

*3-4.Oct. 2012, Nordic Seminar*

# **Evaluation of material deterioration of rails subjected to rolling contact fatigue using x-ray diffraction**

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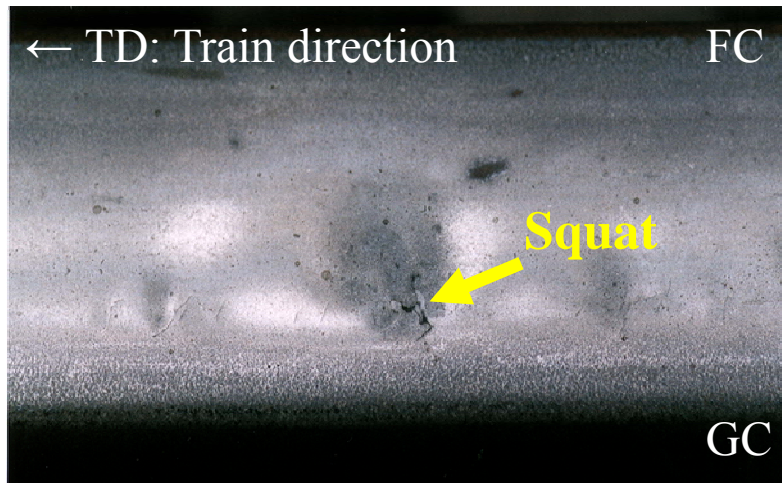
*Railway Technical Research Institute*

# Overview

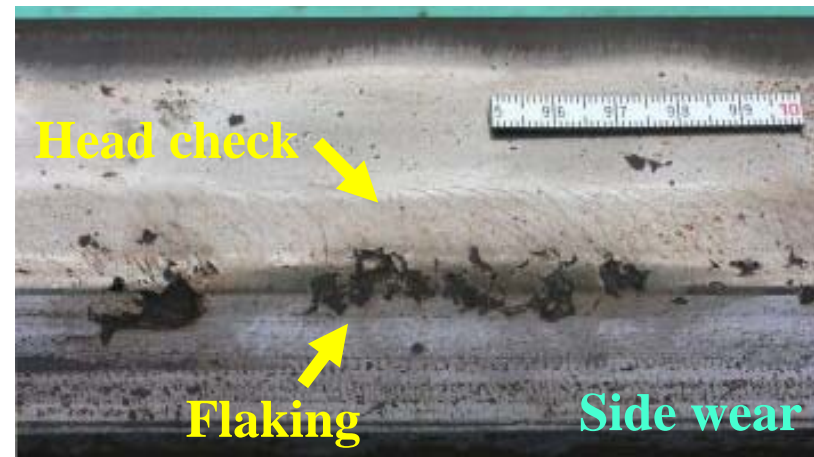
- 1) Background**
- 2) Purpose of this work**
- 3) Experimental**
- 4) Results of x-ray examinations**
- 5) Conclusions**



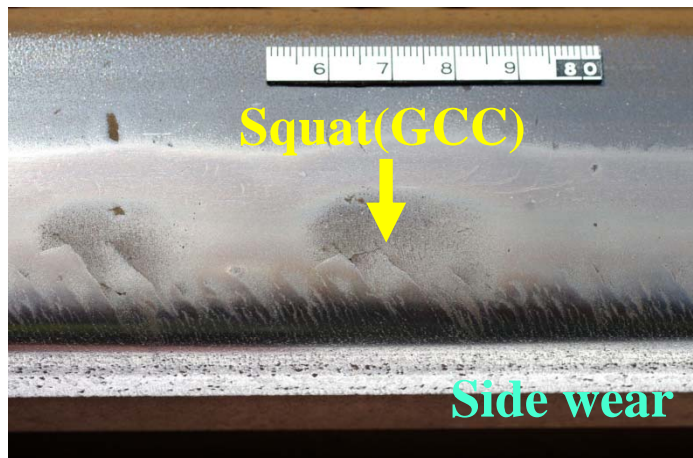
# Appearance of rail RCF damage



As-rolled (tangent)



Head-hardened (curve)



Head-hardened (curve)

**Other problem:**  
side wear  
corrugation  
corrosion fatigue(bottom side)  
etc..

# Chemical composition of rail in Japan

(mass%)

	C	Si	Mn	P	S	Cr
As-rolled	0.63-0.75	0.15-0.30	0.70-1.10	$\leq 0.030$	$\leq 0.025$	-
Head hardened (HH340)	0.72-0.82	0.10-0.55	0.70-1.10	$\leq 0.030$	$\leq 0.020$	$\leq 0.20$

:JIS (Japanese Industrial Standard)

As-rolled : tangent rail

Head hardened : only curve rail (usually less than R800m)



