

KTH Electrical Engineering

SIMULATION OF ELECTRICITY MARKETS

MONTE CARLO METHODS

Lectures 15-18 in EG2050 System Planning

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COURSE OBJECTIVES

To pass the course, the students should show that they are able to



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 apply both probabilistic production cost simulation and Monte Carlo simulation to calculate expected operation cost and risk of power deficit in an electricity market.

To receive a higher grade (A, B, C, D) the students should also show that they are able to

 create specialised models both for probabilistic production cost simulation and Monte Carlo simulation, and to use the results of an electricity market simulation to judge the consequences of various actions in the electricity market.



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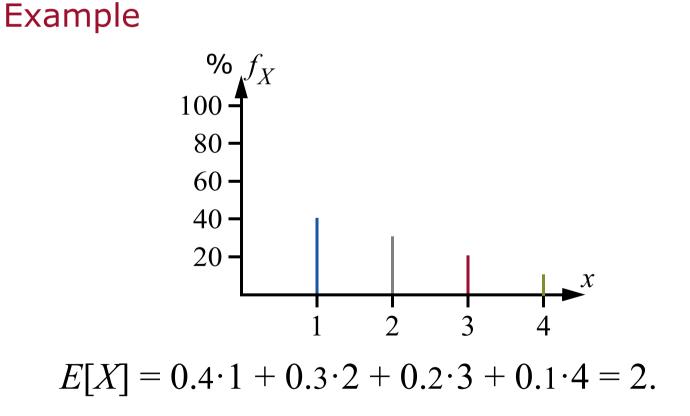
The probability distribution of a random variable can be described using the density function, $f_X(x)$.

The expectation value of a discrete random variable is then

 $E[X] = \sum_{x} x f_X(x).$



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An alternative approach to describe probability distribution is to consider a random variable, X, as a population of individual units:

$$\chi_1, \ldots, \chi_N$$

where

 $\chi_i =$ outcome of X for unit i,

N = number of units in the population.



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Using this alternative approach, the expectation value of a discrete random variable can be written as

$$E[X] = \frac{1}{N} \sum_{i=1}^{N} x_i.$$

Example



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$$E[X] = \frac{1}{10}(1+1+1+1+2+2+2+3+3+4) = 2.$$

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Theorem 6.21. If there are *n* independent observations, $x_1, ..., x_n$, of the random variable *X* then the mean of these observations, i.e.,

$$m_X = \frac{1}{n} \sum_{i=1}^{n} x_i$$

is an estimate of E[X].

Compare
$$E[X] = \frac{1}{N} \sum_{i=1}^{N} X_i$$
 and $m_X = \frac{1}{n} \sum_{i=1}^{n} x_i$.

 Simple sampling means that a limited number of random observations are evaluated instead of the whole population!



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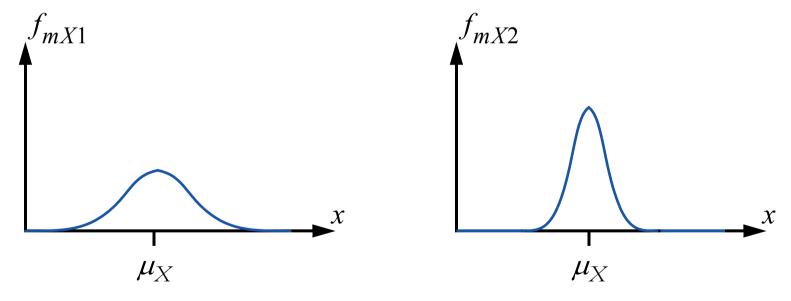
- Notice that the estimate m_X is also a random variable!
- $E[m_X] = E[X]$ (If not, the estimate would be biased.)
- Var[m_X] is given by the following theorem: Theorem 6.22. The variance of the esti-mate from simple sampling is

$$Var[m_X] = \frac{Var[X]}{n}$$
.



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The variance of the estimate, $Var[m_X]$, is interesting because it states how much an estimate might deviate from the true value.



Here m_{X1} is *likely* to be less accurate than m_{X2} .



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SIMPLE SAMPLING - Precision

The practical conclusion of theorem 6.22 is that if the number of samples is increased, it is *likely* that we get a result close to the real value.

