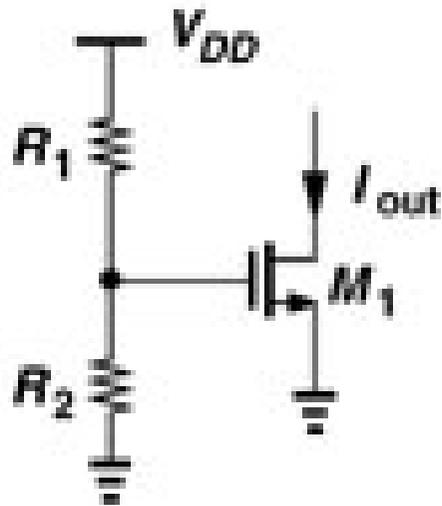


Lecture 4

IL2218 Analog electronics, advanced course

- Chapter 5
- Passive current mirrors
- Active current mirrors
- Examples

Current controlled by voltage V_{GS}



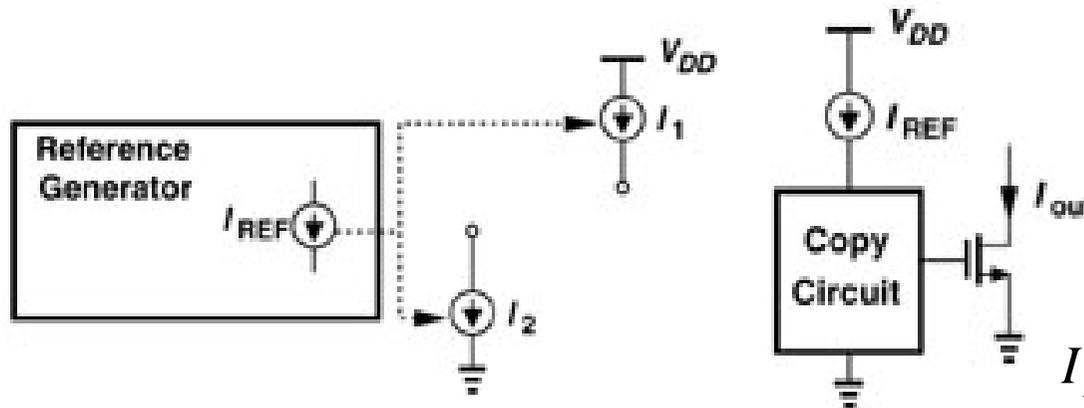
$$V_{GS} = \frac{R_2}{R_2 + R_1} V_{DD}$$

$$I_{OUT} \approx \frac{\mu_n C_{ox}}{2} \frac{W}{L} (V_{GS} - V_{TH})^2$$

Current is controlled by resistive divider

I_{out} is poorly defined because current is depending on process V_{TH} and μ_n , that varies from wafer to wafer. They are also temperature dependent!

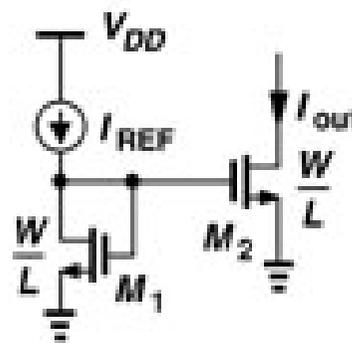
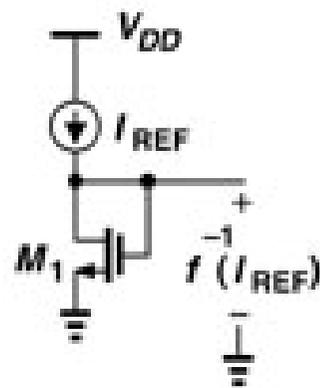
Reference currents



$$I_{REF} = \frac{\mu_n C_{ox}}{2} \left(\frac{W}{L} \right)_1 (V_{GS} - V_{TH})^2$$

