# High-fidelity simulations of turbulent boundary layers on flat and curved surfaces

Philipp Schlatter, Ricardo Vinuesa,

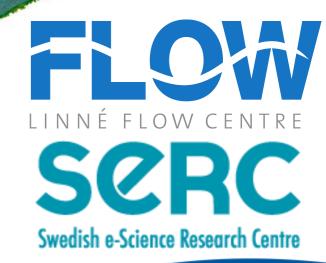
Ramis Örlü

Linné FLOW Centre and

Swedish e-Science Research Centre (SeRC)

KTH Mechanics, Stockholm, Sweden







- Introduction HPC
- Turbulent boundary layers Simulation
- Wing simulations
- Flow control
- Codes and tools



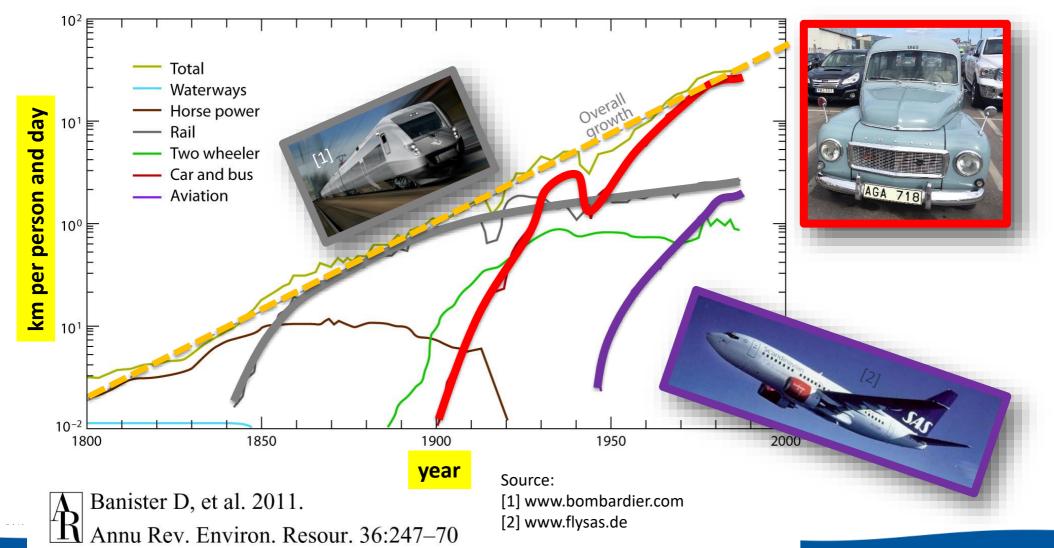


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Skin friction/drag reduction is the key for economically and ecologically more efficient transport



Marine 2019, May 14, 2019



# Navier-Stokes equations...

Data from Mira (ANL, 2013), million core hours

<ul><li>Engineering/CFD</li></ul>	525	19%
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Subsurface flow & reactive transport 80 3%

Combustion 100 4%

• Climate 280 10%

Astrophysics 133 5%

1118 40%

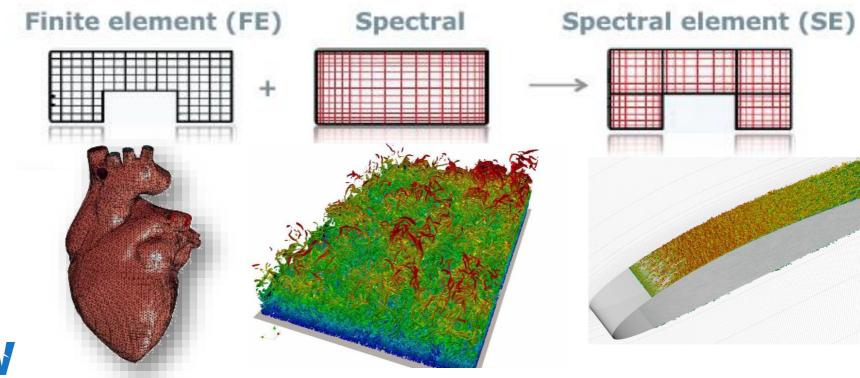
(fraction of Navier-Stokes based simulations on current supercomputers)





### Why Spectral Elements?

- ➤ **High-order numerical methods** are beneficial for accurate simulations of turbulent flows due to the significant scale disparity of the flow structures, both in time and space.
- > Spectral elements allow to solve flows in complex geometries.

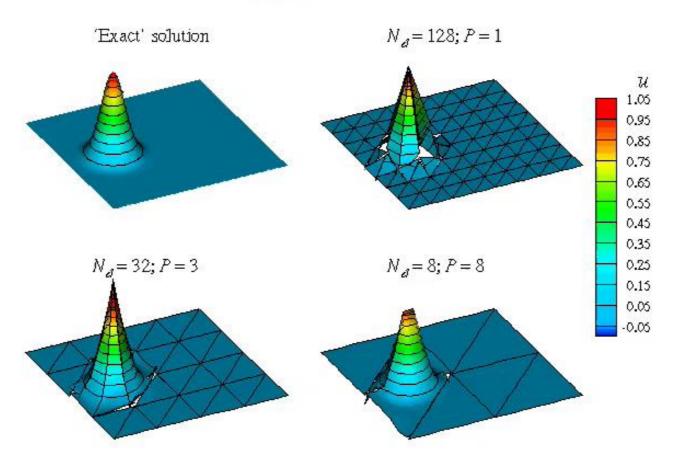




### **Why Spectral Elements?**

• Higher order p (vs. smaller grid spacing h) means more work per core/communication: "convecting cone"

$$Time = 0$$





From David Moxey, Univ. Exeter



# Nek5000 - Spectral Elements (CG)

- SEM code by Paul F. Fischer, Argonne National Lab, USA Open source: nek5000.mcs.anl.gov
- 80 000 lines of Fortran 77 (some C for I/O), MPI (no hybrid)
- Gordon Bell Prize 1999 for algorithmic quality and performance
- KISS ("Keep it simple, stupid") world's most powerful computers have very weak operating systems

EU Projects on algorithms (CRESTA, ExaFLOW, Excellerat ...):

adaptive meshing, GPUs, ...



Good scaling up to 1,000,000 ranks on Mira (10PFlops BG/Q)







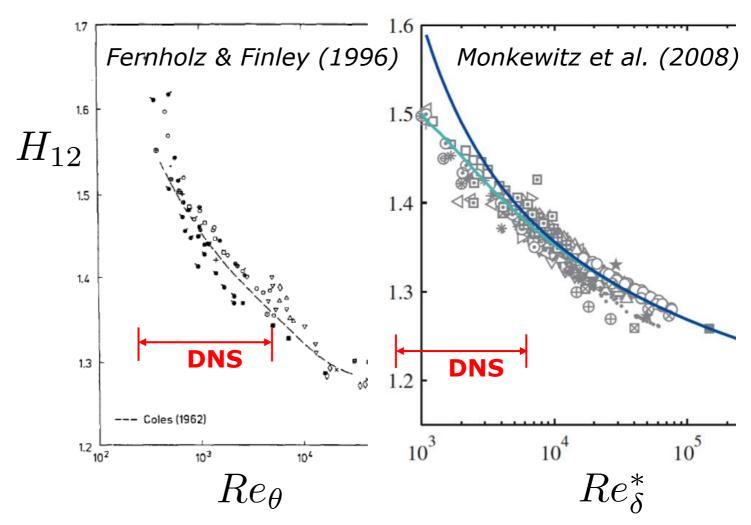
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# What we are used/expect to see ...



