- Presentation based on report
 - Equivalent Conicity on Norwegian Tracks: Gardermo Line
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 - Track recording and wheel/rail profile measurements
 - Calculations and Statistical Methods
 - Gardermoen Track Geometry
 - Calculation of equivalent conicity as a function of track gauge
 - $\cdot\,$ nominal and worn wheel and rail profiles
 - Statistical distribution of equivalent conicity
 - $\cdot\,$ measured track gauge, worn wheel and rail profiles



Motivation

Background is that conicity is a <u>local</u> quantity which is valid at one location only on the track for one wheelset

The value obtained <u>depends</u> on the displacement of the wheelset laterally and on the measured track gauge at the defined location on the track



A method being demonstrated in this presentation is based on a proposal from CEN 256/WG 10 in order to be able to define the conicity for a whole section

• Description of the method:

Lateral displacement of the wheelset between 2 and 4 mm is considered. If the flangeway clearance is narrow, then a smaller lateral displacement is applied; if the flangeway clearance < 5 mm, then a lateral displacement of 2 mm is used.

Then 2 different local conicities are being calculated, γ_{mid} in the middle of the interval, and γ_{max} which is the largest conicity in the interval 2 to 4 mm.

These 2 sizes are being converted into <u>conicities over a whole defined section</u>; due to calculation of a <u>mean value</u> based on local γ_{mid} , respectively the <u>max. value</u> of the local conicities γ_{max} . In this way informations are given what conicities the wheelset will be exposed for when running on the actual section.

The method presupposes <u>rail profiles being measured continuously</u> over the section. This is <u>not the case in this project</u>. On the contrary, rail profiles have been measured at 12 locations in order to illustrate the method. Hence, the method will give an apprehension of how it could be working, but is of course not correct. The presenting results will therefore deviate from a correct calculation in accordance with the complete method



• Track quality:

Measured with the Track Recording car ROGER 1000
 between Oslo and Eidsvoll in April 2011

- In focus: Gauge and curvature
- Application of Miniprof Equipment
 - Worn rail profiles of type 60E1 on 12 locations measured in June 2008

• Wheel profiles:

- Application of Miniprof Equipment
 - $\cdot\,$ Worn wheel profiles P8 and RD9 measured in 2008
- Nominal profiles also applied in the study:
 - Rail 60E1
 - Wheel profiles S1002, P8, RD9



• Wheel profiles (nominal)



Wheel profil RD9



Distance from back of flange to centre of wheel tread for both profiles: 70 mm



Wheel profile P8

For both profiles: Flange angle: 68° Radius in flange root corner: R13 Differencies in geometry of the profiles P8: R87, R100, R330 RD9: R120, R400

- Calculation of equivalent conicity
 - Depending on track gauge (TG) and spacing of active faces (SR), wheelset amplitude y in this work applies:

 $y_{\max} = 4 mm \qquad if \quad (TG - SR) \ge 9 mm$ $y_{\max} = \left(\frac{(TG - SR) - 1}{2}\right) \qquad if \qquad 5 mm \le (TG - SR) < 9 mm$ $y_{\max} = 2 mm \qquad if \qquad (TG - SR) < 5 mm$

– Values to be calculated in accordance with amplitude:

 $(\tan \gamma_e)_{\max}$ the maximum reached between y = 2 mm and $y = y_{\max}$

Applied method due to proposals in EN 14363

 $(\tan \gamma_e)_{mid}$: for $y = (2 + y_{max})/2$





Gardermobanen-equivalent conicity • Statistical method applied Illustration on Bergen Line (from former work) _ 1 🖵 0.5 Red lines show tangent 1/R [m⁻¹] track sections of length of 250 m -0.5 -1└─ 286 288 292 296 290 294 298 300 kmp 1440 Measured track gauge မြို့ ၂435 ပို 1430 288 292 298 286 290 294 296 300 kmp



• Statistical method applied

– Illustration on Bergen Line (continues); three step method applied for calculations due track gauge and nominal profiles



294

kmp

294.2

294.4

294.6

Equivalent conicity, mean value: blue lines: local values red lines: sliding mean values over 100 m green lines: mean value of red line over a length of 250 m

Equivalent conicity, max value: blue lines: momentary values red lines: sliding mean values over 100 m green lines: maximum value of red line over a length of 250 m