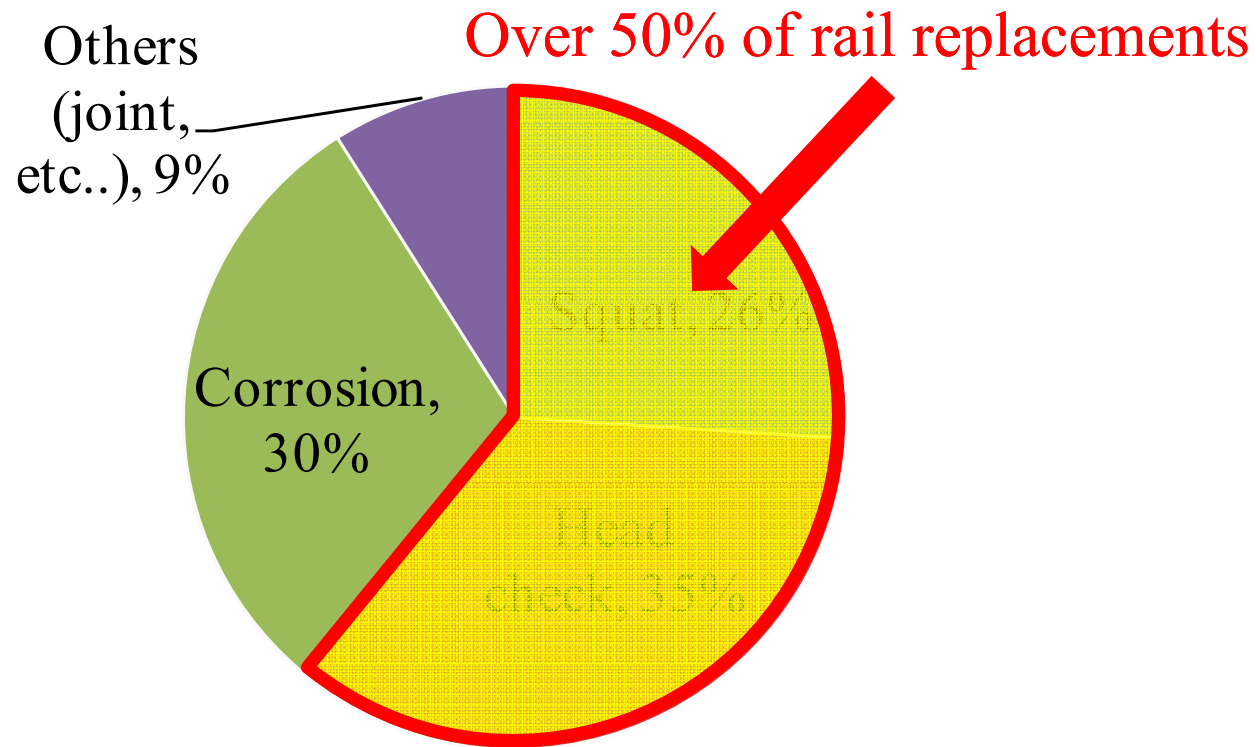
# Mechanical strength of rail in Japan

	Tensile strength (MPa)	Total elongation (%)
As-rolled	$\geq 800$	$\geq 10$
Head hardened (HH340)	$\geq 1080$	$\geq 8$

:JIS (Japanese Industrial Standard)



# Portion of RCF damage for rail replacement



2008-2009 in Tokyo district

Reduction in reliability and operational life of rails



# Mitigating action (Rail grinding by grinding stones)



**Grinding operation**

## **SPENO grinding car for Shinkansen line**

Rail grinding operations are periodically performed to remove the RCF layers.

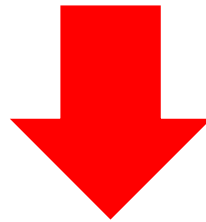
Grinding depth and interval are almost empirically decided.

Quantitative microstructural analyses on RCF layers



## **Purpose of this work**

**Clarify how the RCF layer forms from a material aspect, aiming at the effective mitigating actions for RCF damage**



**Estimate the crystallite size and dislocation density of RCF layer using x-ray diffraction**

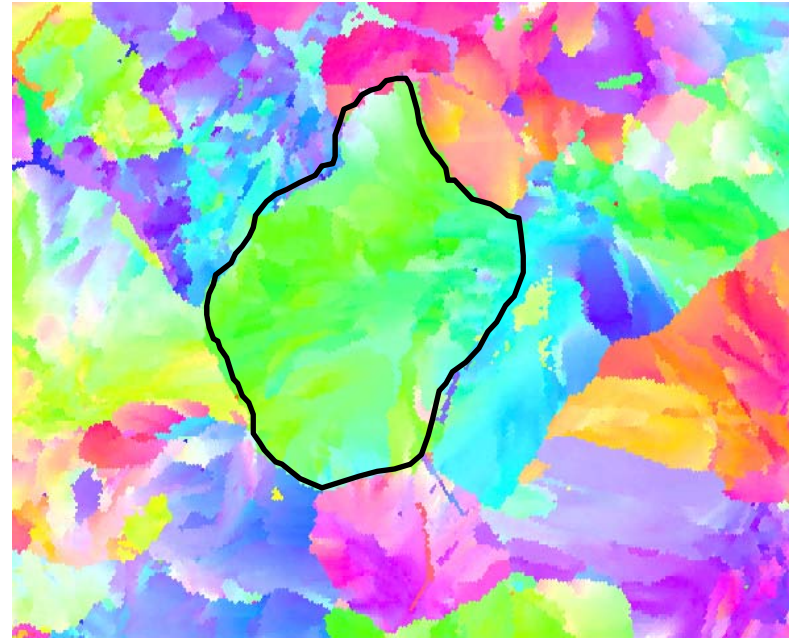




## What is crystallite ?

Grain size from x-ray measurement

Crystal grain with nearly the same crystal orientation



## What is dislocation ?

Irregularity of alignment of atoms

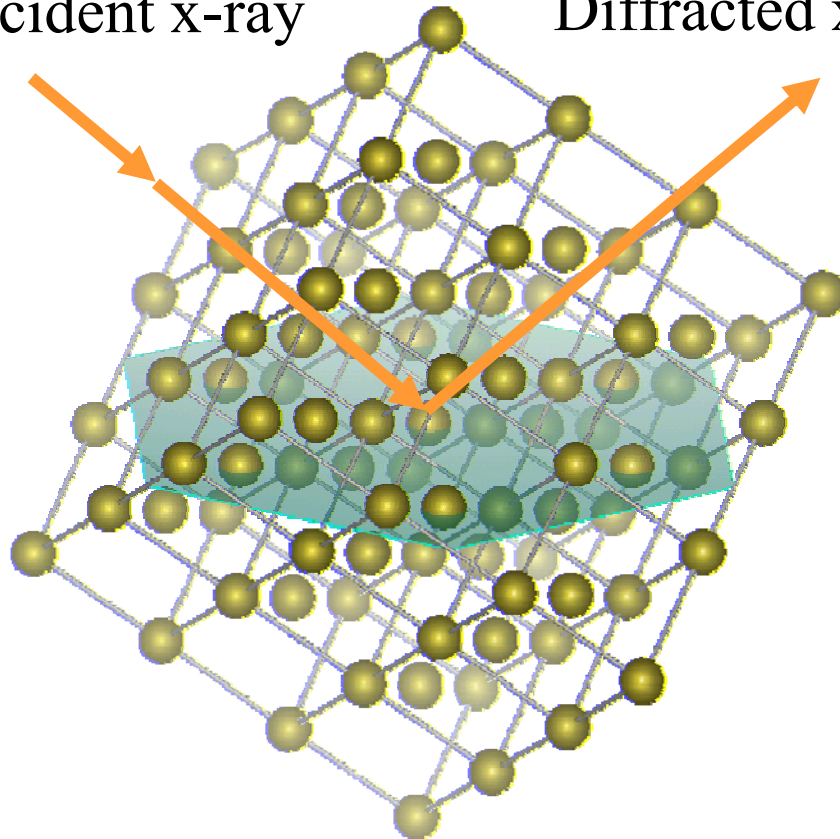


When a material is plastically deformed, dislocations are induced and increase.