Compilation/ Assessment of experimental data from ZPG TBL flows



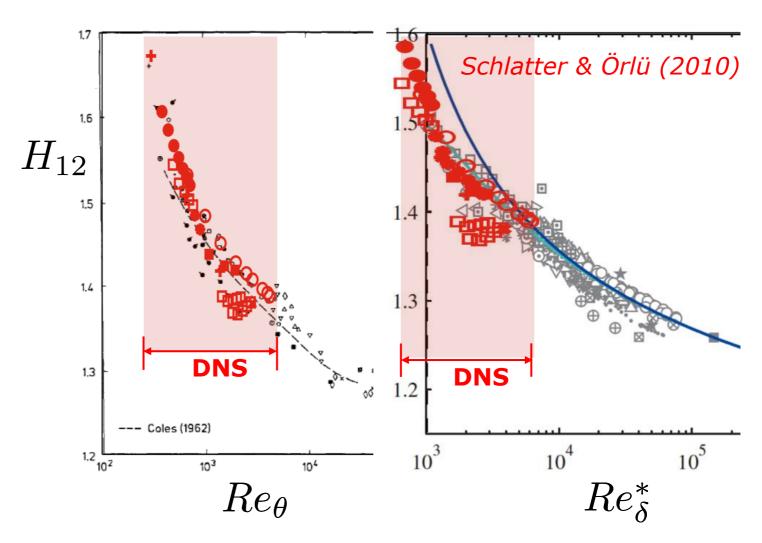
**Physical experiments** are commonly scrutinised before they are employed to calibrate, test, or validate other experiments, scaling laws or theories

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### ... and what "we" are not so used to see



Red symbols are data from 7 independent DNS from ZPG TBL flows



**Simulation data** are hardly scrutinised, when it comes to basic (integral) quantities

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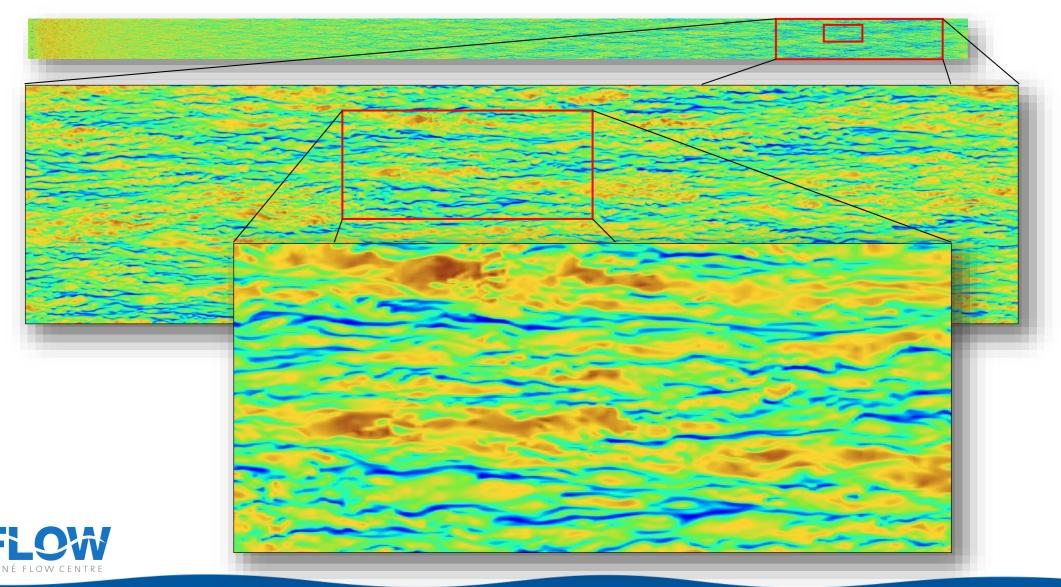
# Turbulent flow close to solid walls...





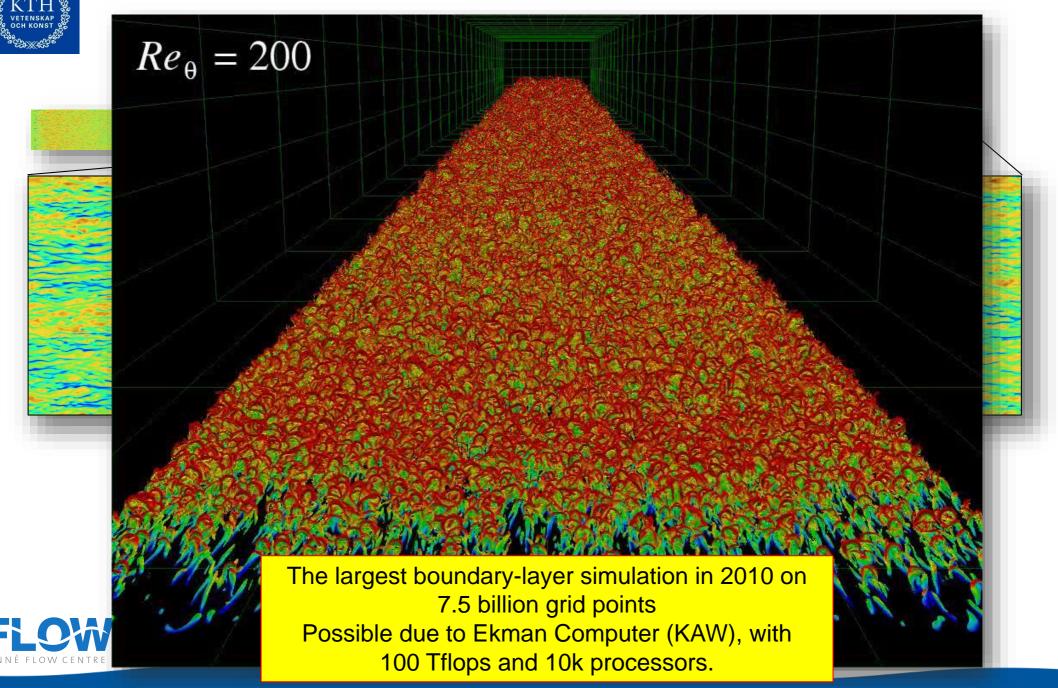
# Turbulent flow close to solid walls... TSFP-7 in 2011

#### simulation result





# Turbulent flow close to solid walls...



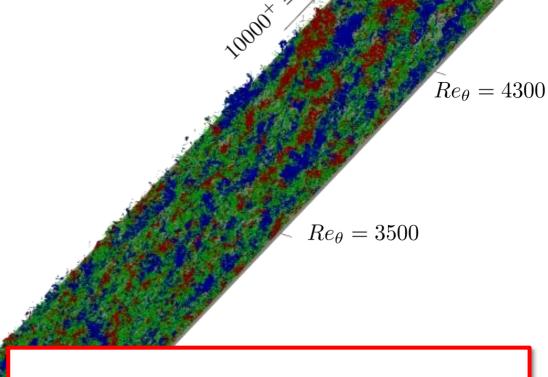
# How to get turbulence?