Example 6.20—Problem

Let C_i be the result of tossing a coin:

Heads
$$\Rightarrow C_i = 1$$

Tails $\Rightarrow C_i = 0$

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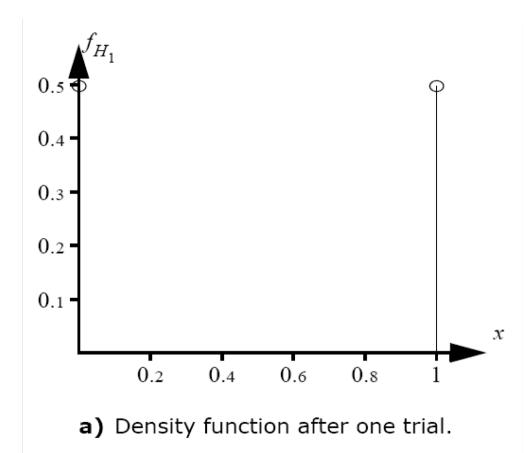
What is the probability distribution of

$$H_n = m_C = \frac{1}{n} \sum_{i=1}^{n} c_i$$
?

Example 6.20—Solution



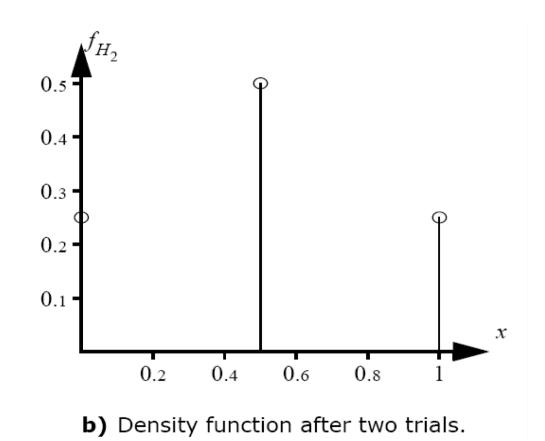
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Example 6.20—Solution



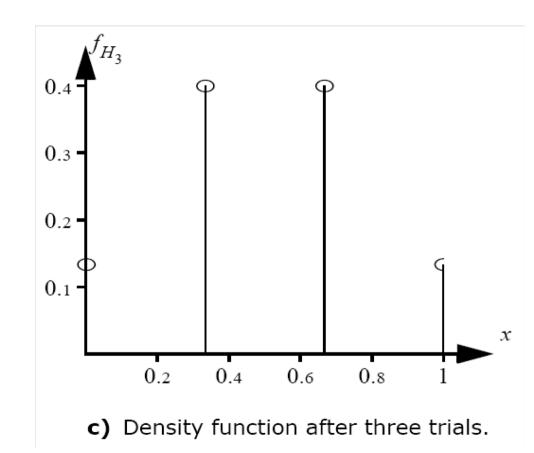
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Example 6.20—Solution



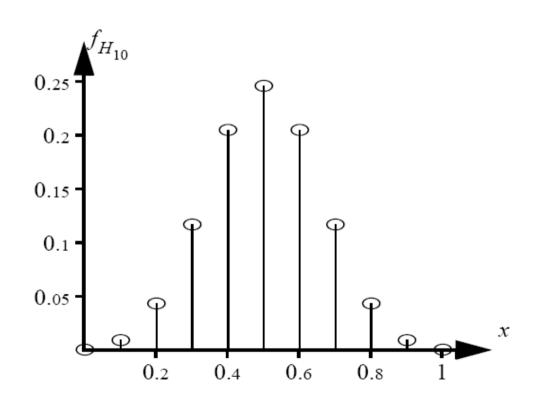
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Example 6.20—Solution



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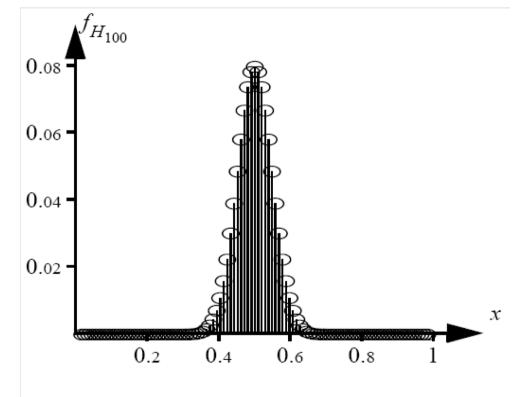


d) Density function after ten trials.

