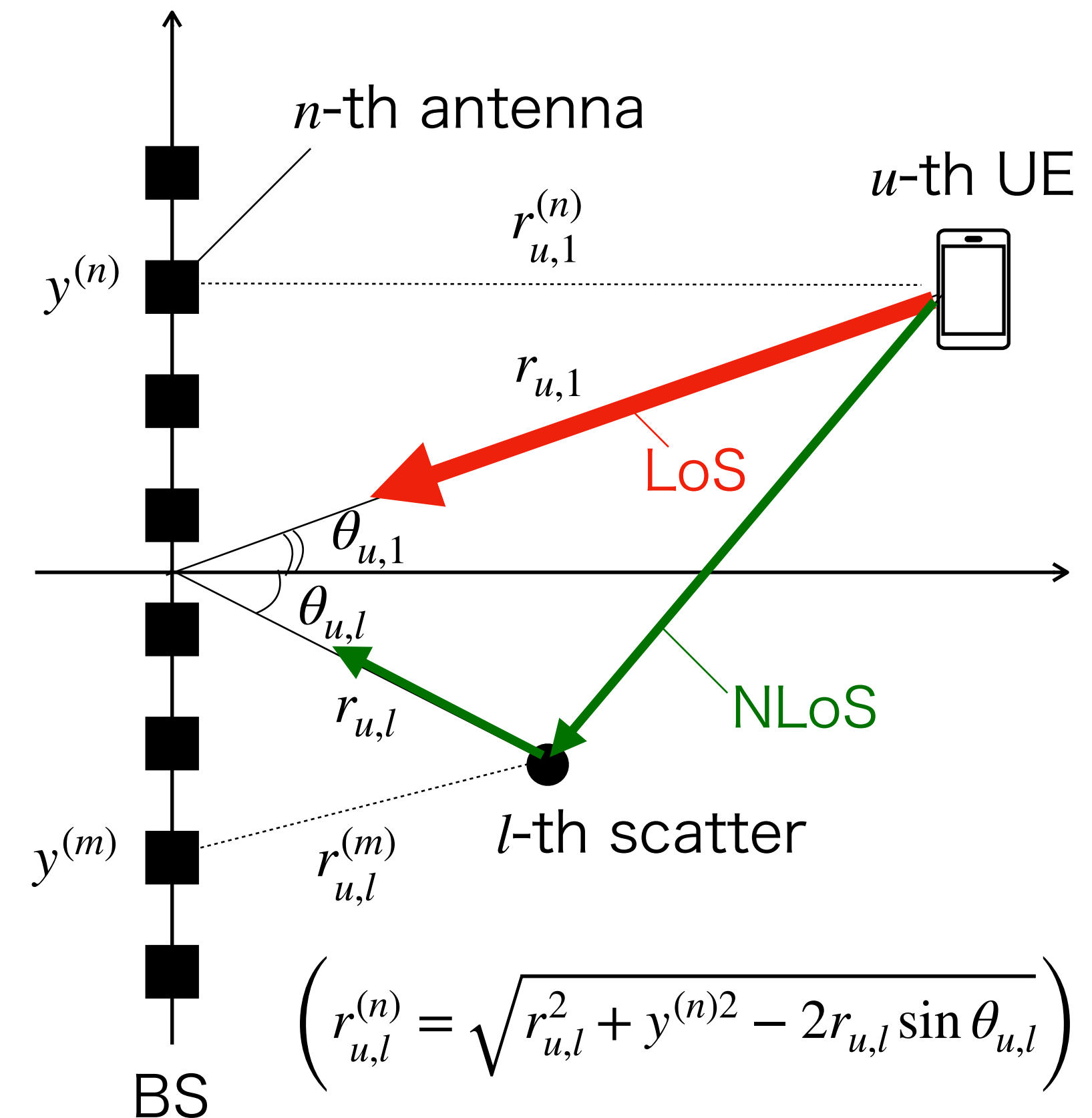
Purpose : Estimate channel \mathbf{H} and data \mathbf{X}_d with pilot \mathbf{X}_p

- Near-field channel vector

$$\mathbf{h}_u = \underbrace{\begin{bmatrix} \mathbf{a}(\theta_{u,1}, r_{u,1}) & \dots & \mathbf{a}(\theta_{u,L}, r_{u,L}) \end{bmatrix}}_{\mathbf{A}(\boldsymbol{\theta}_u, \mathbf{r}_u) \in \mathbb{C}^{N \times L} \text{ (Array response)}} \underbrace{\begin{bmatrix} \mathbf{z}_{u,1} \\ \vdots \\ \mathbf{z}_{u,L} \end{bmatrix}}_{\mathbf{z}_u \in \mathbb{C}^{L \times 1} \text{ (Path gain)}} = \mathbf{A}(\boldsymbol{\theta}_u, \mathbf{r}_u) \mathbf{z}_u$$