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 $\geq 3.2\delta_{99}$ 

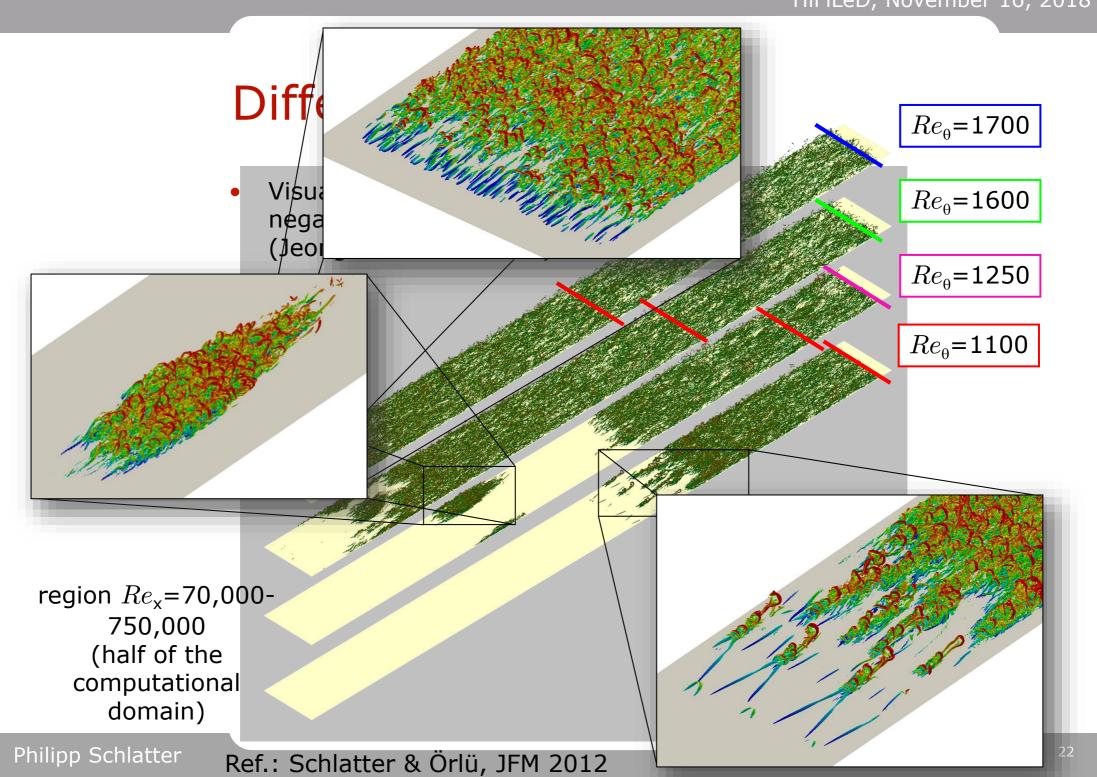
How to get turbulence?



- artifical turbulence (e.g. Klein et al.)
- precursor (periodic) simulation
- recycling/rescaling (Lund et al.)
- tripping/transition to turbulence

$$Re_{\theta} = 1410$$

Isocontours of negative  $\lambda_2$  and positive / negative disturbance velocity



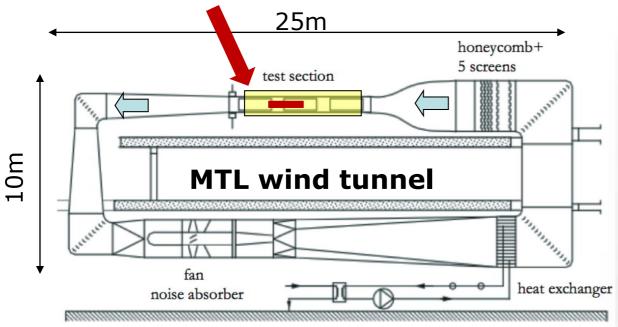


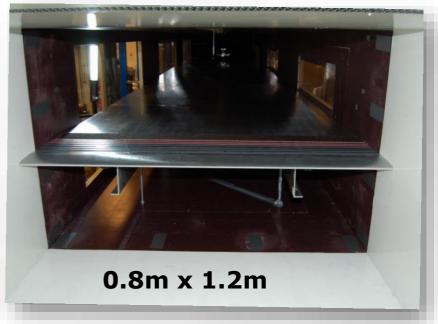
# Let's compare DNS and experiments...

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# New experiments at KTH

- ZPG TBL flow in the range 2300<  $Re_{\theta}$  < 7500 ( $\ddot{O}rl\ddot{u}$ , 2009)
  - single hot-wire measurements at 1.65m from leading edge of a 7m long plate fulfilling "equilibrium" criteria (à la Chauhan et al. 2009)
  - independent skin friction measurements by means of oil-film interferometry
  - DNS corresponds to a 2m stretch...

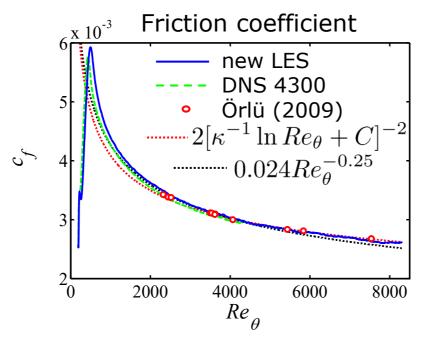


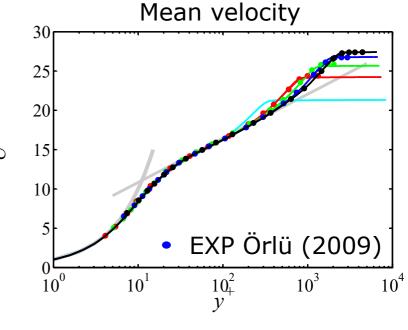


# TBL LES up to $Re_{\theta}$ =8300

**Ongoing** LES (using ADM-RT)







**Domain**:

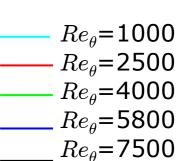
13500 x 400 x 540 $\delta_0$ \*

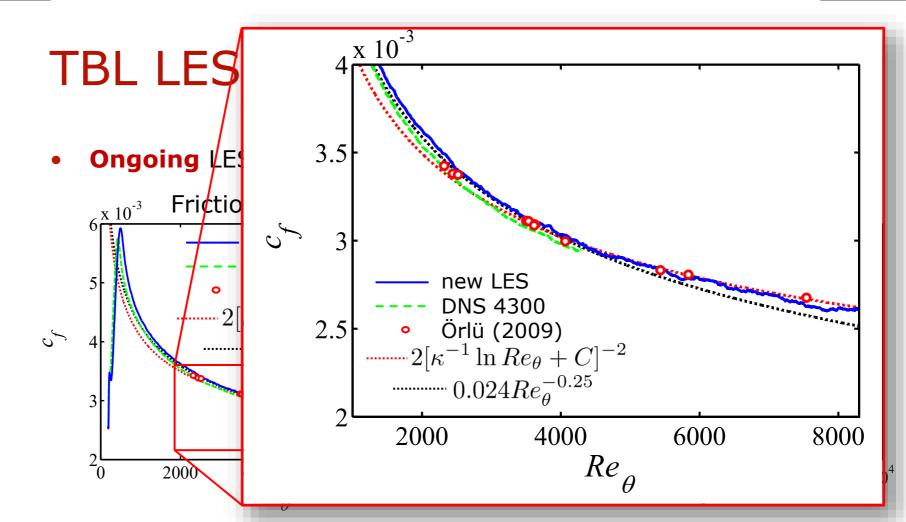
 $Re_{\rm H}$  = 500-8300 ;  $Re_{\tau}$  = 2500

Resolution: 9216 x 513 x 768

(8.5 billion grid points)

 $\Delta x^{+}=18$ ,  $\Delta y^{+}=0.06-16$ ,  $\Delta z^{+}=8$ 





**Domain**:

**ROYAL INSTITUTE** 

OF TECHNOLOGY

13500 x 400 x 540 $\delta_0$ \*

 $Re_{\theta}$  = 500-8300 ;  $Re_{\tau}$  = 2500

Resolution: 9216 x 513 x 768

(8.5 billion grid points)

 $\Delta x^{+}=18$ ,  $\Delta y^{+}=0.06-16$ ,  $\Delta z^{+}=8$ 

 $Re_{\theta}$ =1000

 $Re_{\theta}$ =2500

 $Re_{\theta}$ =4000

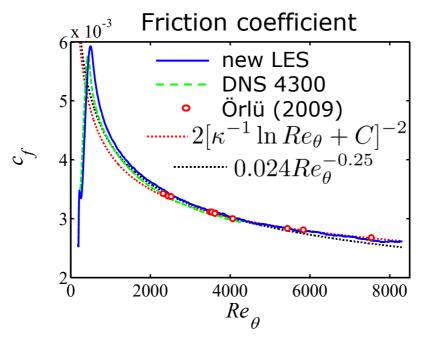
 $Re_{\theta} = 5800$ 

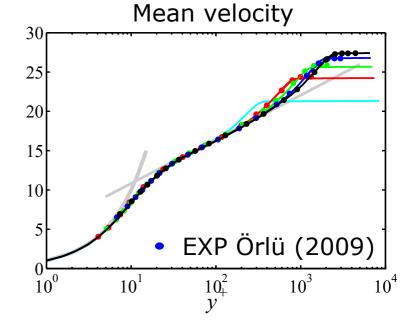
 $Re_{\theta}$ =7500

# TBL LES up to $Re_{\theta}$ =8300

Ongoing LES (using ADM-RT)