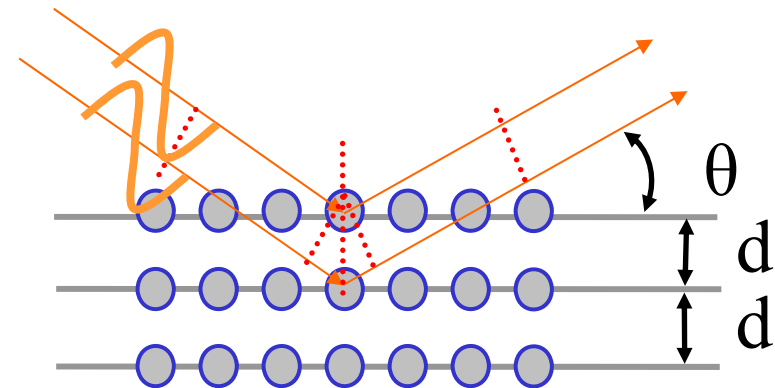
# Principle of x-ray diffraction

Incident x-ray      Diffracted x-ray



Bragg's law

$$n\lambda = 2d \cdot \sin \theta$$



Wavelength :  $\lambda$

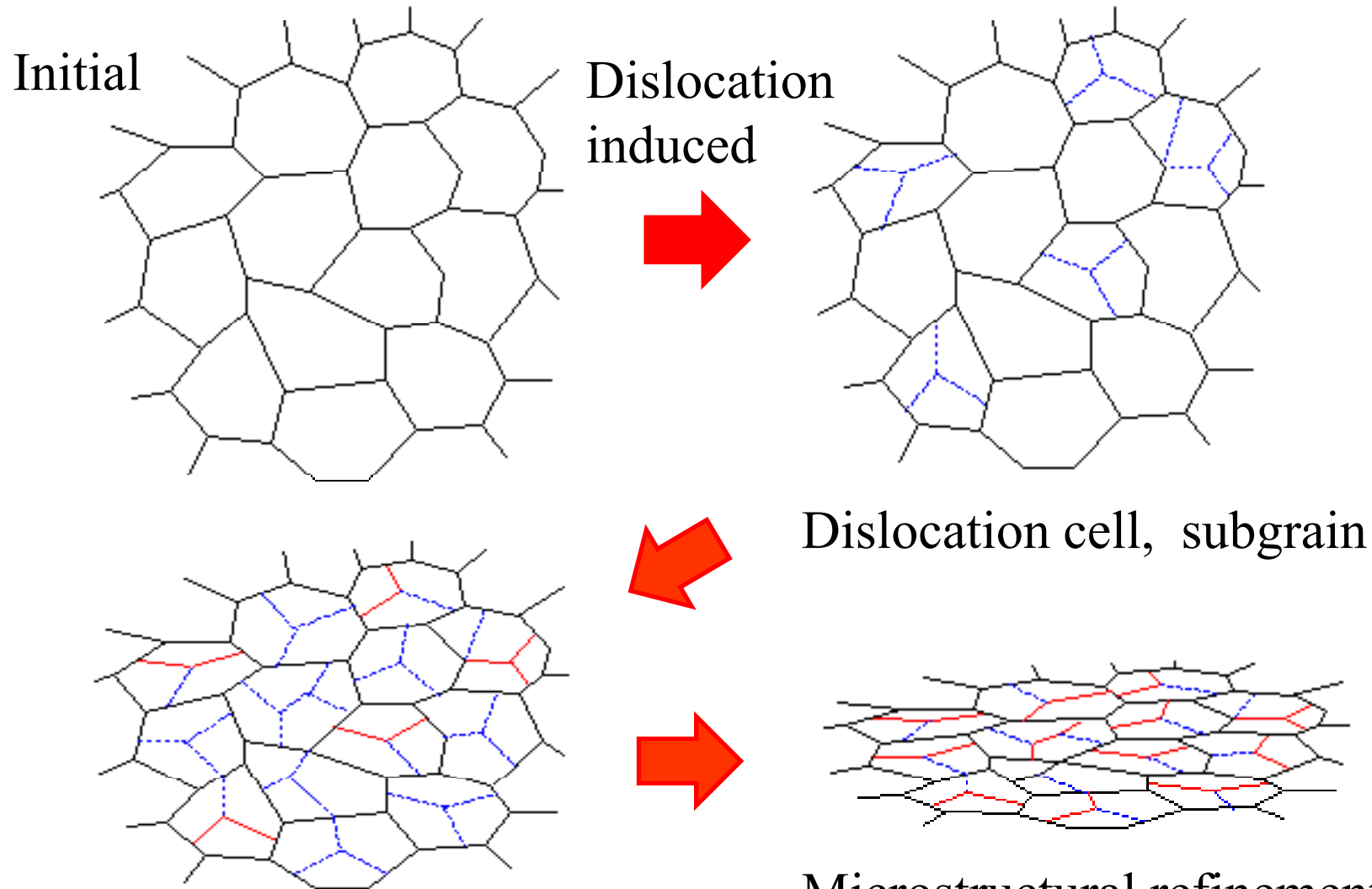
Lattice spacing:  $d$

angle:  $\theta$

Texture formation, crystallite size,  
nonuniform distortion(lattice strain)  
and dislocation density etc..