0.3

.25

0

0.15 <u>li</u> 293.4

293.6

293.8

(tan γ_e)_{max}

• Track gauge and curvature, Gardermoen



Red lines: boundaries for the evaluated tangent track sections; gauge, curvature

Track gauge on almost 90 sections: min. value max value

• Equivalent conicity

has been calculated for nominal and worn profiles
as a function of track gauges:

- nominal P8 and nominal 60E1
- nominal P8 and worn 60E1
- worn P8 and nominal 60E1
- $\cdot\,$ worn P8 and worn 60E1
- $\cdot\,$ nominal RD9 and nominal 60E1
- nominal RD9 and worn 60E1
- worn RD9 and nominal 60E1
- $\cdot\,$ worn RD9 and worn 60E1
- $\cdot\,$ nominal S1002 and nominal 60E1
- $\cdot\,$ nominal S1002 and worn 60E1



• Nominal and worn profiles

- Rail profiles (one example of 12 locations)



Wear pattern is identified for all rails at 12 locations



Right track, km 32+863 left rail

Right track, km 32+863 right rail

• Moderately worn wheel profiles; P8; RD9









Wear pattern is identified

Wheel profile RD9

• Conicity cal., nominal P8 on nominal 60E1



as function of track gauge Sd: flange thickness A: spacing of activ faces

Remarks:

Highest values of conicities in interval for nominal track gauge (1433 – 1436 mm)

Wheel – rail contact geometry



• Conicity cal., nominal P8 on worn 60E1



Worn rail profiles measured at 12 locations; equivalent conicity calculated as function of track gauge



Track gauge at each location of measured rail profile has not been applied

• Conicity cal., worn P8 on nominal 60E1



Flange thickness Sd = 28,9 Very high values in the range for nominal track gauge





• Conicity cal., worn P8 on worn 60E1





Worn rail profiles measured at 12 locations; moderately worn P8 profile (Sd = 28,9 mm); equivalent conicity calculated as a function of track gauge

Track gauge at each location of measured rail profile has not been applied

• Conicity cal., nom. RD9 on nom 60E1



as a function of track gauge Sd: flange thickness A: spacing of active faces

Remarks: Low values of conicities in range for nominal track gauge (1433 – 1436 mm)



Wheel - rail contact geometry

• Conicity cal., nom. RD9 on worn 60E1



Worn rail profiles measured at 12 locations; equivalent conicity calculated as a function of track gauge



Track gauge at each location of measured rail profile has not been applied



• Conicity cal., worn RD9 on nominal 60E1



• Conicity cal., worn RD9 on worn 60E1



Worn rail profiles measured at 12 locations; equivalent conicity calculated as function of track gauge; moderately worn RD9

Track gauge at each location of measured rail profile has not been applied

• Conicity cal., nom. P8, RD9, S1002, 60E1

(tan γ_e)_{mid} (tan γ_e)_{max}





Comparision of equivalent conicities of 3 nominal wheel profiles P8, RD9, S1002 with nominal rail profile 60E1



tan γ_e 0.4

0.3

0.1

e.0 2

1428 1430 1432 1434 1436 1438 1440 1442 1444 1446 track gauge [mm]

Rail: 60E1 (UIC60) 1:20 Wheel: RD9 Sd=27.65 mm A=1360 mm





P8 and worn 60E1



Comparision of equivalent conicity of 3 nominal wheel profiles P8, RD9, S1002 with worn rail profile 60E1

S1002 and worn 60E1



RD9 and worn 60E1

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- Statistical distribution
 - Measured track gauge has been applied in order to calculate the conicities along the track
 - Worn rail profiles have been choosen and used randomly from the 12 sets of measured rail profiles
 - There are almost 90 sections
 - The selected rail profile being choosen randomly, is constant for a section
 - \cdot no variation of worn rail profile inside of a section
 - In this way a distribution of conicities have been found



• Distribution, nom. P8 and nom. 60E1



Track: Oslo-Eidsvoll Rail: 60E1 (UIC60) 1:20 Wheel: P8 Sd=30 mm A=1360 mm 0.997 $(\tan \gamma_e)_{mid}$ 0.99 0.98 $(\tan \gamma_e)_{max}$ 0.95 0.90 0.75 Probability 0.50 0.25 0.10 0.05 0.02 0.003 0.05 0.1 0.15 0.2 0.25 0.3 0.35 04 0.45 tan γ_e

Equivalent conicity has been calculated as explained in previous slides:

 $(\tan \gamma_e)_{mid}$ $(\tan \gamma_e)_{max}$

Rail profiles have been choosen randomly from 12 locations and is being held constant in a section