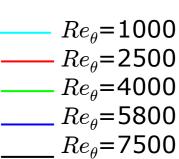
<u>Domain</u>:  $13500 \times 400 \times 540\delta_0^*$ 

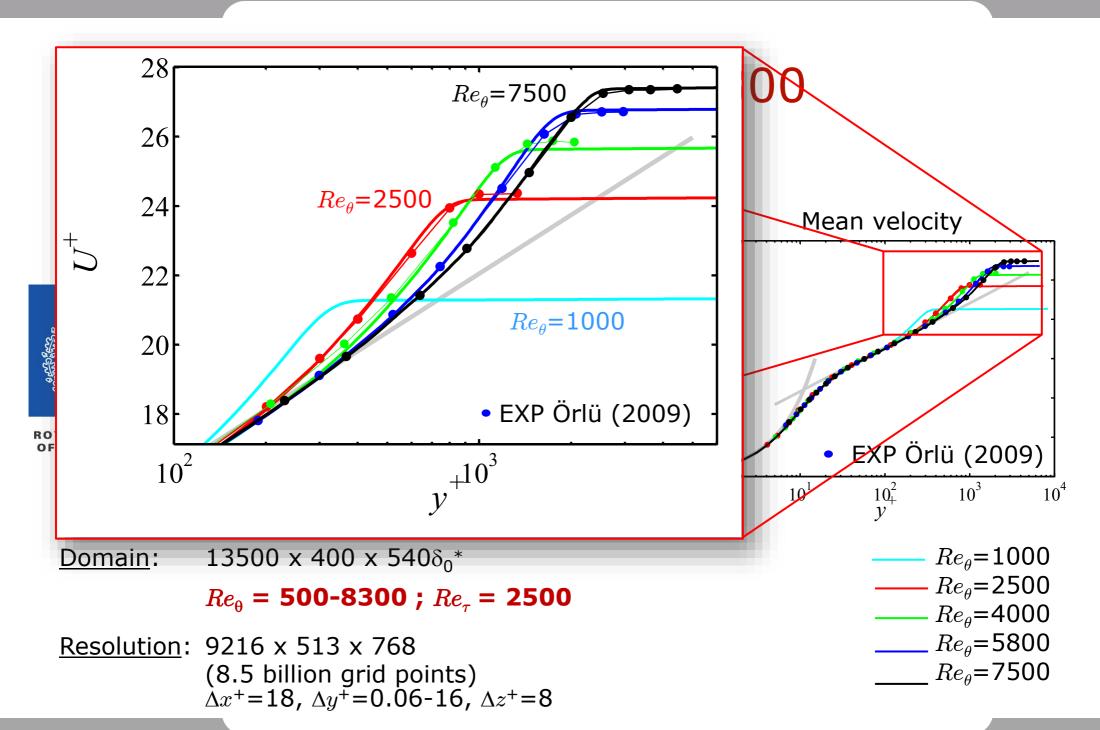
 $Re_{\theta}$  = 500-8300 ;  $Re_{\tau}$  = 2500

Resolution: 9216 x 513 x 768

(8.5 billion grid points)

 $\Delta x^{+}=18$ ,  $\Delta y^{+}=0.06-16$ ,  $\Delta z^{+}=8$ 

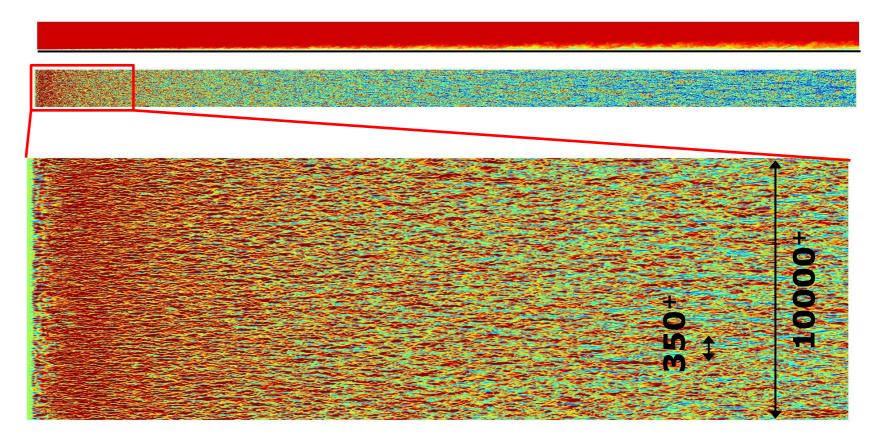




## Visualisation

• Streamwise velocity u in wall-parallel plane  $y^+ {\approx} 15$ 



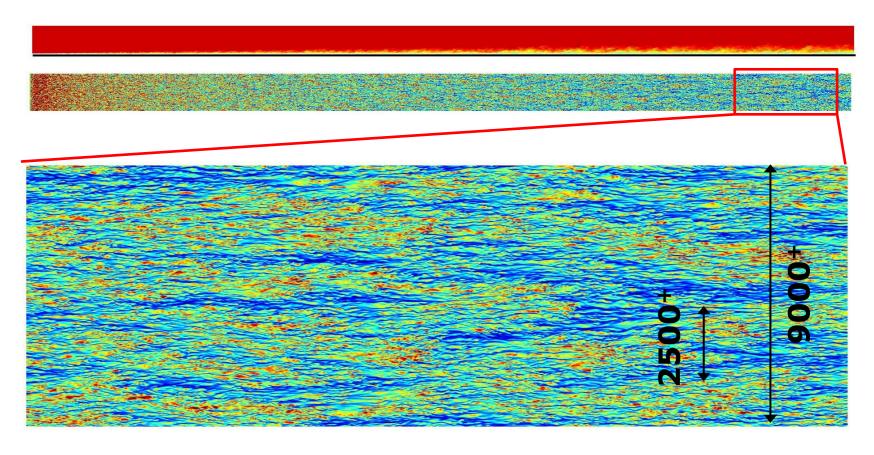


$$Re_{\theta}$$
=180-1400  $Re_{\tau}$ =350

# Visualisation

• Streamwise velocity u in wall-parallel plane  $y^+ {\approx} 15$ 

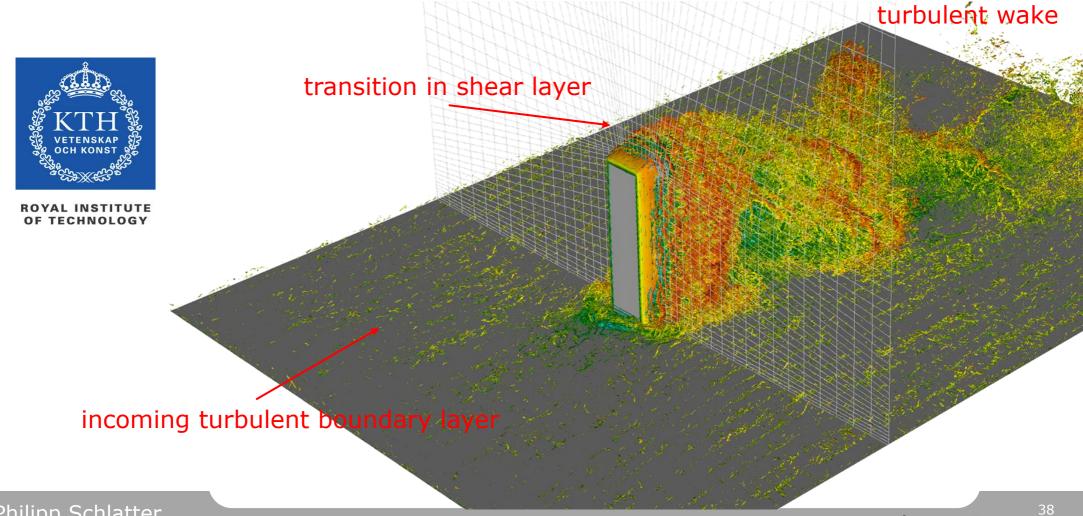




$$Re_{\theta}$$
=8300  $Re_{\tau}$ =2500

# TBL with "obstacles"

"Skyscraper" reference case: Canadian CFD Challenge (2014)