# Microstructural evolution due to RCF (grain subdivision)



Initial

Dislocation induced

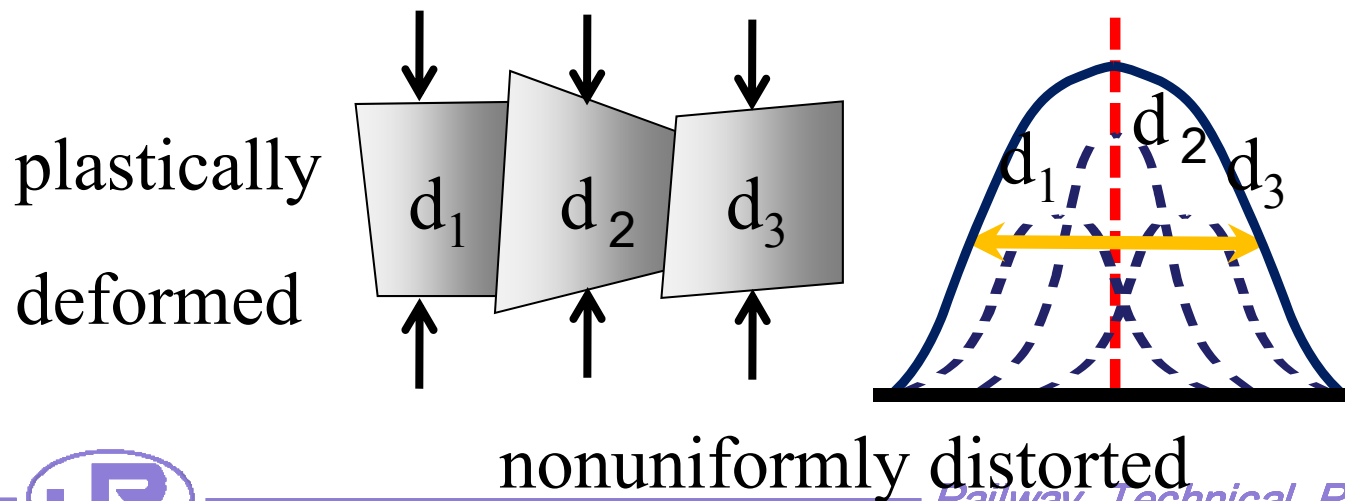
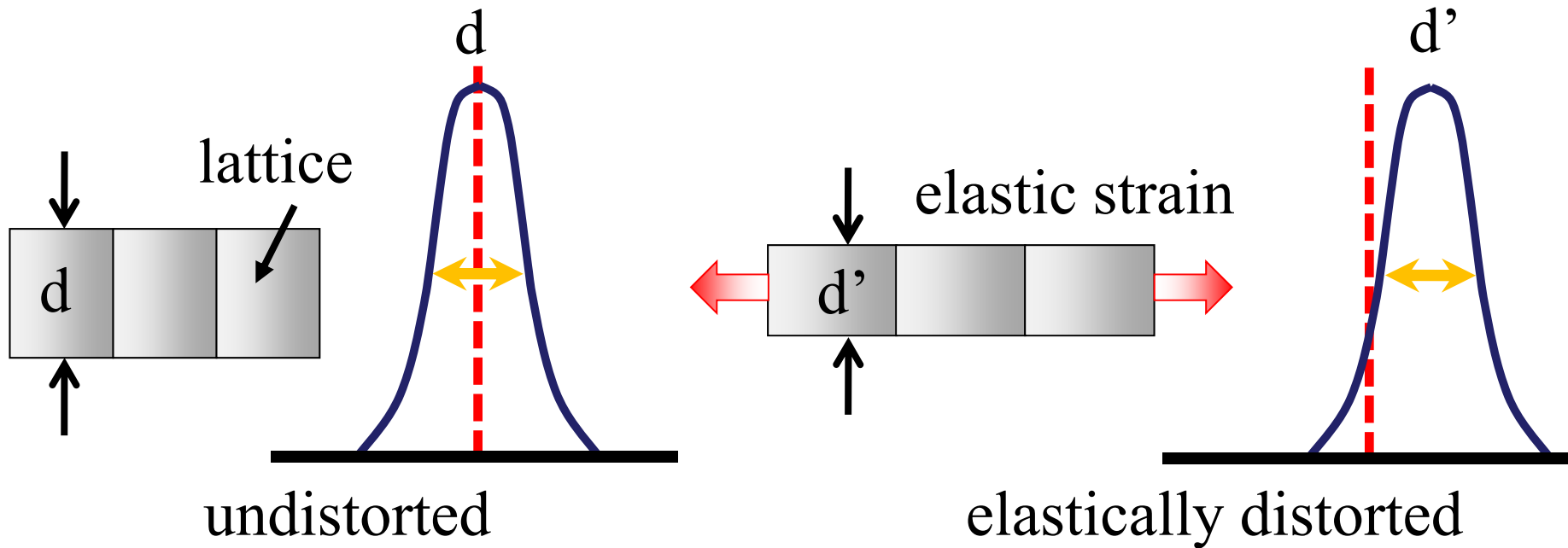
Dislocation cell, subgrain

High angle grain boundary

Microstructural refinement,  
metallic flow, texture .....



# Effect of strain on x-ray diffraction peak



# How to estimate crystallite size and dislocation density

## Williamson-Hall equation

$$\beta \frac{\cos\theta}{\lambda} = 2\eta \frac{\sin\theta}{\lambda} + \frac{1}{\varepsilon}$$

$\beta$  : integral peak width

$\theta$ : diffraction angle

$\eta$  : nonuniform distortion

$\varepsilon$  : crystallite size (nm)

$\lambda$  : incident x-ray wave length

## Modified Williamson-Hall equation

$$\Delta K = \alpha' + \beta KC^{1/2} + O(KC^2)$$

$$\alpha' = \frac{1}{\varepsilon'} \quad K = \frac{2 \sin \theta}{\lambda}$$

C: dislocation contrast factor defined by Warren

## Modified Warren-Averbach equation

$$\ln A(L) = \gamma - X(L)(K^2 C) + P(K^2 C)^2$$

coefficient of (hkl) diffraction

L: Fourier length

A(L): real part of Fourier

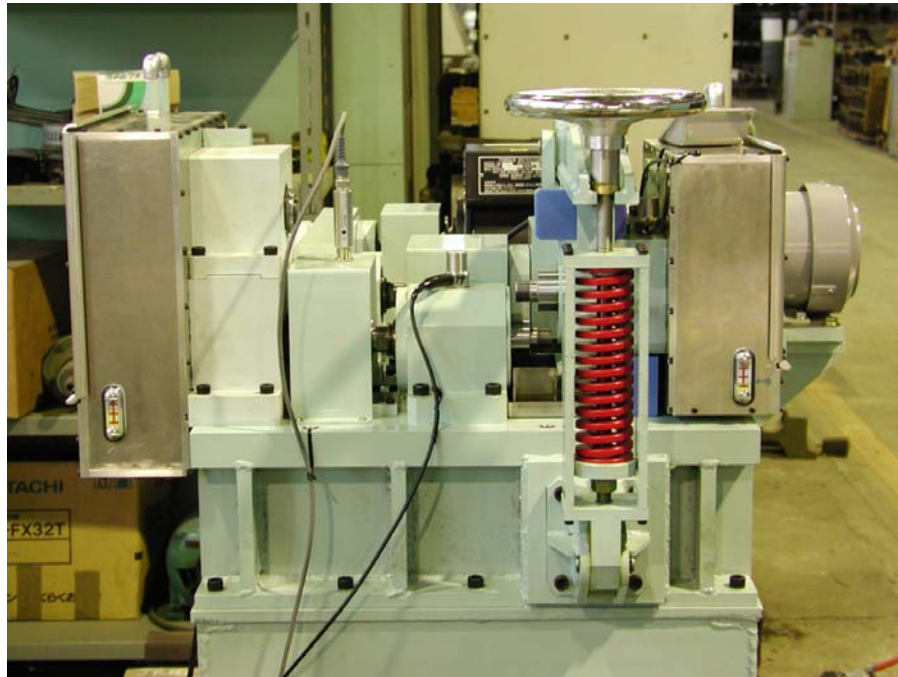
coefficient of (hkl) diffraction

$\rho$ : dislocation density (1/m<sup>2</sup>)