Distribution is shown



• Distribution, nom. P8 and worn 60E1



Track: Oslo-Eidsvoll Rail: Random, measured in 12 locations Wheel: P8 Sd=30 mm A=1360 mm

0.25

0.2

tan γ_e

0.35

0.4

0.3

0.45

Track: Oslo-Eidsvoll Rail: Random, measured in 12 locations Wheel: P8 Sd=30 mm A=1360 mm

Equivalent conicity has been calculated as explained in previous slides:

 $(\tan \gamma_e)_{mid}$

 $(\tan \gamma_e)_{\max}$

 $(\tan \gamma_e)_{mid}$

· (tan γ_e)_{max}

Rail profiles have been choosen randomly from 12 locations and is being held constant in a section

Distribution is shown



0.997

0.99 0.98

0.95 0.90

0.75

0.25 0.10 0.05 0.02 0.01 0.003

0

0.05

0.1

0.15

Probability 0.50

• Distribution, worn P8 and nom. 60E1





Equivalent conicity has been calculated as explained in previous slides:

 $(\tan \gamma_e)_{mid}$

 $(\tan \gamma_e)_{\max}$

Rail profiles have been choosen randomly from 12 locations and being held constant in a section

Distribution is shown



• Distribution worn P8, worn 60E1



Track: Oslo-Eidsvoll Rail: Random, measured in 12 locations Wheel: FT08_35kkm_P8_BMU_2 Sd=29.9 mm A=1360 mm

Equivalent conicity has been calculated as explained in previous slides:

$$(\tan \gamma_e)_{mid}$$

 $(\tan \gamma_e)_{\max}$

Rail profiles has been choosen randomly from 12 locations and is being held constant in a section

Distribution is shown





• Distribution nom. RD9 and nom. 60E1



Track: Oslo-Eidsvoll Rail: 60E1 (UIC60) 1:20 Wheel: RD9 Sd=27.65 mm A=1360 mm

Equivalent conicity has been calculated as explained in previous slides:

$$(\tan \gamma_e)_{mid}$$

 $(\tan \gamma_e)_{\max}$

(tan γ_e)_{mid}

- (tan γ_e)_{max}

Rail profiles have been choosen randomly from 12 locations and is being held constant in a section

Distribution is shown



0.997

0.99 0.98

0.95 0.90

0.75

0.25 0.10 0.05

0.02 0.01 0.003 L... 0

0.05

0.1

0.15

0.2

tan γ_e

0.25

0.3

0.35

0.4

0.45

Probability 0.50

• Distribution nom. RD9 and worn 60E1





Equivalent conicity has been calculated as explained in previous slides:

$$(\tan \gamma_e)_{mid}$$

 $(\tan \gamma_e)_{\max}$

Rail profiles have been choosen randomly from 12 locations and is being held constant in a section

Distribution is shown

• Distribution, worn RD9 and nom. 60E1



 $(\tan \gamma_e)_{\max}$ Track: Oslo-Eidsvoll Rail: 60E1 (UIC60) 1:20 Wheel: FT03 52kkm RD9 BMU 2 Sd=27.73 mm A=1360 mm Rail profiles have been (tan y_e)_{mid} choosen randomly (tan y_e)_{max} from 12 locations and in a section

is being held constant

Equivalent conicity has

explained in previous

been calculated as

slides:

 $(\tan \gamma_e)_{mid}$

Distribution is shown



0.997

0.99 0.98

0.95 0.90

0.75

0.50 0.25

0.10 0.05 0.02 0.01

0.003

0.05

0.1

0.15

0.2

tan γ_e

0.25

0.3

0.35

0.4

0.45

Probability

• Distribution, worn RD9 and worn 60E1



Equivalent conicity has been calculated as explained in previous slides:

$$(\tan \gamma_e)_{mid} (\tan \gamma_e)_{max}$$

Rail profiles have been Choosen randomly From 12 locations and is Being held constant In a section

Distribution is shown







• Conclusions

Equivalent conicities of Gardermoen Airport Line have been shown

- Measurements
 - \cdot track gauges
 - $\cdot\,$ nominal and worn wheel and rail profiles
- Statistical methods have been applied
 - $\cdot\,$ Three step method for mean and max values
- Results are considered as satisfactorily
 - For most cases the simple formula is satisfied:

$$(\tan \gamma_e) \le \left(0,50 - \frac{V_{\text{lim}}}{1000}\right) = \left(0,50 - \frac{210}{1000}\right) = 0,29$$