Philipp Schlatter



#### **Outline**

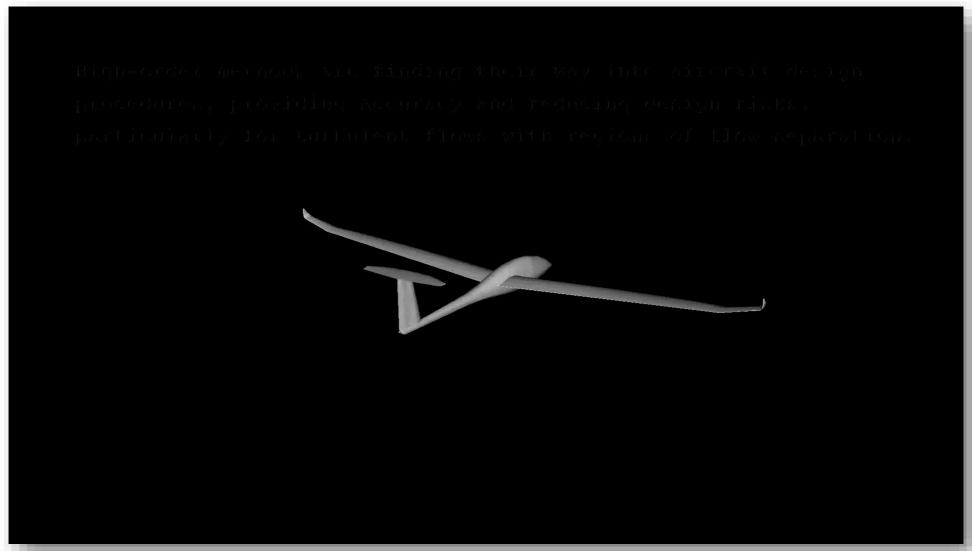
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# DNS of flow around a NACA4412 wing section; $Re_c$ =400 000 and AoA=5°









# Direct numerical simulation of flow over a full NACA4412 wing at $Re_c$ = 400 000

- DNS with Nek5000
- $Re_{\tau}$ =400,  $Re_{\theta}$ =2800
- AoA=5 deg.
- $z_L$ =10% chord

Flow separation

Turbulence on the wing

Transition to turbulence



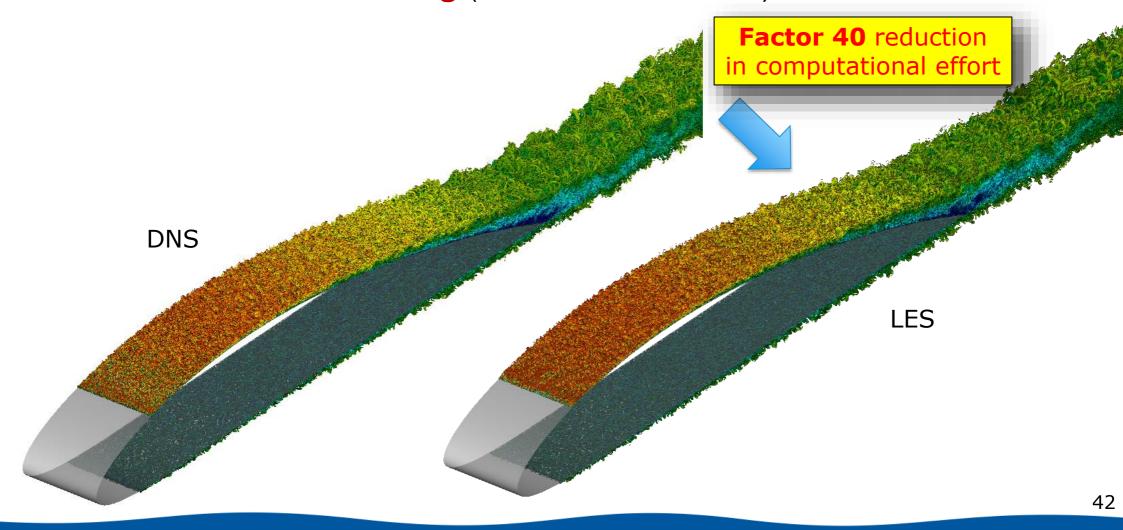
- 3.2 billion grid points
- 35 million CPU hours needed for convergence of turbulence
- 75 TB data, 12 ETT





# LES towards Re = 1M and beyond...

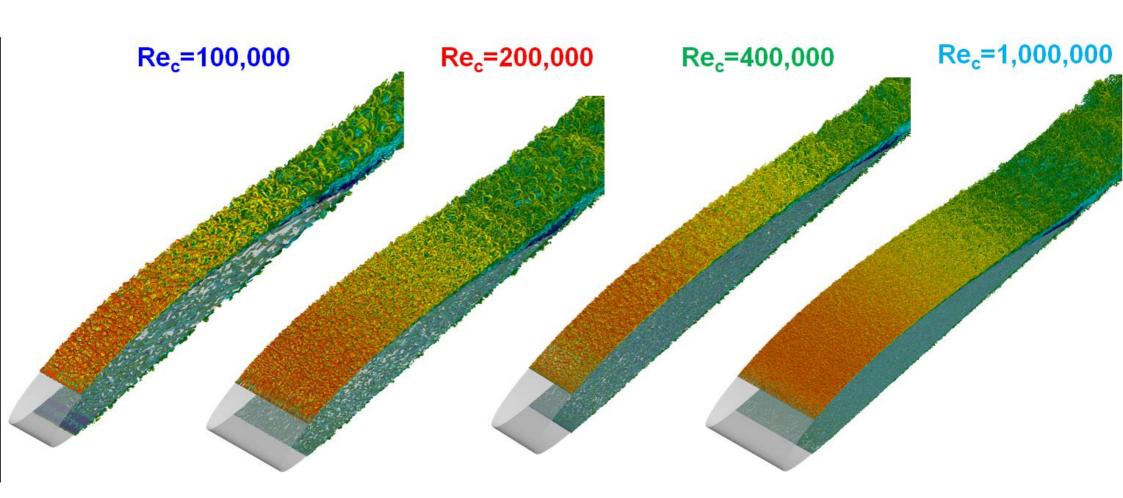
 Similar approach as Eitel-Amor et al. (2014) based on relaxation filtering (Schlatter et al. 2005)



Philipp Schlatter Marine 2019, May 14, 2019



### Four different wings...



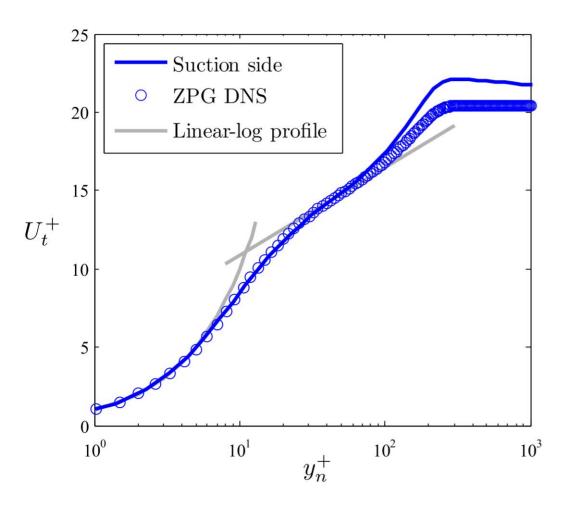


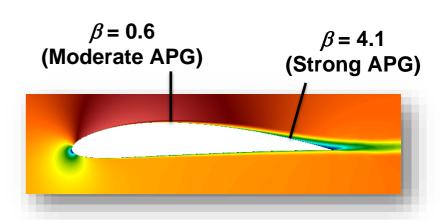
Vinuesa et al. Int. J. Heat Fluid Flow 2018



### Mean velocity profiles

- Inner-scaled **mean flow** at x/c=0.4.