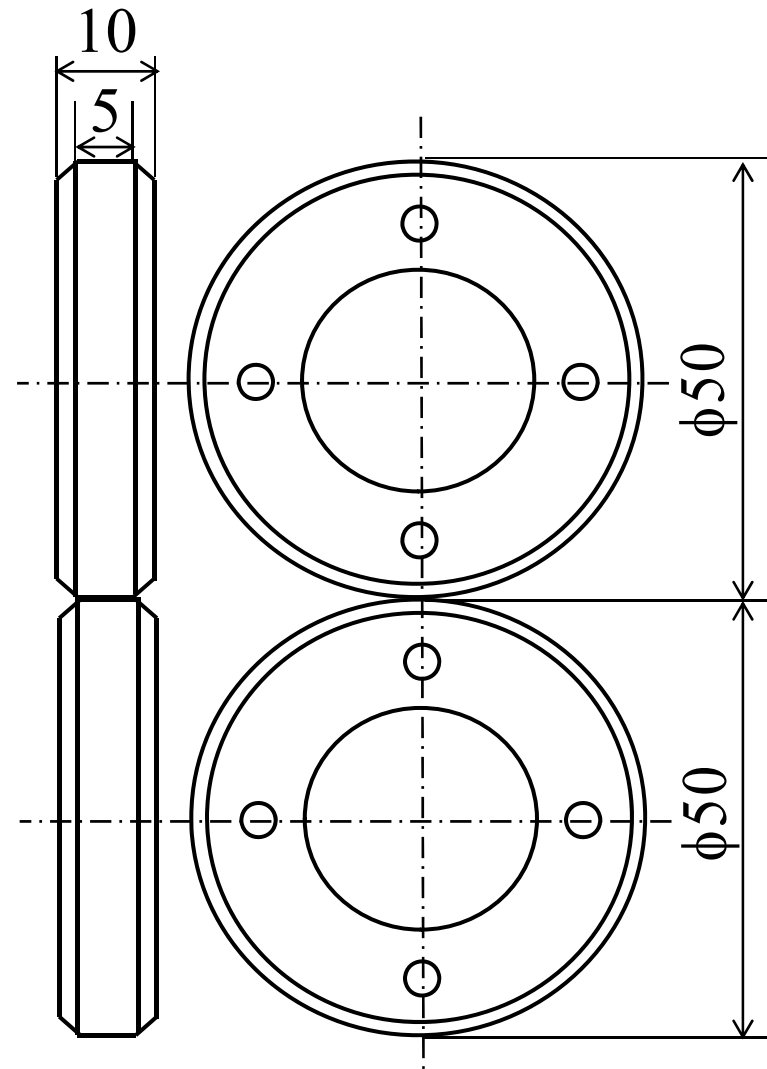
$$X(L) = \frac{\pi b^2 L^2}{2} \rho \ln\left(\frac{R_e}{L}\right)$$



# RCF test equipment



Overview

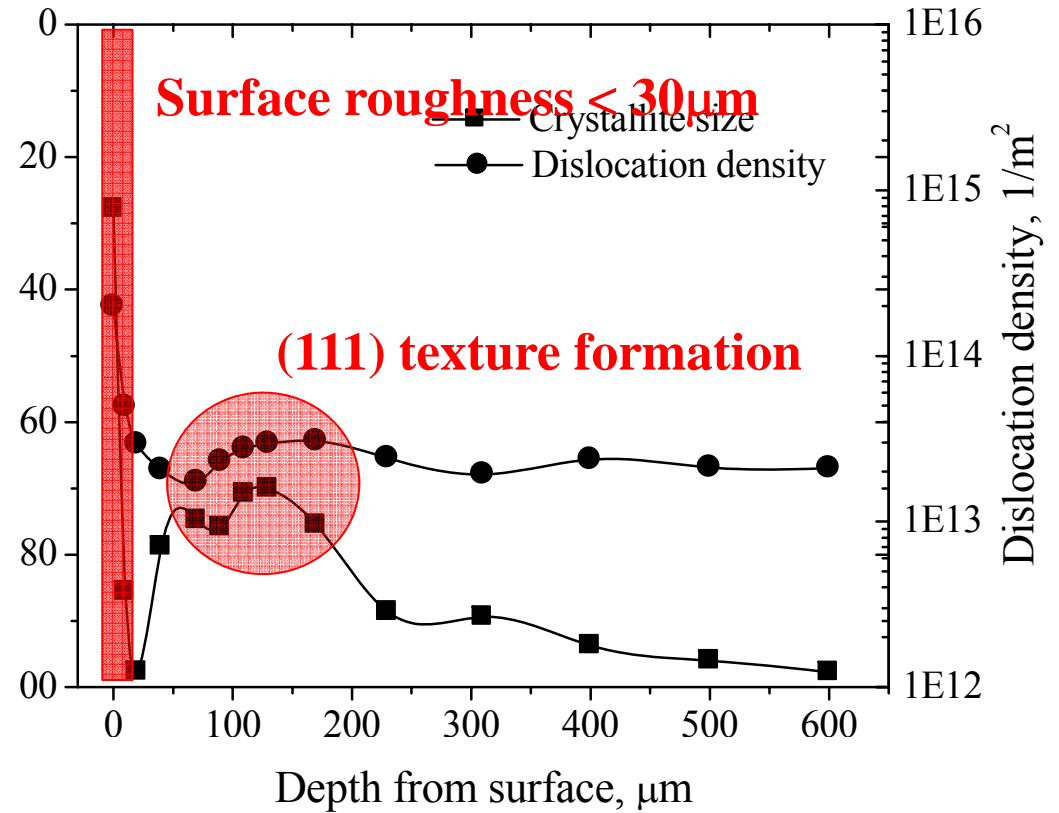
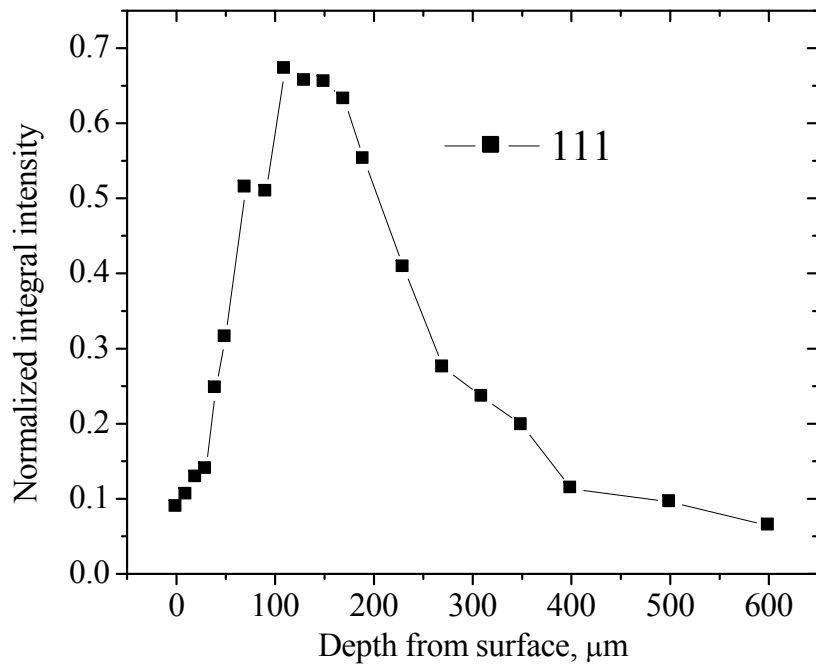
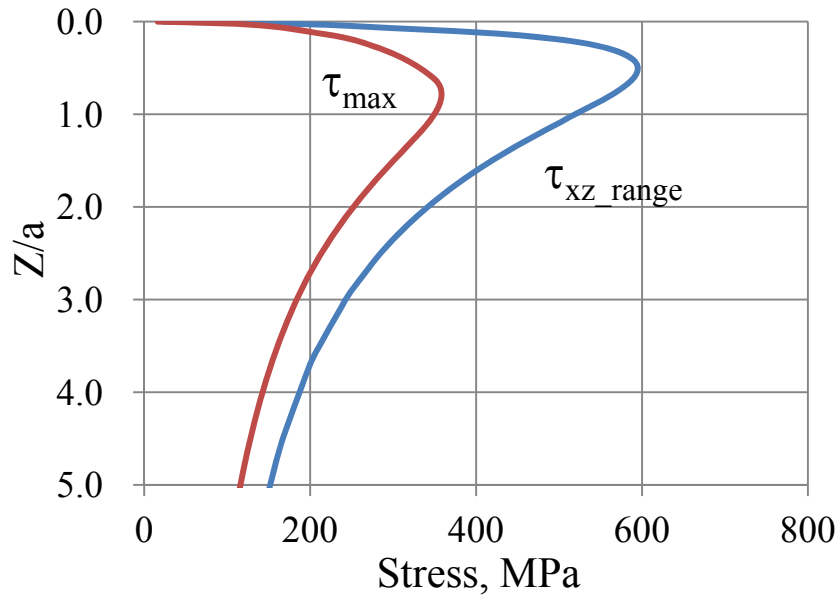