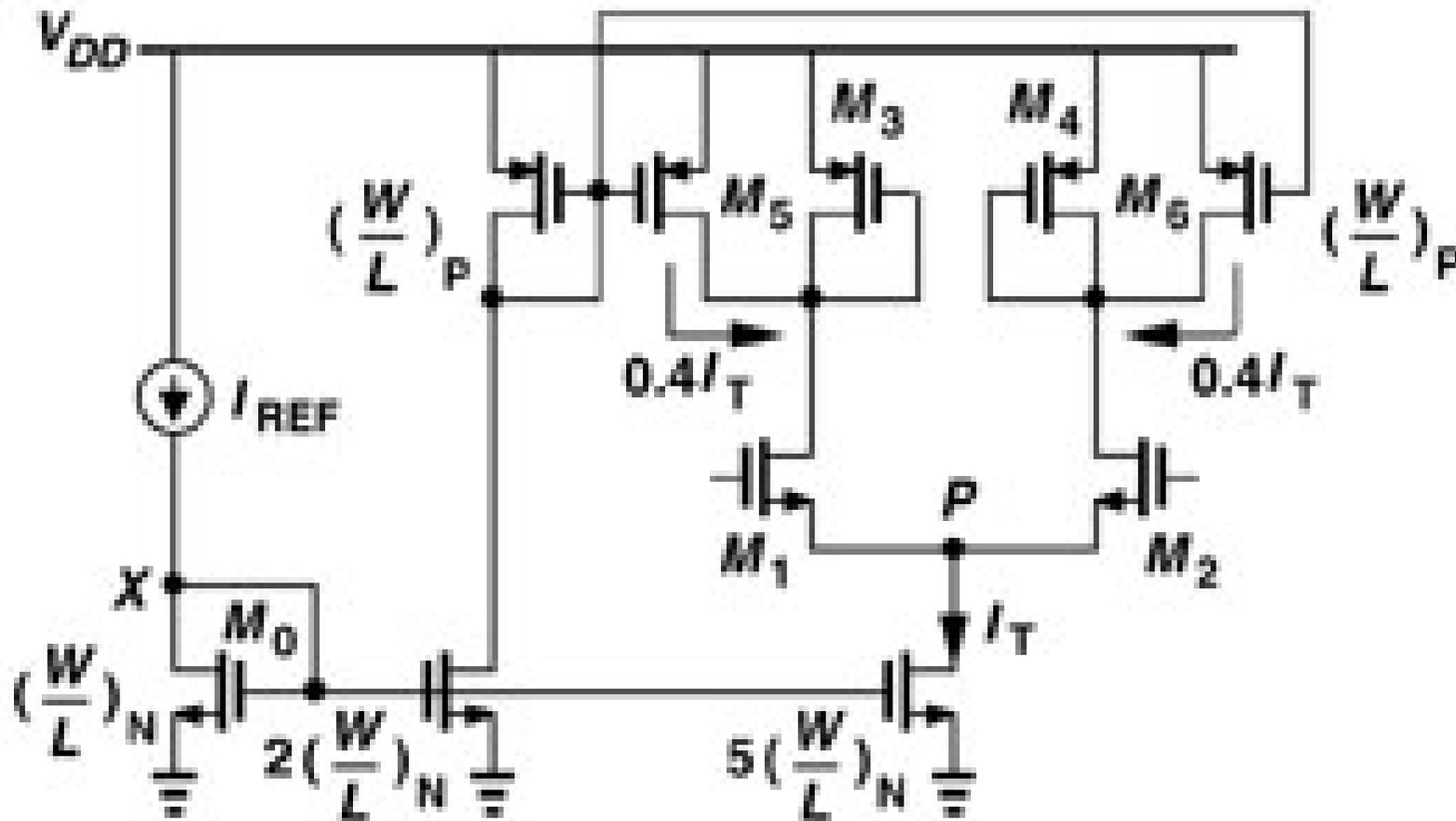
$$I_{out} = \frac{\mu_n C_{ox}}{2} \left(\frac{W}{L} \right)_2 (V_{GS} - V_{TH})^2$$

$$I_{out} = \frac{\left(\frac{W}{L} \right)_2}{\left(\frac{W}{L} \right)_1} I_{REF}$$