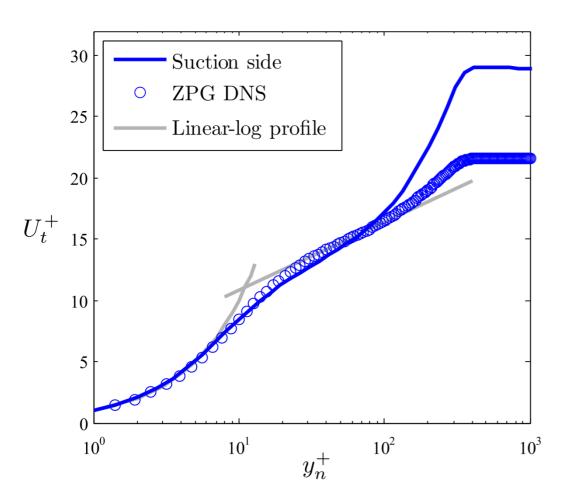
Effect on the outer part, more prominent wake

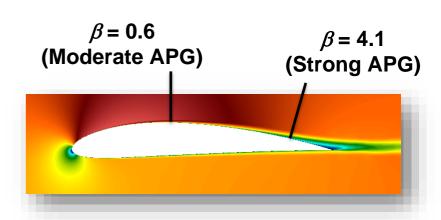
Parameter	At x/c=0.4	ZPG (S&Ö)
$Re_{\scriptscriptstyle{ au}}$	242	252
Re <sub>e</sub>	712	678
Н	1.59	1.47
$C_f$	4.1×10 <sup>-3</sup>	4.8×10 <sup>-3</sup>
κ	0.38	0.42
В	4.20	5.09
П	0.56	0.31



### Mean velocity profiles

- Inner-scaled **mean flow** at x/c=0.8.





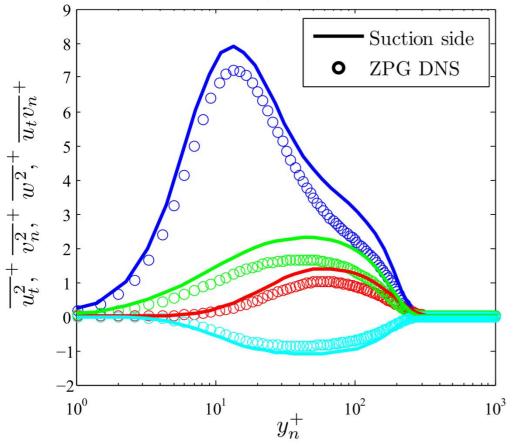
 Effect on the outer part (more prominent wake), but also in the incipient log region and even the buffer layer.

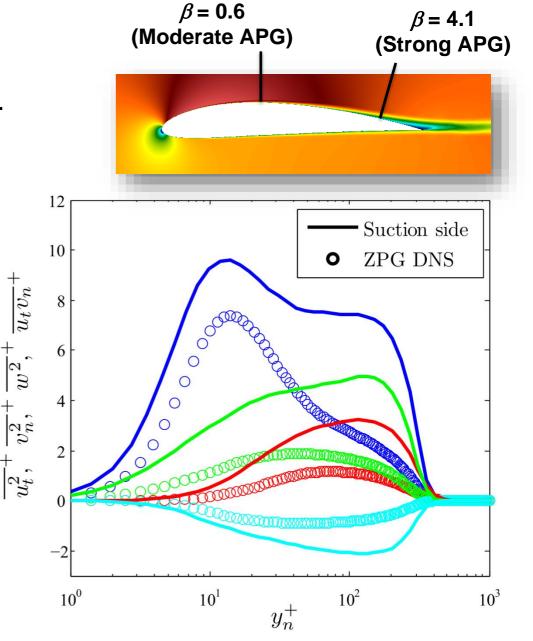
Parameter	At x/c=0.8	ZPG (S&Ö)
$Re_{\scriptscriptstyle{ au}}$	373	359
Re <sub>e</sub>	1,722	1,007
Н	1.74	1.45
$C_f$	2.4×10 <sup>-3</sup>	4.3×10 <sup>-3</sup>
к	0.33	0.41
В	2.08	4.87
П	1.35	0.37



# Reynolds stress tensor components

- Reynolds stress tensor at x/c=0.4 and 0.8.
- Comparison with ZPG from Schlatter and Örlü, 2010.



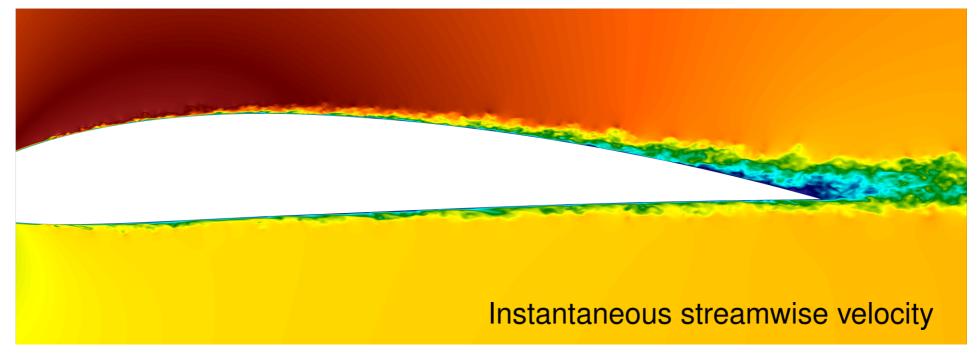




#### **Outline**

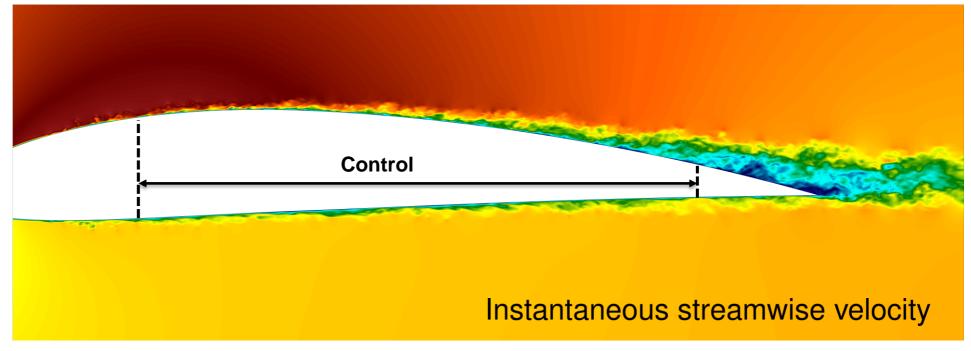
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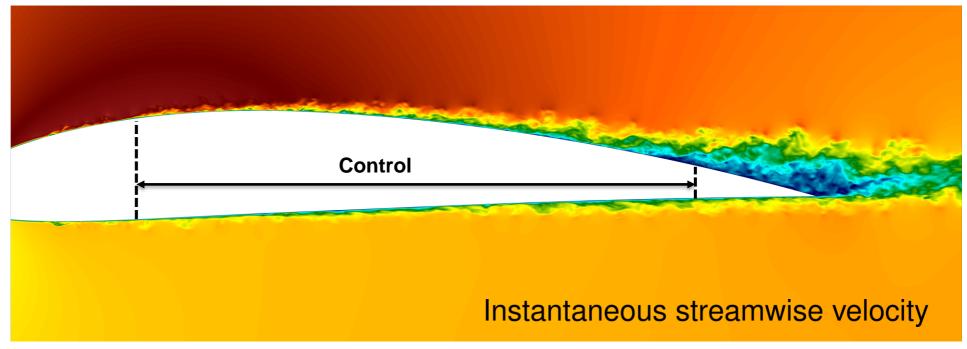
- ullet Reference case: NACA4412,  $Re_c=200,000$
- Controlled case 1: Uniform blowing,  $0.1\%U_{\infty}$ , at  $0.25 < x_c < 0.86$
- Controlled case 1: Uniform blowing,  $0.2\%U_{\infty}$ , at  $0.25 < x_c < 0.86$
- Controlled case 1: Uniform suction,  $0.1\%U_{\infty}$ , at  $0.25 < x_c < 0.86$



