

Rail Vehicle Response to Carbody Excitations Imitating Crosswind

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Overview

- Introduction
- Measurement setup
- Simulation setup
- Measurement and simulation results
- Conclusions







- Crosswind on rail vehicles may result in
 - ⇒ large lateral displacements and roll motion of the carbody relative to the centre of track
 - \Rightarrow large deflections in the vehicle secondary suspension
 - ⇒ vehicle overturning about one of the rails in extreme cases
- Field tests to determine vehicle response to crosswind are not applicable due to
 ⇒ safety and economical reasons
 - \Rightarrow defined conditions hard to realise
- Determination of vehicle response to crosswind thus requires simulations, but these need to be validated











In present work:

⇒ Full-scale measurements:

Introduction of lateral, crosswind-like loads to the carbody of a still-standing vehicle and measuring the vehicle response

Calculate the corresponding vehicle response by means of multibody simulations

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Introduction

Vehicle used in present work: One car of electric multiple unit

- Carbody length: 25.5 m
- Bogie centre distance: 19.0 m
- Axle distance within bogie: 2.7 m
- Axle load: 15.4 ton (4 axles)



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Bogie frame Max. force 30 kN Max. stroke 80 mm 1.45 m 19 m Max. force 30 kN Max. stroke 80 mm Rear view Top view research where ECOlogy & ECOnomy me



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Two quasi-static load cases











Measurement setup: vehicle response





Simulation setup

- Detailed multibody dynamics model of the vehicle comprising 46 rigid bodies and 124 degrees of freedom
- Simulations performed using the software SIMPACK
- Measured actuator forces as input for the simulations



• Same output quantities as for the measurements





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Measurement results & simulation input: actuator forces for quasi-static load cases



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Measurement results & simulation input: actuator forces for dynamic load cases





Measurement & simulation results: quasi-static synchronous load case



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Measurement & simulation results: dynamic synchronous load case

simulation measurement 40 Deflection [mm] Angle [degree] Rel. lat. deflection CB BG1 Rel. lat. deflection CB BG1 30 Rel. lat. deflection CB BG2 0.75 Rel. lat. deflection CB BG2 Rel. roll angle CB BG2 20 Rel. roll angle CB BG2 .5 10 .25 n. 0.3 0.2 0.1 0.1 0.1 .at. acc. CB floor BG1 Lat. acc. CB floor BG1 Lat. acc. CB floor BG2 Lat. acc. CB floor BG2 -0.1 tg -0.2 40Delta Q [kN] Delta Q BG2 WS1 Delta O BG2 WS1 Delta O BG2 WS2 30 Delta Q BG2 WS2 20 10 0 20 35 15 20 25 5 10 15 25 30 10 30 35 Π í٥ Time [s] Time [s]

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Measurement & simulation results: quasi-static asynchronous load case





Measurement & simulation results: dynamic asynchronous load case

simulation measurement 40 Deflection [mm] [degree] Rel. lat. deflection CB BG1 Rel. lat. deflection CB BG1 30 Rel, lat, deflection CB BG2 Rel. lat. deflection CB BG2 .75 Rel. roll angle CB BG2 Rel, roll angle CB BG2 20 Angle | 10 25 acc [m/s^2] 0.3 Lat. acc. CB floor BG1 Lat. acc. CB floor BG1 0.2 Lat. acc. CB floor BG2 at. acc. CB floor BG2 0.1 0 -0 .1 Lat. -0.2 30 Delta Q [kN] Delta Q BG2 WS1 Delta O BG2 WS1 Delta O BG2 WS2 Delta O BG2 WS2 20 100 20 25 30 35 í٥ 10 15 35 40 15 20 25 30 40 Ω 10 Time [s] Time [s]

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- Responses of a still-standing rail vehicle due to carbody excitations imitating steady and unsteady crosswind have been investigated by means of full-scale measurements and multibody simulations.
- A gust-like event in the force application produces an overshoot in load transfer of vertical wheel-rail forces, which also represents the maximum force response of the vehicle.
- As compared to synchronous loads, the asynchronous loads result in carbody yaw, less roll response and less load transfer of vertical wheel-rail forces.
- Measurements and simulations show in general good agreement; simulated oscillations indicate too low damping.





Short movie





Thank you for your attention!

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