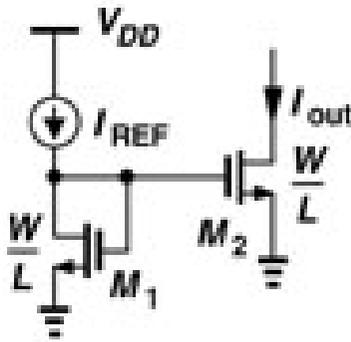


Precise copying of the current with no dependence on process and temperature

Use of current mirrors to bias amplifiers



Channel length modulation

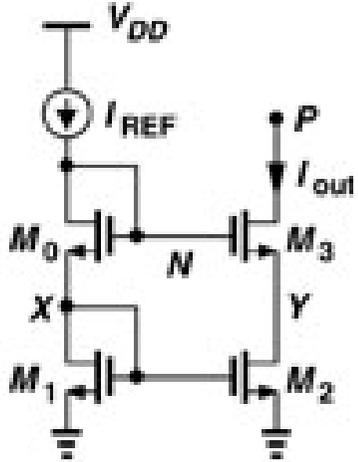
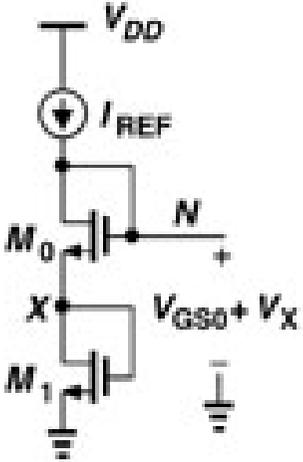
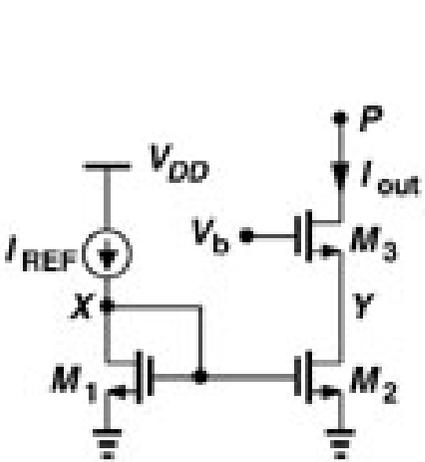


$$I_{REF} = \frac{\mu_n C_{ox}}{2} \left(\frac{W}{L} \right)_1 (V_{GS} - V_{TH})^2 (1 + \lambda V_{DS1})$$

$$I_{out} = \frac{\mu_n C_{ox}}{2} \left(\frac{W}{L} \right)_2 (V_{GS} - V_{TH})^2 (1 + \lambda V_{DS2})$$

$$\frac{I_{out}}{I_{REF}} = \frac{\left(\frac{W}{L} \right)_2 (1 + \lambda V_{DS2})}{\left(\frac{W}{L} \right)_1 (1 + \lambda V_{DS1})}$$

Cascode current mirror



If V_X equals V_Y then I_{out} closely track I_{REF}

$$V_N = V_{GS0} + V_X$$

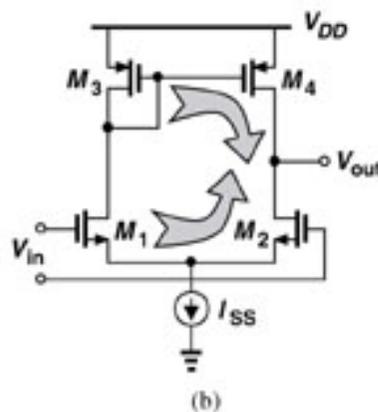
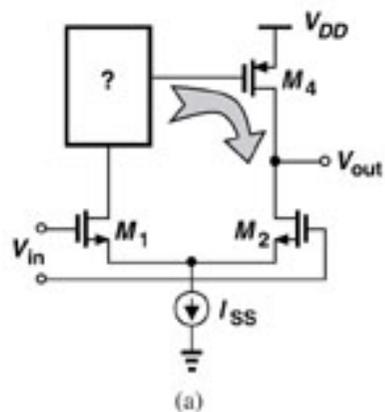
$$V_{GS0} + V_X = V_{GS3} + V_Y$$