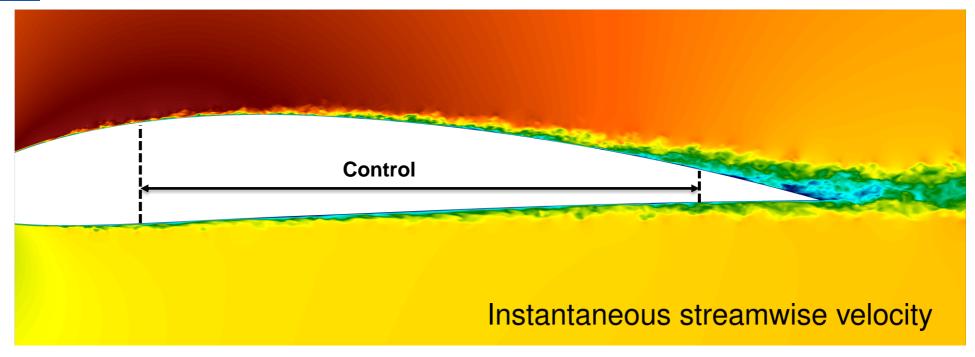


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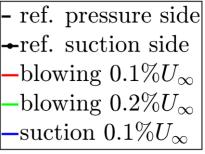


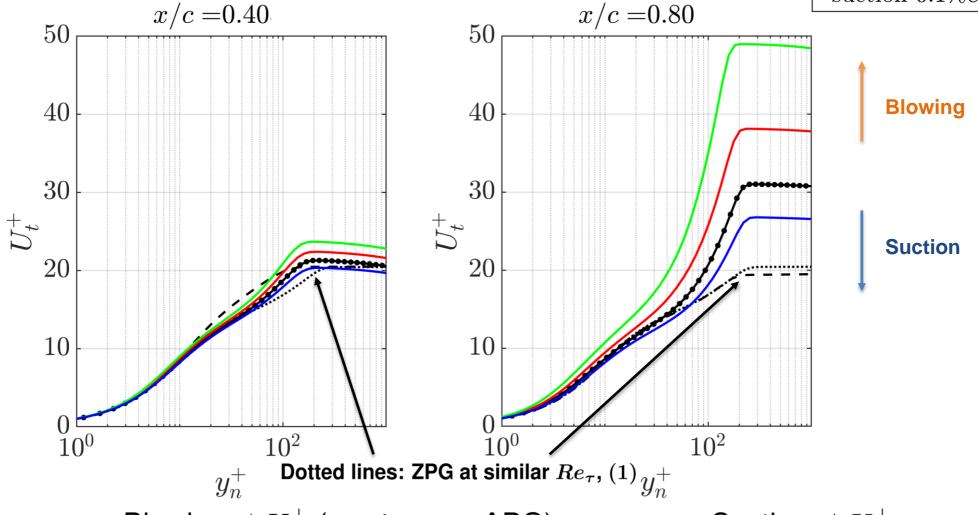
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- ullet Controlled case 1: Uniform suction,  $0.1\% U_{\infty}$ , at  $0.25 < x_c < 0.86$



## Comparison with pressure-gradient effects:

Inner-scaled mean tangential velocity





Blowing:  $\uparrow U_t^+$  (as stronger APG)

Suction:  $\downarrow U_t^+$ 

(1): Schlatter & Örlü, J. Fluid Mech. (2018), 710:5-34

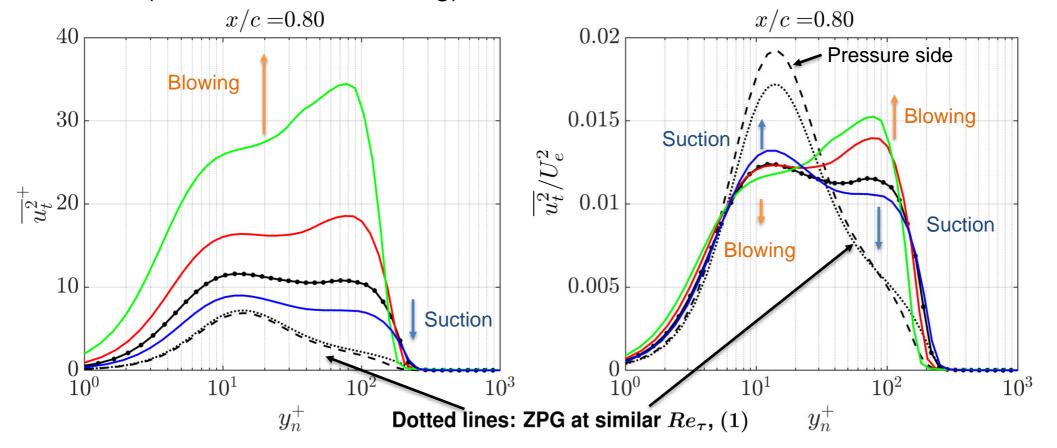


## Comparison with pressure-gradient effects:

ref. suction side blowing  $0.1\%U_{\infty}$  blowing  $0.2\%U_{\infty}$  suction  $0.1\%U_{\infty}$ 

- ref. pressure side

Fluctuations of the tangential velocity component (inner and outer scaling)



Blowing:  $\uparrow \overline{u_t^2}^+$  (as APG) Suction:  $\downarrow \overline{u_t^2}^+$ 

(1): Schlatter & Örlü, J. Fluid Mech. (2018), 710:5-34



#### Effects of the control on the aerodynamic efficiency:

	$c_f$		$c_p$		$C_d$	$C_l$	L/D
ref.	0.0125	+	0.0071	=	0.0196	0.87	44
blowing $(0.1\%U_{\infty})$	<b>0.0119</b> \	+	0.0082 ↑	_	0.0201 ↑	0.84 ↓	<b>42</b> ↓
blowing $(0.2\%U_{\infty})$	$\boldsymbol{0.0115}\downarrow$	+	0.0091 ↑	_	0.0206 ↑	0.82 ↓	<b>40</b> ↓
suction $(0.1\%U_{\infty})$	0.0131 ↑	+	0.0063 ↓	=	0.194 ↓	0.89 ↑	<b>46</b> ↑

- Uniform blowing on the suction side decreases L/D!
- Uniform suction on the suction side improves L/D!

(At this Reynolds number!)



#### **Outline**

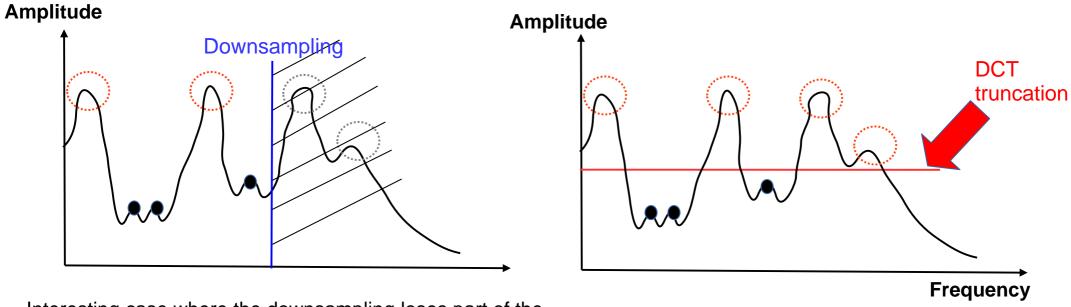
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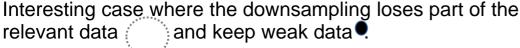




# DCT DATA COMPRESSION ALGORITHM

Novelty: Truncation algorithm based on the amplitude of the modes and not on the frequencies (downsampling).