L_u paths

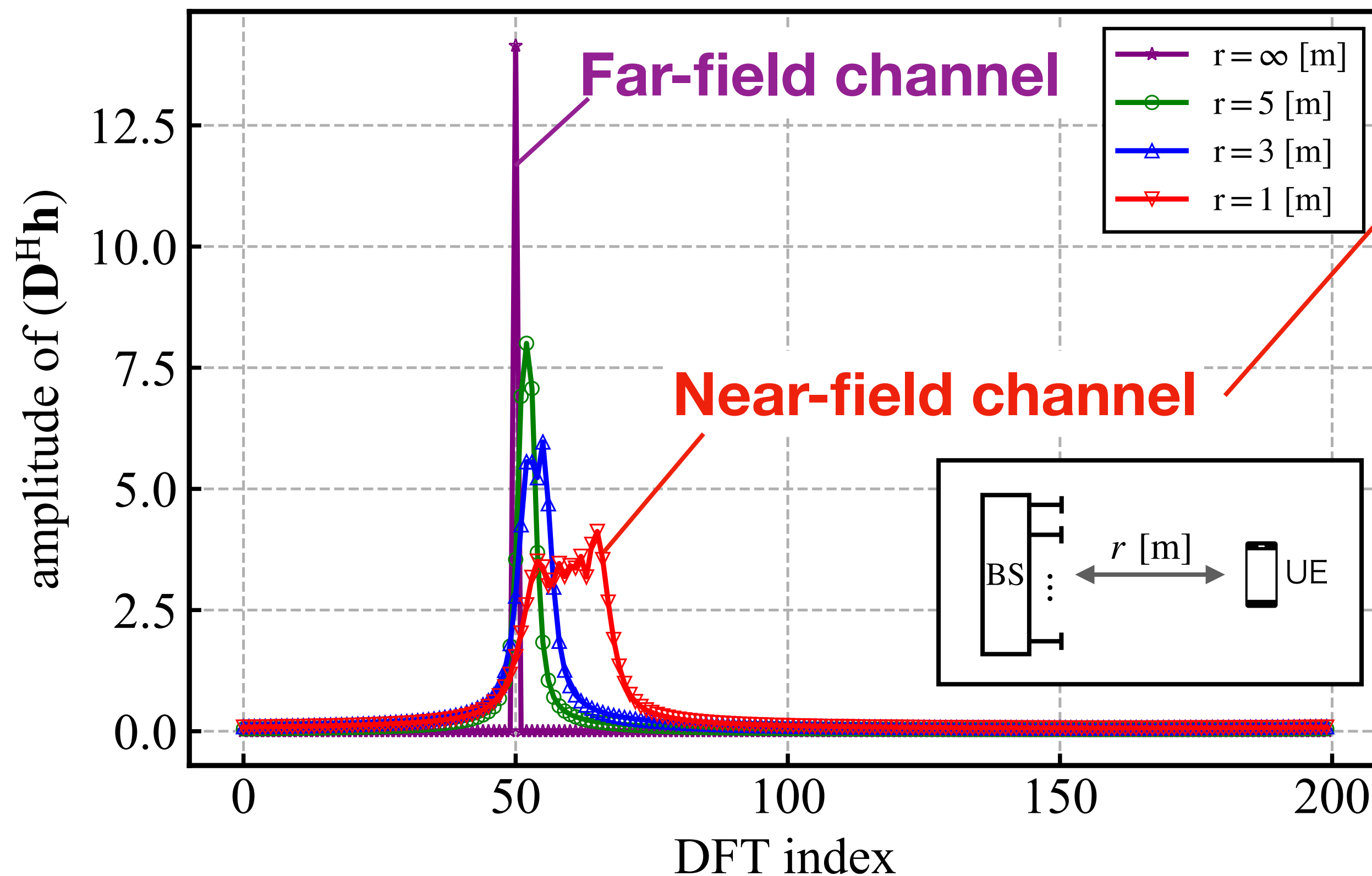
$$[\mathbf{a}(\theta_{u,l}, \underline{r_{u,l}})]_n = \exp \left[-j \frac{2\pi}{\lambda} \left(r_{u,l}^{(n)} - r_{u,l} \right) \right]$$



Array response depends on distance r

To exploit channel sparsity, transform \mathbf{H} and \mathbf{Y} using DFT matrix $\mathbf{D}_N \in \mathbb{C}^{N \times N}$

$$\mathbf{H} \leftarrow \mathbf{D}_N^H \mathbf{H}, \quad \mathbf{Y} \leftarrow \mathbf{D}_N^H \mathbf{Y}$$



**Cluster sparsity
due to energy leakage**

\Rightarrow Cannot use conventional channel estimation method [JSAC'17] relying on the **far-field assumption**