Test sample



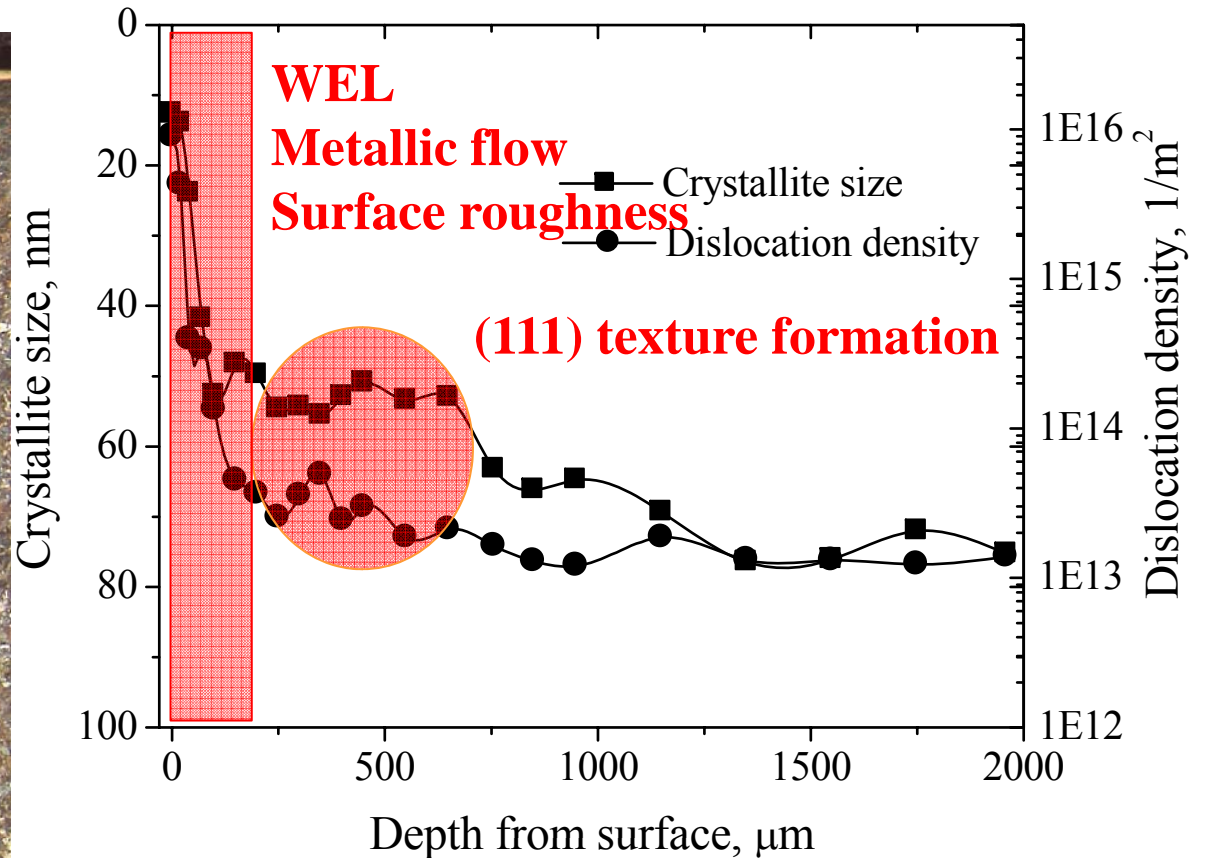
# CF test

Contact pressure : 1.2GPa  
 Slip ratio : 0%  
 100,000 cycles  
 Dry  
Rarely worn after test



It is significant to consider the effect of surface roughness on the contact patch