Current tracks with proper dimensions of transistors

$$\left(\frac{W}{L}\right)_3 = \left(\frac{W}{L}\right)_2$$

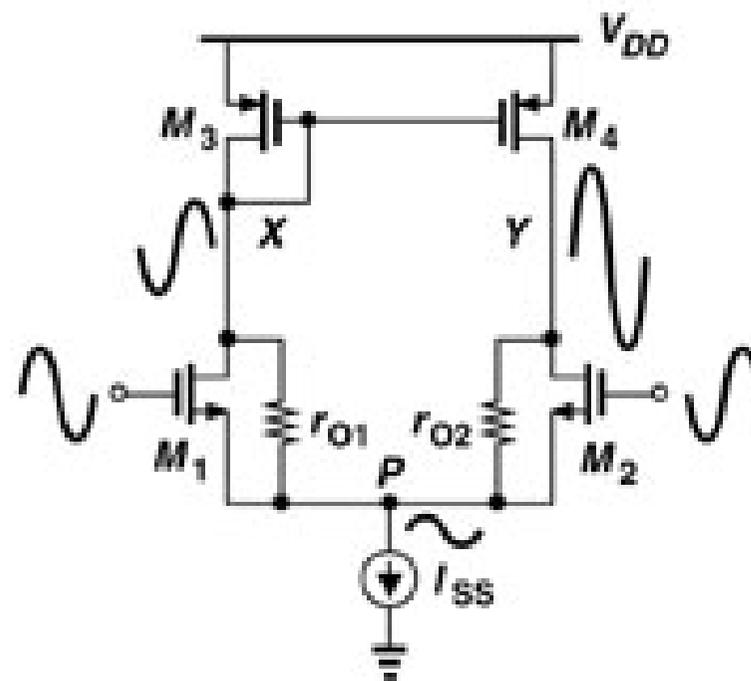
$$\left(\frac{W}{L}\right)_0 = \left(\frac{W}{L}\right)_1$$

Active current mirror

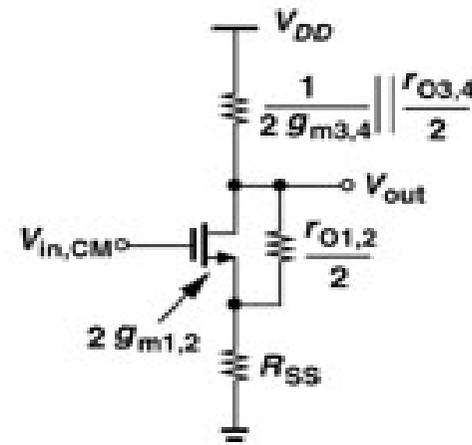
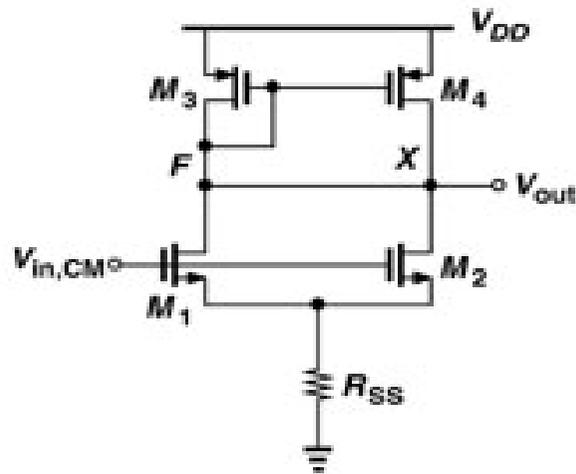


The current is mirrored over to the output side

Small signal gain?



Common mode properties



$$A_{CM} \approx \frac{-\frac{1}{2g_{m3,4}} \parallel \frac{r_{o3,4}}{2}}{\frac{1}{2g_{m1,2}} + R_{SS}} = \frac{-1}{1 + 2g_{m1,2}R_{SS}} \cdot \frac{g_{m1,2}}{g_{m3,4}}$$

$$CMRR = \left| \frac{A_{DM}}{A_{CM}} \right| \approx \frac{g_{m1,2}(r_{o1,2} \parallel r_{o3,4})}{g_{m1,2}} = \frac{g_{m3,4}(r_{o1,2} \parallel r_{o3,4})(1 + 2g_{m1,2}R_{SS})}{g_{m3,4}(1 + 2g_{m1,2}R_{SS})}$$