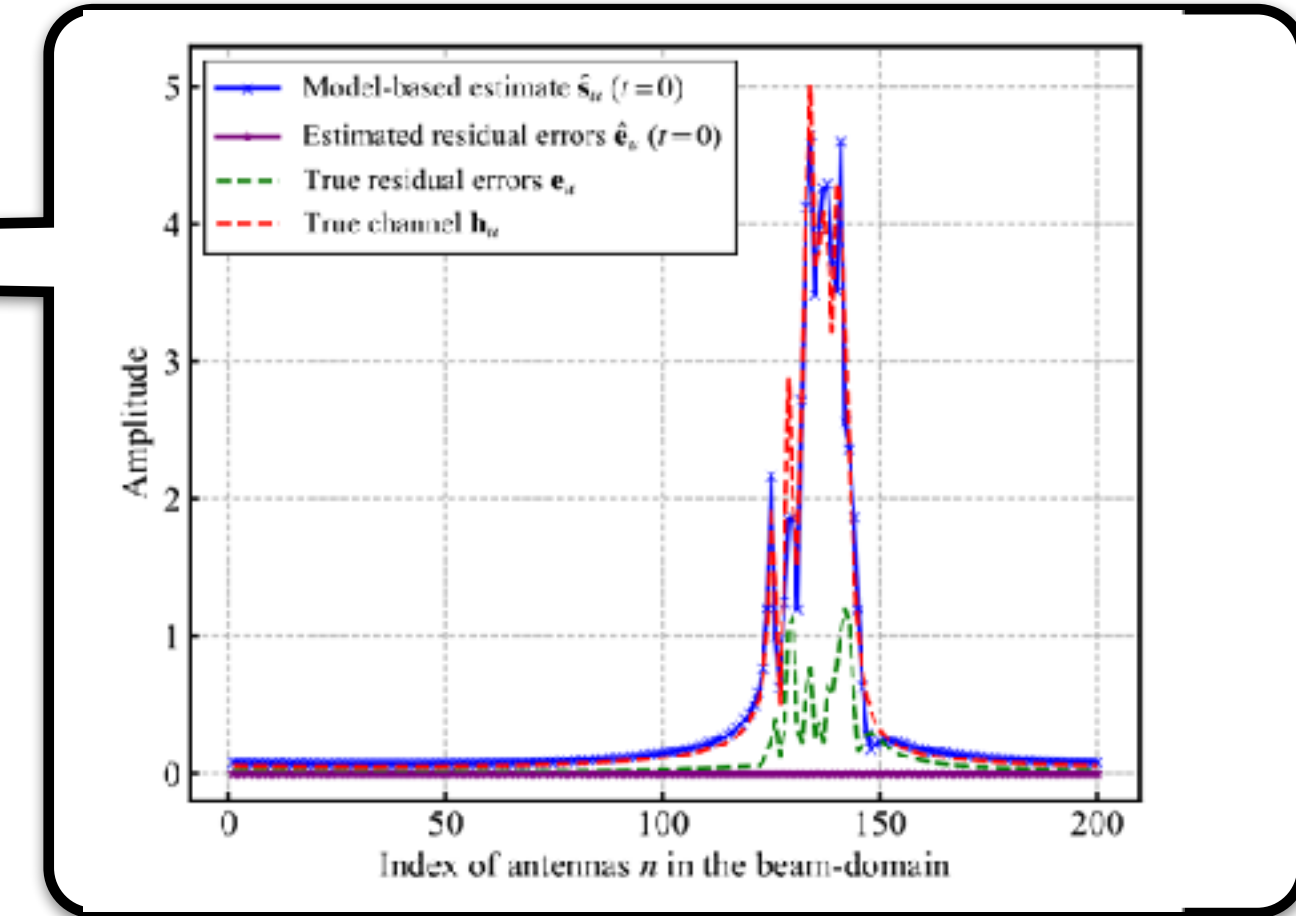
$N = 200, f_c = 100$ [GHz], antenna aperture 0.3m,
Fraunhofer distance 59.4m

To tackle energy leakage effects, decompose \mathbf{H} into $\hat{\mathbf{S}} \in \mathbb{C}^{N \times U}$ and $\mathbf{E} \in \mathbb{C}^{N \times U}$

$$\mathbf{H} = \hat{\mathbf{S}} + \mathbf{E}$$

\mathbf{E} : Residual error \leftarrow As a random variable

$\hat{\mathbf{S}}$: Model-based estimate \leftarrow As a deterministic variable



$$\left(\begin{array}{ll} \hat{\mathbf{s}}_u = \mathbf{A}(\hat{\boldsymbol{\theta}}_u, \hat{\mathbf{r}}_u) \hat{\mathbf{z}}_u & \mathbf{A}(\hat{\boldsymbol{\theta}}_u, \hat{\mathbf{r}}_u) : \text{estimated array response} \\ & \hat{\mathbf{z}}_u : \text{estimated path gain} \end{array} \right)$$