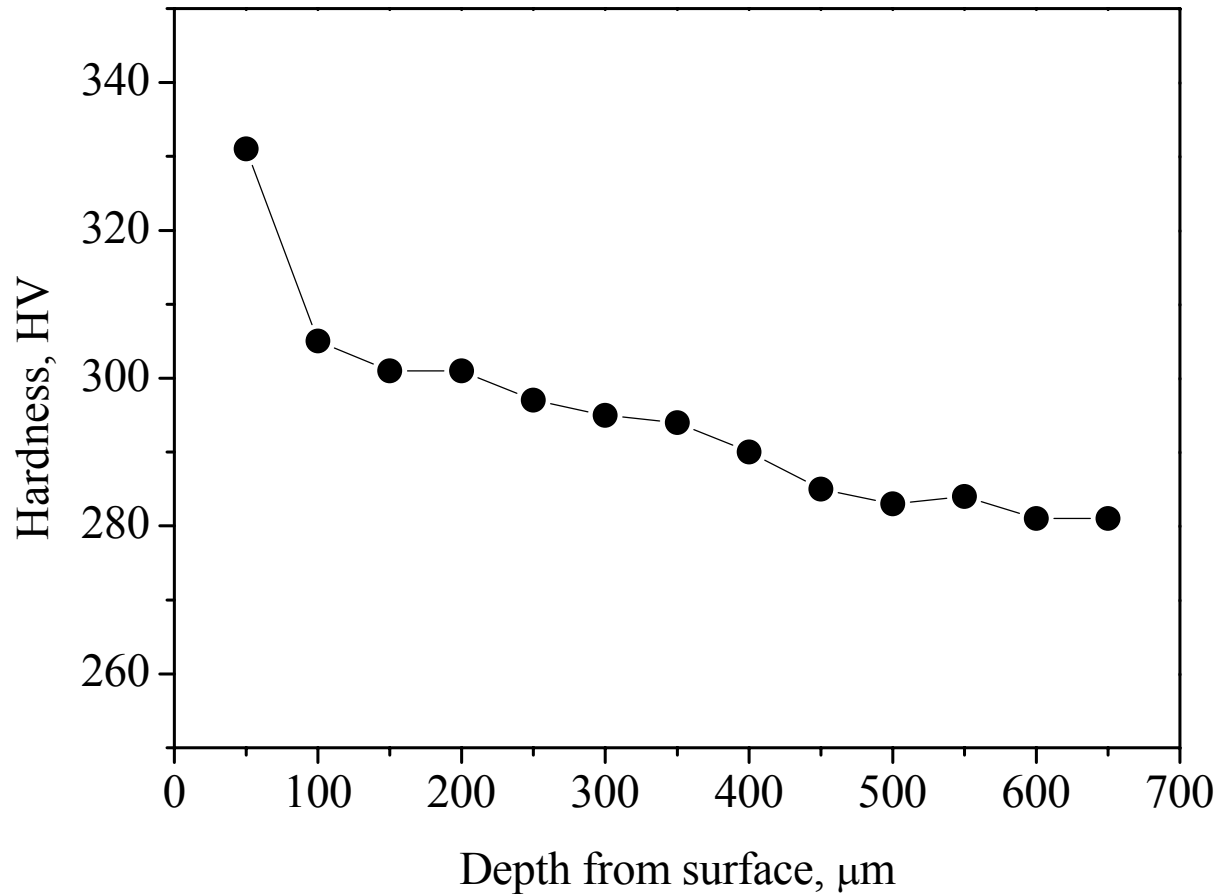
# Serviced tangent rail without rail grinding (500MGT, passenger & freight mixed)



- Similar tendency to the test sample.
- It is possible to investigate how the RCF evolves even in the case of serviced rail.



# Hardness (500MGT)

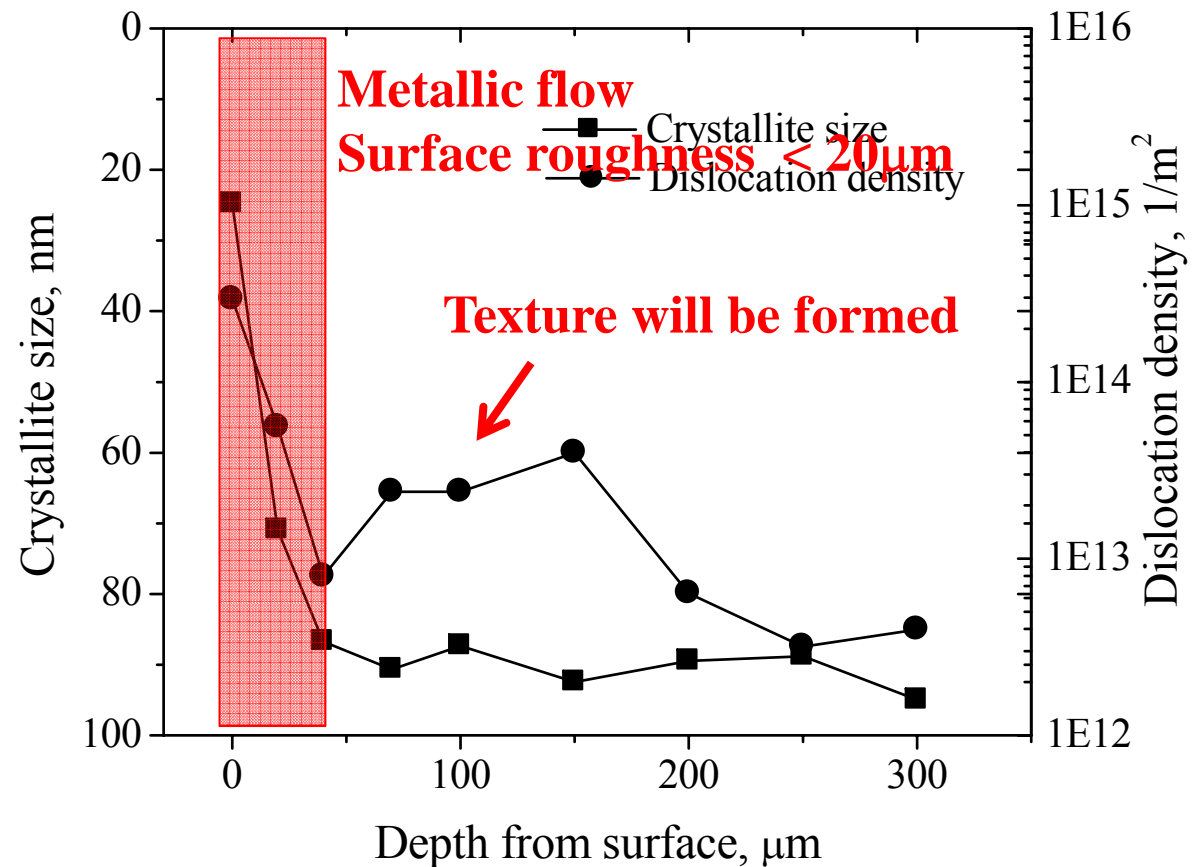
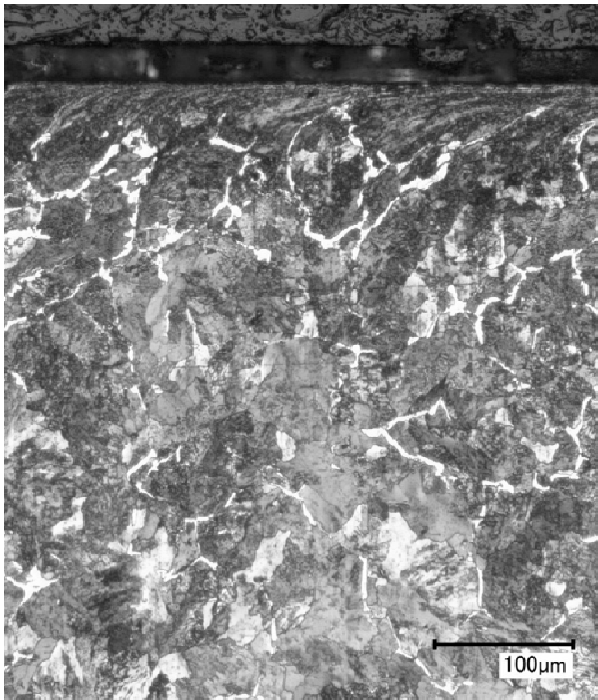


Vickers hardness distribution (0.3HV)

- Total RCF layer is not evaluable.
- Measurement beneath the surface is difficult.



