## Mechanistic Empirical Design Exercise

AC thickness optimization against top down cracking

Teaching assistant: Yared Dinegdae (dinegdae@kth.se)

Road Construction and Maintenance (AF 2903)

Deadline of submission (25/04/2013)

1. The following four layer pavement system has to be checked against top down fatigue cracking. The pavement is subjected to a single-axle dual-wheel load of magnitude 22480pound (100KN) and a tyre pressure of 166psi (800KPa). The spacing between the dual wheels is 12inch (30.5cm) center-to-center. The expected traffic during the design period is 10 million ESALs and it is designed with a reliability of 95%. The design period is 20 years and the pavement is located in an area with a mean annual air temperature (maat) of 75°F. A reference temperature of 50°F should be used to predict aging condition).

The tensile stress at the bottom of the AC layer for the trial pavement system should be calculated based on the following structure. Use English units in the Matlab calculation (inch, psi...)

AC layer:thickness 4.5 inch, AC stiffness, from AC stiffness predictive modelBase layer:thickness 12 inch, modulus 63600 psiSubbase layer:thickness 12 inch, modulus 51000 psiSubgrade:semi-infinite layer 999 inch, modulus 361000 psi

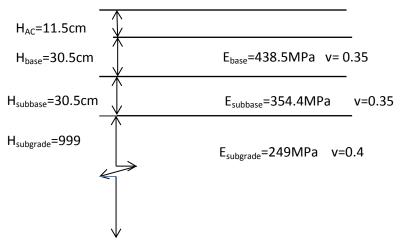


Figure 1 Pavement system

The aging effect on the AC stiffness is considered by dividing the AC layer into sub-layers and since aging is most pronounced close to the surface, the Ac stiffness can be obtained at  $1/8H_{AC}$  and  $1/2H_{AC}$ .

A predictive equation is provided to calculate the AC stiffness, tensile strength and creep parameters at different depths in the AC layer. Use time of loading t=0.1 sec for the AC stiffness prediction and t=1800 sec for tensile strength prediction.

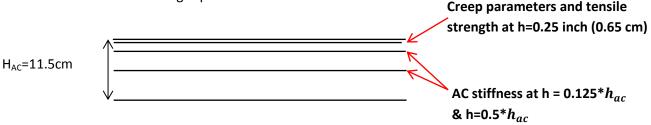


Figure 2 AC layer

Use the following mix gradation, volumetrics and rheological properties of the AC layer as input in the predictive equations.

Gradation (Percent passing by weight)				Volumetric		Rheological properties	
$\rho_{\frac{3}{4}(19mm)}$	$\rho_{\frac{3}{8}(9.5 mm)}$	$ ho_{4(4.75 mm)}$	$ ho_{200(0.075mm)}$	V <sub>a</sub> (%)	$V_{beff}$ (%)	A	VTS
100	93.7	74.6	5.6	3.2	10.7	10.6316	-3.548

## Tasks

- 1. Estimate the energy ratio optimum, *ER*<sub>opt</sub>
  - Uncomment line 13 to 21 in the file *eropt.m* and write the necessary expression for energy ratio optimum for the given reliability

Reliability (%) 
$$ER_{opt} = f(x: ESALs in 10 millions)$$
  
 $x < 0.14$   $0.14 \le x < 0.8$   $x \ge 0.8$   
95  $ER_{opt} = 0.329 x + 0.65$   $ER_{opt} = 0.640 x + 0.61$   $ER_{opt} = 0.256 x + 0.92$ 

- Use traffic, reliability and the file *fcm.m* to determine *ER*<sub>opt</sub>
- 2. Estimate the tensile strength  $S_t$ 
  - Uncomment line 19 and 20 in the file *tensile\_strength.m* and write the necessary expression for the curve fitting parameters (delta and alpha)

$$\begin{split} \delta &= 2.718879 + 0.079524 \times p_{200} - 0.007294 \times (p_{200})^2 + 0.002085 \times \rho_4 \\ &\quad -0.01293 \times V_a + 0.08541 \frac{V_{be}}{V_{be} + V_a} \end{split}$$

$$\begin{split} \alpha &= 3.559267 - 0.005451 \times \rho_4 + 0.020711 \times \rho_{3/8} - 0.000351 \times \left(\rho_{3/8}\right)^2 \\ &+ 0.00532 \times \rho_{3/4} \end{split}$$

 $ho_{3/4},
ho_{3/8},
ho_4$ : percent weight retained on 19mm, 9.5mm and 4.75mm sieve respectively  $ho_{200}$ : percent passing on 0.075 mm sieve

 $V_a$ : Air void  $V_{be}(V_{beff})$ : effective asphalt content

• To determine the tensile strength uncomment line 40 in the same file and write the tensile strength predictive equation, use the regression constants at line 7 & 8 and tensile dynamic modulus at line 39

$$S_t = \sum_{n=0}^5 a_n \cdot \left(\log S_f\right)^n$$

- Use the required inputs and the file *fcm.m* to determine the tensile strength
- 3. Estimate creep parameters  $D_1$  and m
  - Uncomment line 16 and 17 in the file *creep\_parameters.m* and write the necessary expression for the curve fitting parameters (delta and alpha).
  - To determine *D<sub>1</sub> and m* uncomment lines 29 and 31 and write the necessary description for D0 and temp

$$\begin{split} \log\left(\mathrm{D}_{0}\right) &= -\delta - \alpha - \log\lambda_{\mathrm{r}}, \quad \log\left(\mathrm{D}_{0} + \mathrm{D}_{1}\right) = -\delta - \frac{\alpha}{1 + \mathrm{e}^{\beta}} - \log\lambda_{\mathrm{r}} \\ \mathrm{m}_{0} &= \alpha\gamma \times \frac{\exp\left(\beta + 3\gamma\right)}{\left[1 + \exp\left(\beta + 3\gamma\right)\right]^{2}} \qquad \mathrm{m} = \mathrm{m}_{0} + \frac{\kappa}{\log\log\eta} \end{split}$$

- Use the required inputs and the file *fcm.m* to determine **D**<sub>1</sub>*and* **m**
- 4. Determine the AC thickness  $H_{tot}$ 
  - Uncomment line 12 and 13 in the file *AC\_modulus.m* and write the necessary expression for the curve fitting parameters (delta and alpha)
  - Uncomment line 21 and specify depth levels at which the AC Stiffness has to be calculated.
  - Open and run the file *fcm.m* after you have inputted all the necessary inputs to get optimized thickness