Estimate $\left\{ \begin{array}{l} \mathbf{E} \text{ by } \mathbf{Bayesian Inference} \text{ with a sparse prior} \\ \hat{\mathbf{S}} \text{ by a } \mathbf{deterministic} \text{ approach exploiting near-field structures} \end{array} \right.$

Update Model-Based Estimate $\hat{\mathbf{S}}$

- Sparse reconstruction relying on the **near-field structures**

$$\underset{\tilde{\mathbf{z}}_u}{\text{minimize}} \quad \left\| \underline{\hat{\mathbf{h}}_u} - \underline{\hat{\mathbf{s}}_u} \right\|_2^2$$

$\hat{\mathbf{h}}_u$: Tentative estimate using \mathbf{E} and the previous $\hat{\mathbf{S}}$

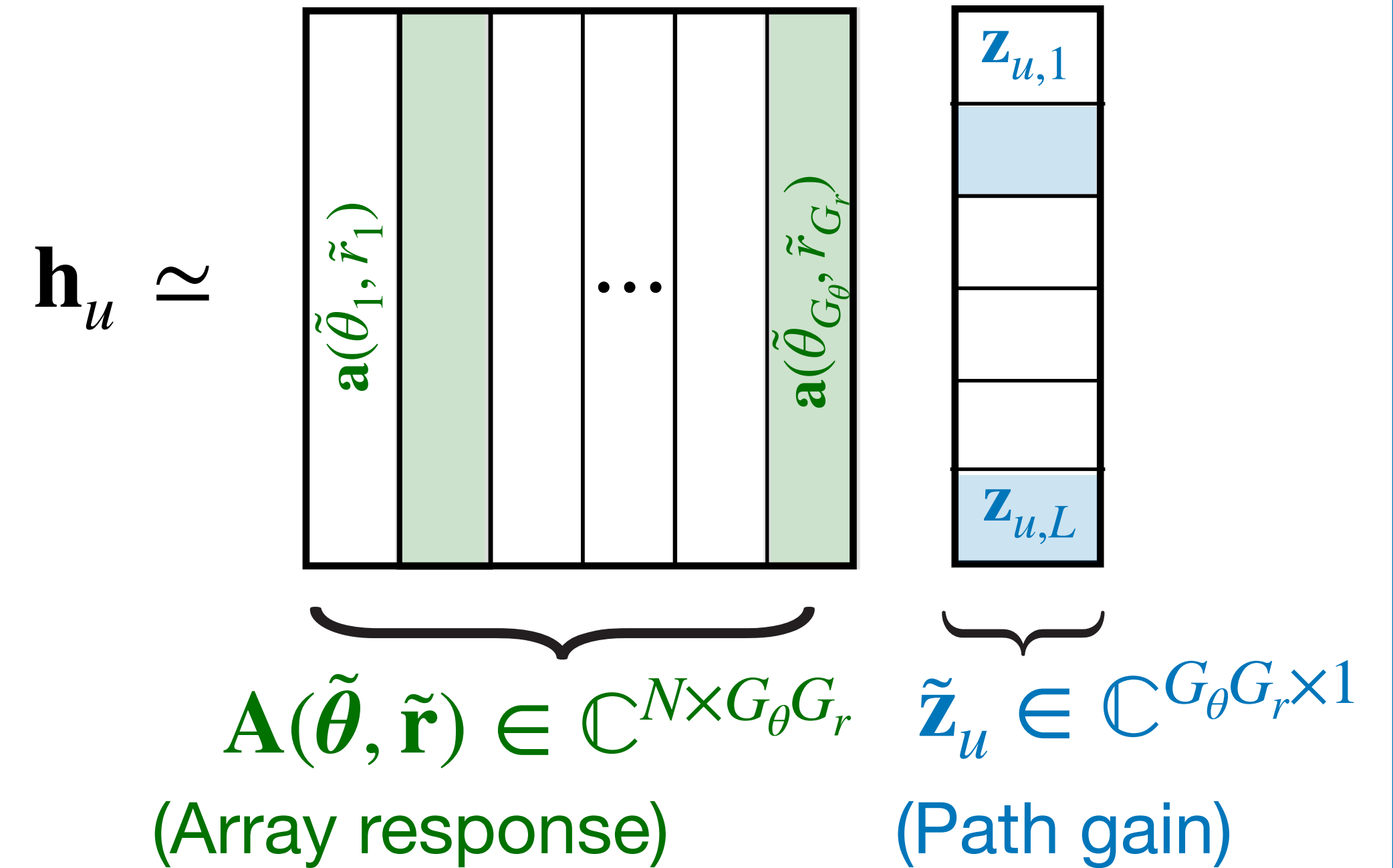
$\hat{\mathbf{s}}_u$: Model-based estimate

$$\text{subject to} \quad \underline{\hat{\mathbf{s}}_u} = \mathbf{A}(\tilde{\boldsymbol{\theta}}, \tilde{\mathbf{r}}) \tilde{\mathbf{z}}_u$$