# Serviced tangent rail without rail grinding (50MGT, passenger & freight mixed)



X-ray is feasible even for a thin RCF layer.

We can quantify the degree of RCF layer formation for each condition.

# Conclusions

1. This x-ray measurement makes it possible to quantify the RCF layer from the surface and into the material in one method. Especially it is feasible even for a quite thin layer.
2. On the other hand, it is hard to carry out hardness measurement just on the surface. The hardness measurement could not cover the total RCF layer.
3. Both crystallite size and dislocation density largely change in RCF layers. The surface layer was in all cases more damaged by RCF than the subsurface layer. (111) texture is formed in some depths. (111) texture can be highly enhanced after a while serviced as a tangent rail.
4. It is significant to consider the surface roughness in the contact patch in the evaluation of RCF layer.

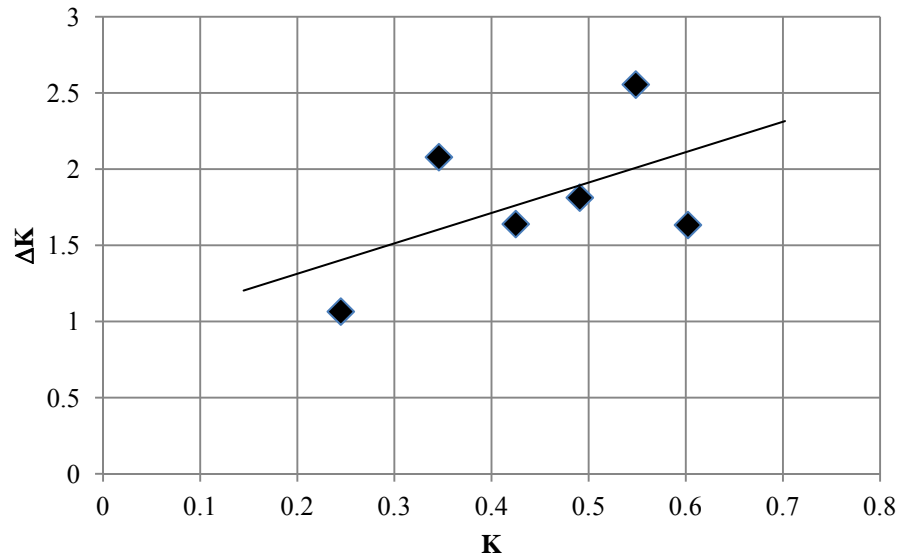


**Thank you for your kind attention**

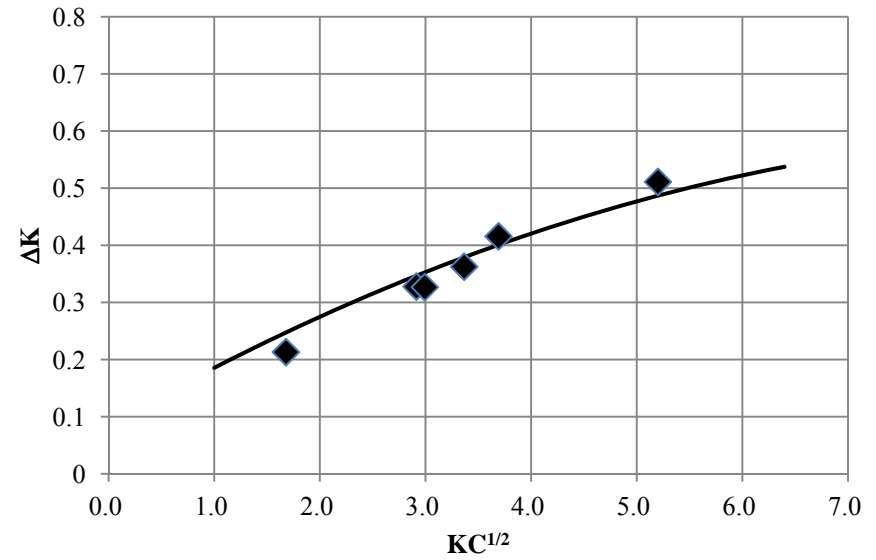


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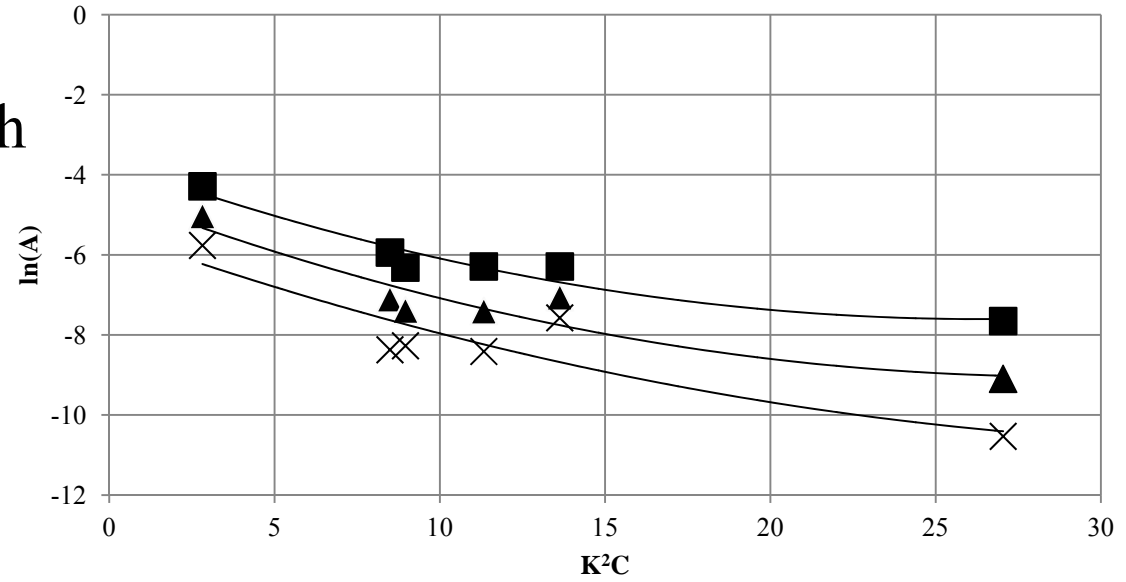
### Williamson-Hall



### Modified Williamson-Hall



### Modified Warren-Averbach



# 111 texture formation(500MGT, serviced tangent rail)