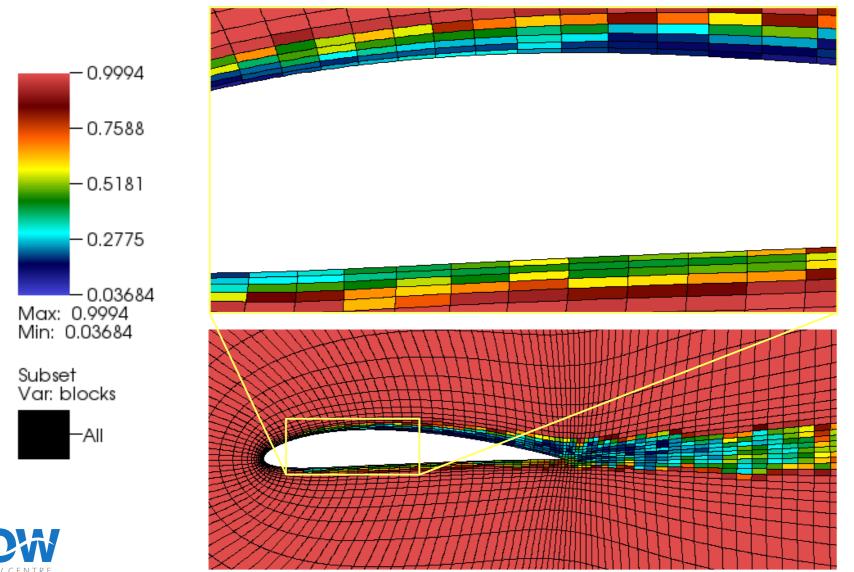
DCT truncation removes data in an adaptive way by removing the weak modes with less contribution to the whole flow representation.





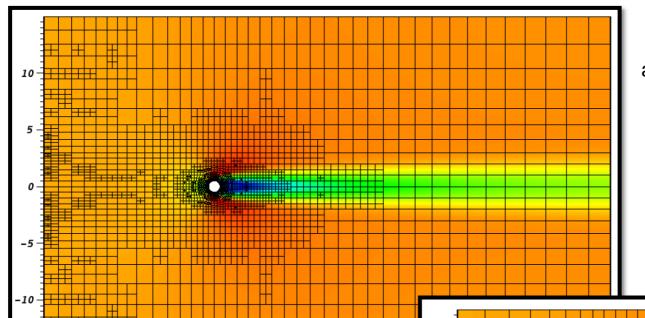
# RESULTS - wing case

Compression ratio (Error: 1e-4, Cr= 90%)



## Adaptive h-refinement (AMR) – 2D cylinder flow





adjoint error estimators

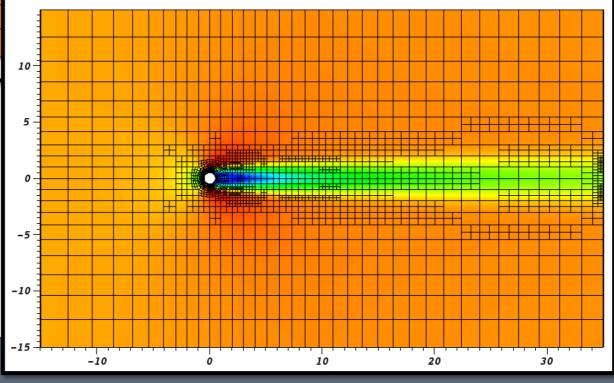
spectral error indicators

Ref. Offermans 2019



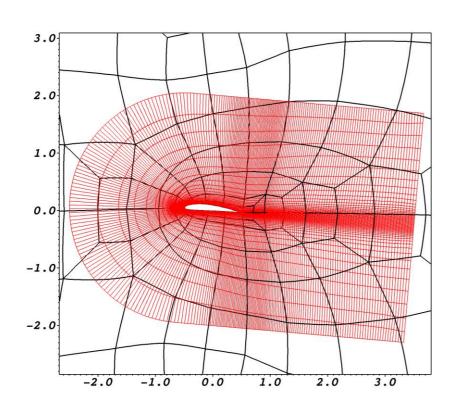
**ExaFLOW** 

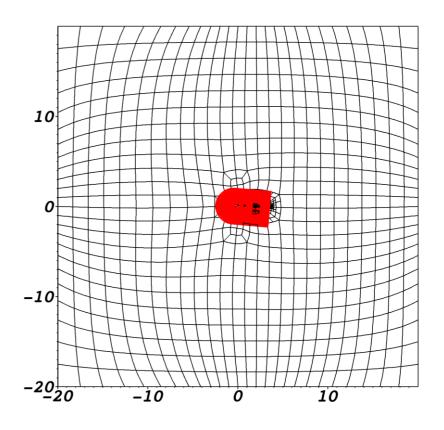
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# 2D AMR NACA4412 $Re_c = 200\,000$







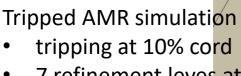
## Comparison of mesh structure

Ref. Offermans 2019

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## 3D AMR NACA4412 $Re_c = 200\,000$





7 refinement leves at trailing edge

5 refinement levels at wing surface

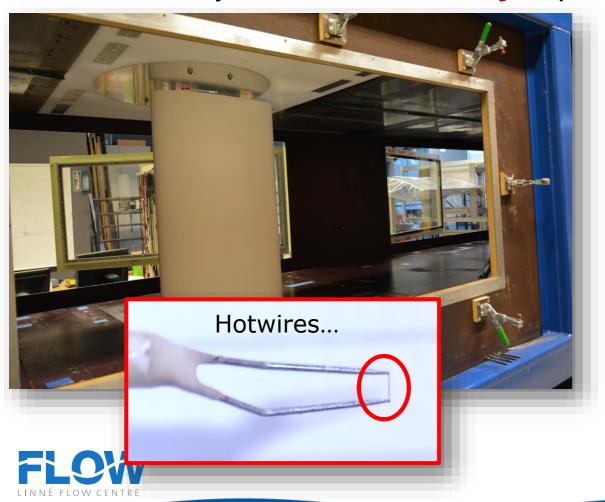
Ref. Tonarro et al. 2019 (TSFP)

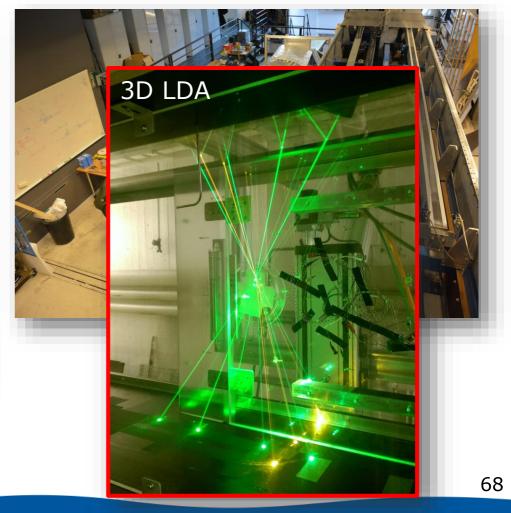
Vørtical structure ( $\lambda_2$  criterion) of velocity field and refinement levels



# "Real Experiments" in the MTL wind tunnel (KTH Mechanics)

- Validation experiments to identify shortcomings
- Reynolds number "only" up to 1.6 M !!!





Philipp Schlatter Marine 2019, May 14



- Large-scale simulations using high-order (spectral) methods
- Numerical databases with **highest** Re in the literature: **DNS**  $Re_c$  = 400 000 and **LES** at  $Re_c$  = 1 000 000
- Non-conformal meshes in Nek5000 with adaptation.
- "Virtual experiments" enables characterisation of complicated flow cases with an unprecedented level of detail:
  - Influence of pressure gradients, comparison to flat plates, tracking of turbulence features, control, ...
  - Experiments in the MTL wind tunnel
- Code development, new computer architectures, ...
- uncertainty analysis for simulations



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