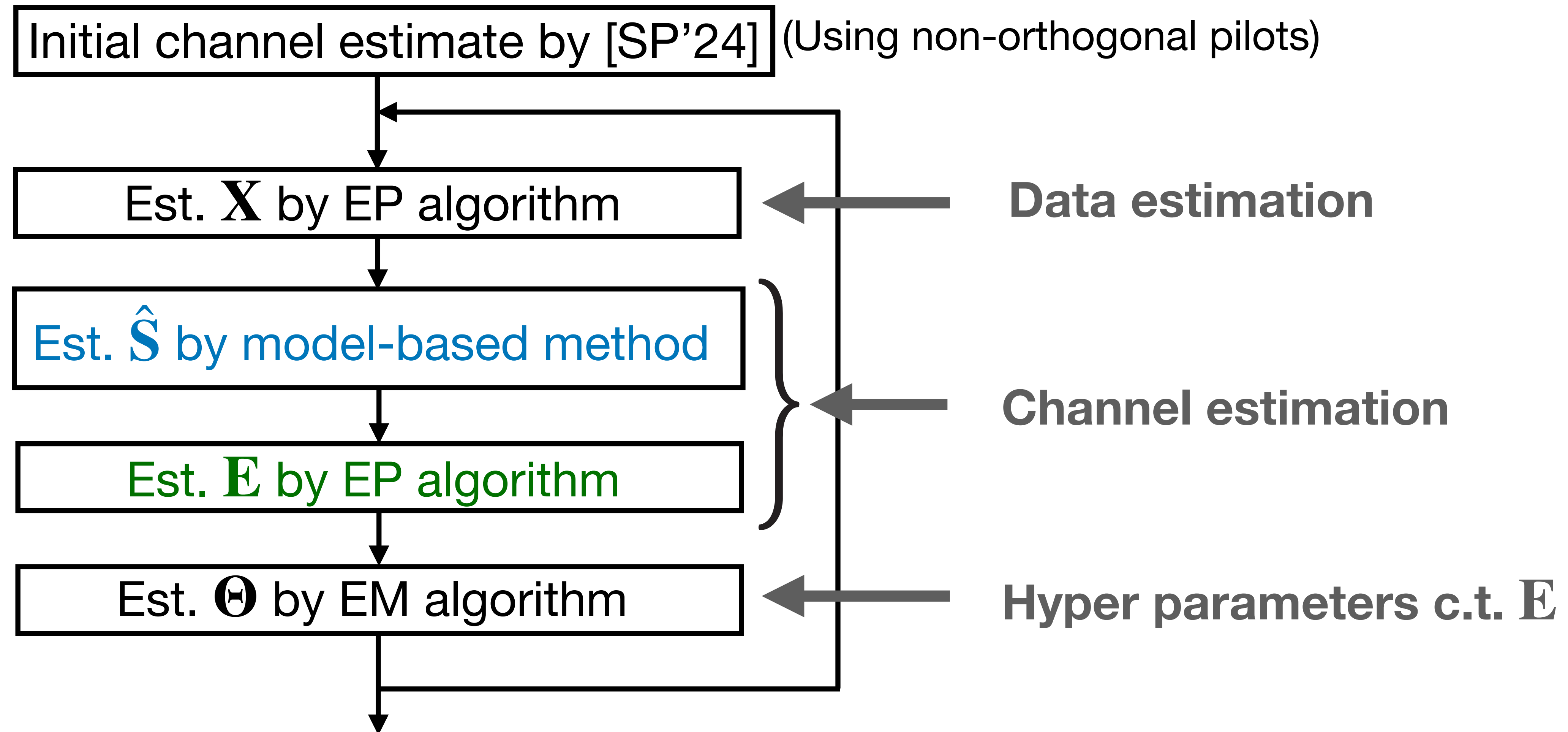
$$\left\| \tilde{\mathbf{z}}_u \right\|_0 = \hat{L}_u$$

- $$\left(\begin{array}{l} \bullet \tilde{\boldsymbol{\theta}} \in \mathbb{R}^{G_\theta \times 1} : \text{candidate AoAs} \\ \bullet \tilde{\mathbf{r}} \in \mathbb{R}^{G_r \times 1} : \text{candidate distances} \end{array} \right)$$

Virtual array approximation



Proposed JCDE Algorithm



Alternately estimate data and channel in iterations

System parameters

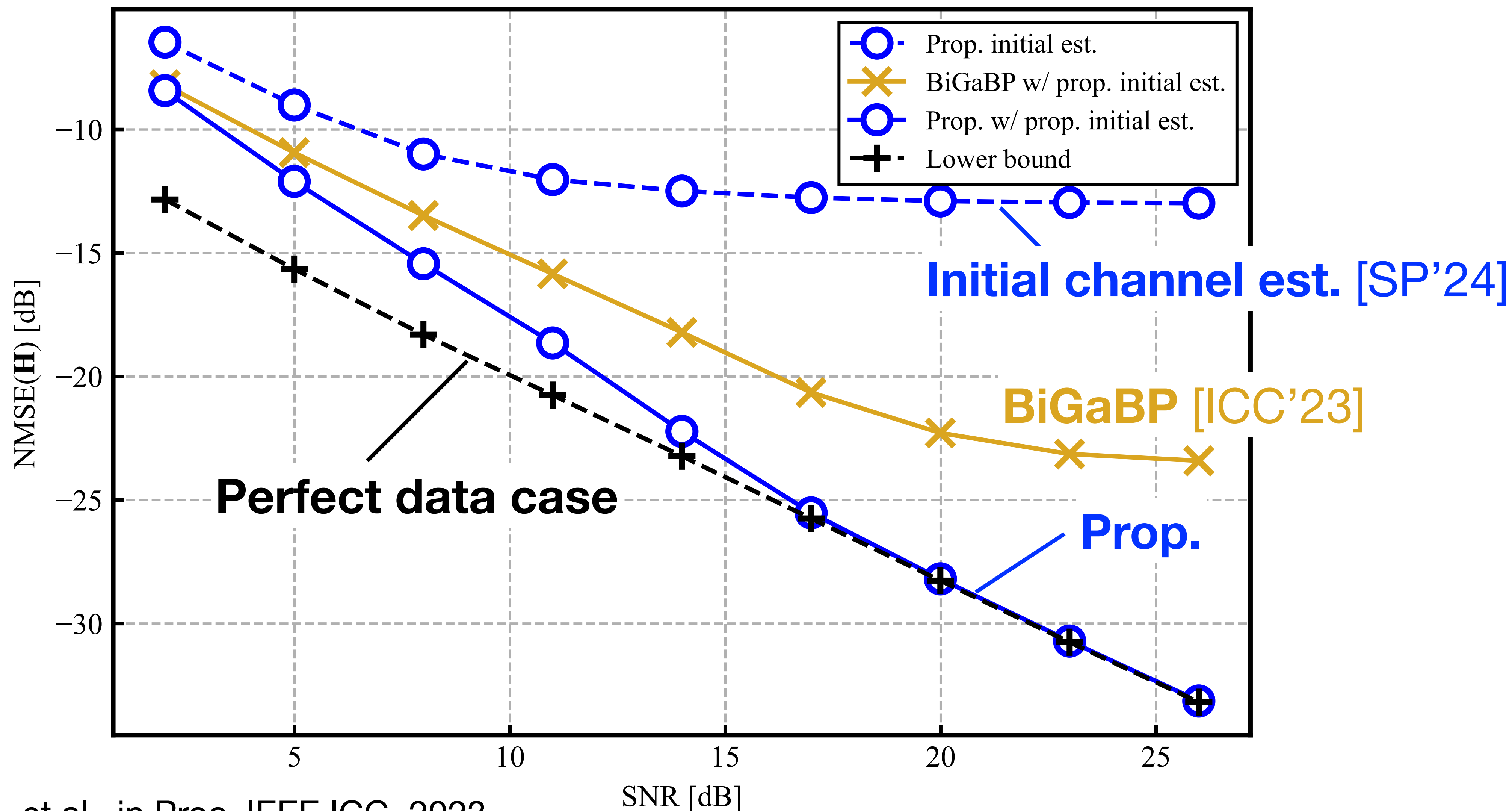
- $N = 200$ (Num. of antennas)
- $U = 50$ (Num. of UEs)
- $K_p = 25$ (Num. of pilots)
 - SIDCO frame [VTC'18] (50×25)
- $K_d = 100$ (Num. of data)
- $Q = 64$ (64QAM)
- $C = 4$ (Num. of sub-arrays)

Channel parameters

- $L_u = 3$ (Num. of paths per UE)
- $K = 10$ dB (K-factor)
- $\theta_l \sim \mathcal{U}(-60^\circ, 60^\circ)$ (Angle of arrival)
- $r_l \sim \mathcal{U}(1, 10)$ m (Distance)
- $G_\theta = 395$, $G_r = 7$ (Num. of grids)
- $f_c = 100$ GHz
- antenna aperture 0.3 m
- Fraunhofer distance 59.4 m

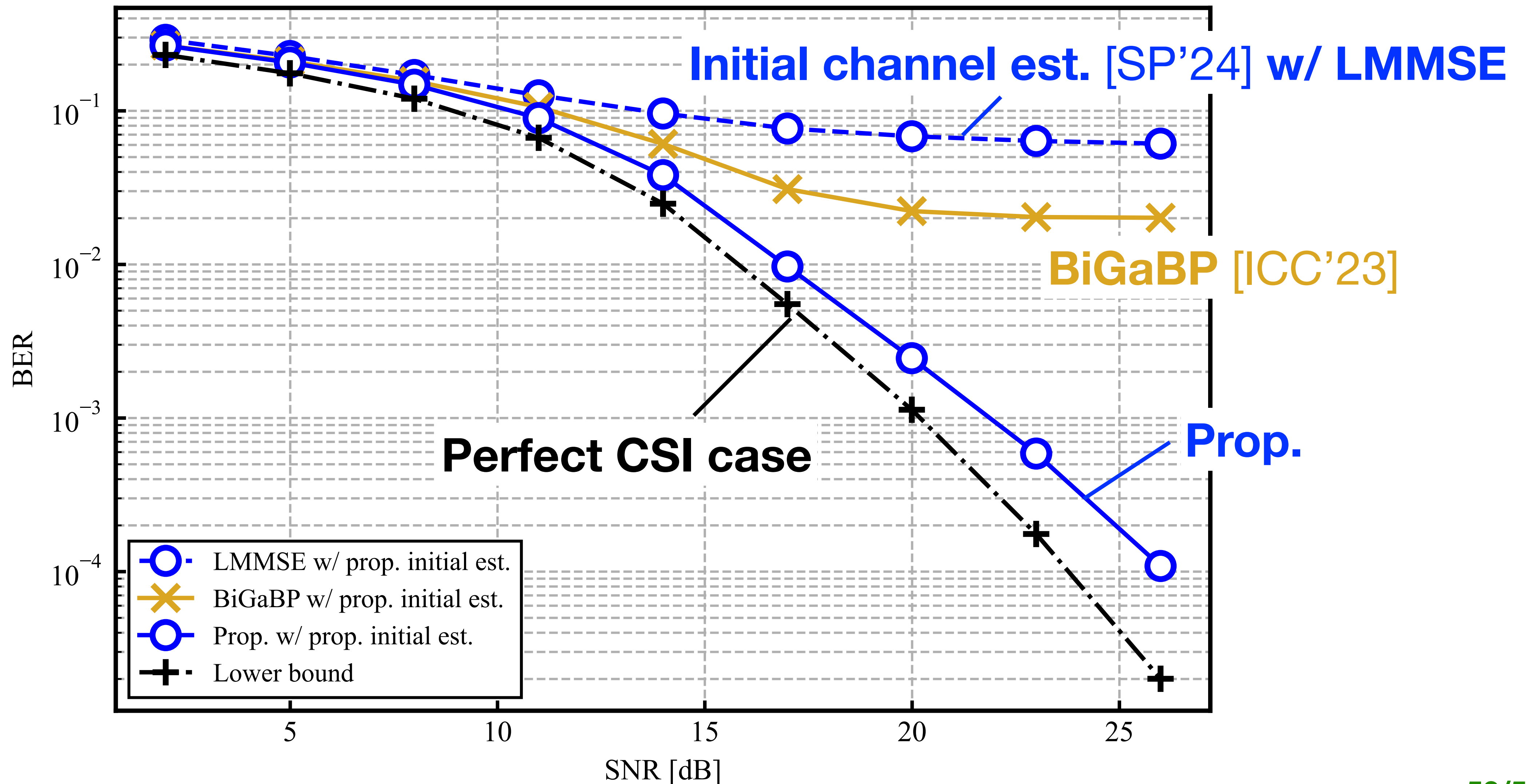
NMSE vs. SNR

- $N = 200, U = 50, K_p = 25, K_d = 100, Q = 64, C = 4$



BER vs. SNR

- $N = 200, U = 50, K_p = 25, K_d = 100, Q = 64, C = 4$



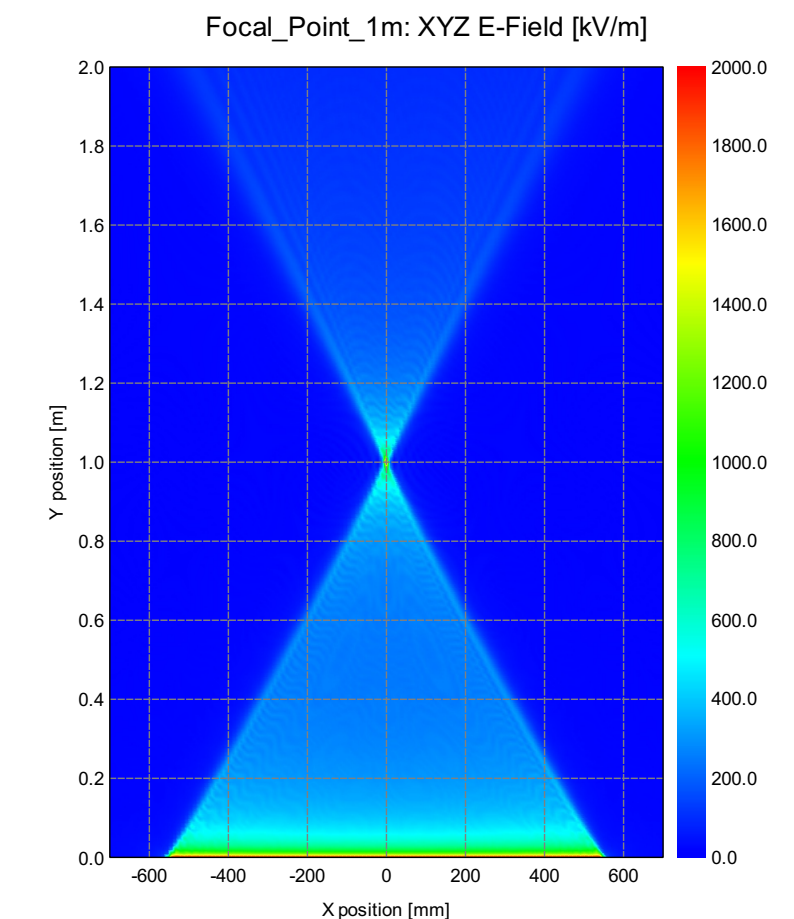
Conclusions and Takeaways

□ In this talk

- Near-field beam generation using uniform linear array (ULA)
- Joint channel and data estimation for multiuser XL-MIMO

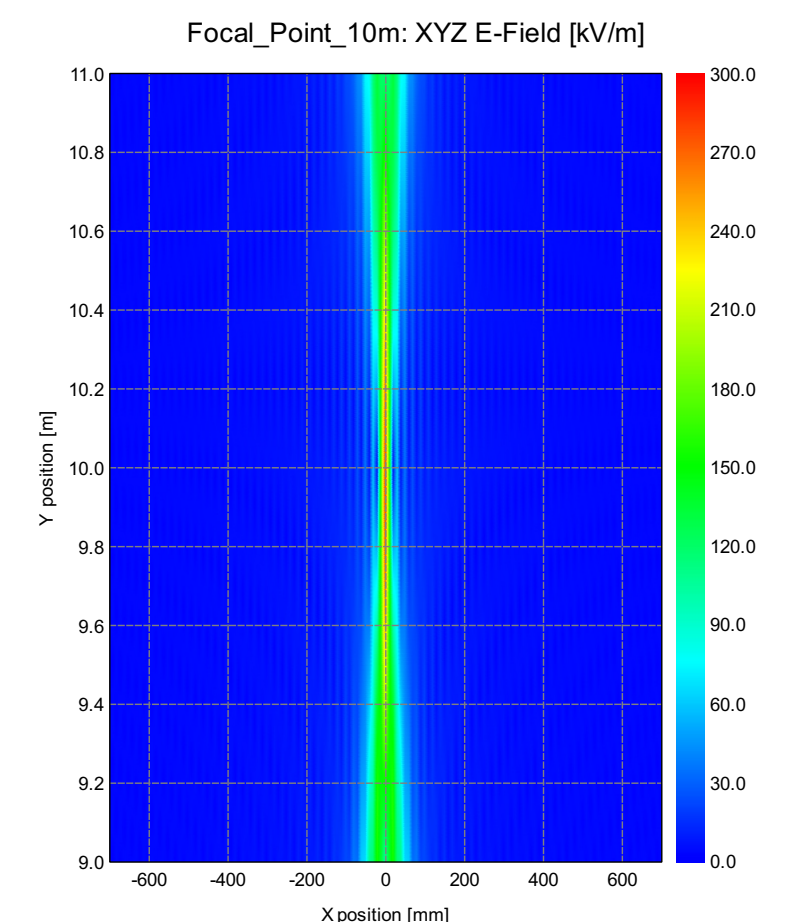
□ Beam with full CSI vs Beam with partial CSI

- Obtaining full CSI is computationally demanding
- Practical limitation to RF chains and focusing gain [WCL'24]
 - ▶ *Focal point blurs* even at 10m despite a 1 km Rayleigh distance
- Possibility of new design for near-field communications



Near field bof structure (Frequency = 140 GHz; Z position = 0 m) - Point_1m

1m



Near field bof structure (Frequency = 140 GHz; Z position = 0 m) - Point_10m

10m