Example 6.20—Solution



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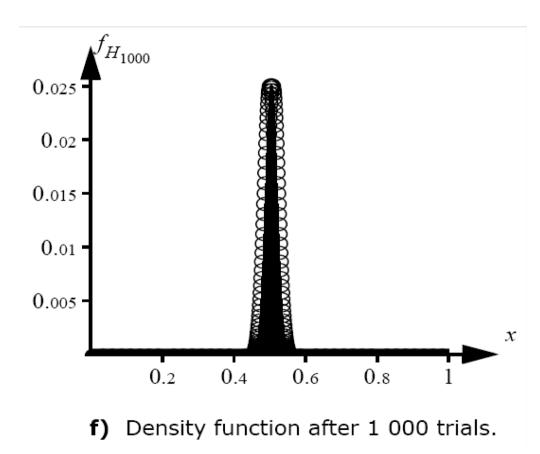


e) Density function after 100 trials.

Example 6.20—Solution



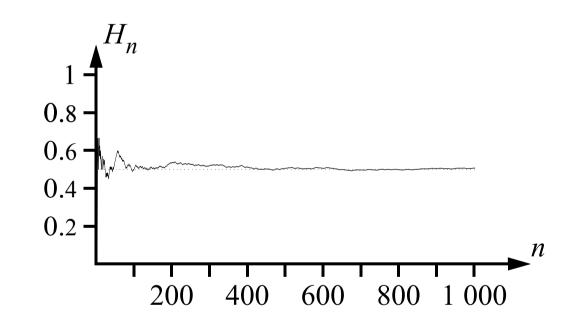
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Example 6.20—Practical test



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How do we know when to stop the sampling?

- Number of samples fixed in advance
- Estimate the precision, for example using the coefficient of variation



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- Convergence criteria

Example 6.21—Problem

- Probabilistic production simulation \Rightarrow $LOLP_{PPC} = 1.0\%$.
- Desired precision: 95% probability that the estimate is within ±0.05% of the true value. This means that if the true *LOLP* is 1.08% then we want the estimate to be in the interval 1.03% to 1.13%.
- The estimate m_{LOLO} is assumed to be normally distributed.



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SIMPLE SAMPLING

- Convergence criteria

Example 6.21—Solution

- The probability is 95% that an $N(\mu, \sigma)$ -distributed random variable belongs to the interval $\mu \pm 1.96\sigma$.
- Here, we want the interval to be $\mu \pm 0.0005$ \Rightarrow The standard deviation of m_{LOLO} must be less than $0.0005/1.96 \approx 0.000255$ \Rightarrow The variance of m_{LOLO} must be less than $0.000255^2 \approx 6.5 \cdot 10^{-8}$.



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Example 6.21—Solution (cont.)

 The variance of m_{LOLO} depends on Var[LOLO], which is unknown but can be estimated using the results from the PPC simulation:

 $Var[LOLO] \approx LOLP_{PPC}(1 - LOLP_{PPC}) =$ = 0.01.0.99 = 0.0099.



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Example 6.21—Solution (cont.)

From theorem 6.22 we now have

$$Var[m_{LOLO}] = \frac{Var[LOLO]}{n}.$$

• $Var[m_{LOLO}] < 6.5 \cdot 10^{-8} \Rightarrow n > 152$ 127.



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Coefficient of variation Definition: The coefficient of variation is

defined as

$$a_X = \frac{\sqrt{Var[m_X]}}{m_X}$$



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SIMPLE SAMPLING

- Convergence criteria

Estimation of accuracy

- Select a few samples.
- Estimate *Var*[X] by

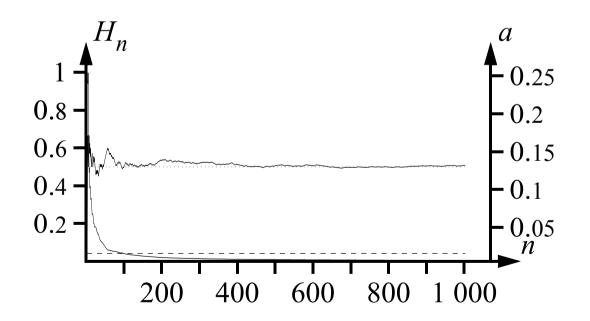
$$s_X^2 = \frac{1}{n} \sum_{i=1}^n (x_i - m_X)^2.$$

• Test if a_X is less than some tolerance limit, ρ . If yes, stop sampling, otherwise generate a few more samples, etc.

Example of using the coefficient of variation



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SIMULATION OF ELECTRICITY MARKETS $\xrightarrow{Y} g(Y) \xrightarrow{X}$



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- The scenario parameters, *Y*, have known probability distributions.
- The result variables, *X*, have unknown probability distributions.
- We are primarily interested in system indices, which are defined as expectation values of some result variables.

SIMULATION OF ELECTRICITY MARKETS

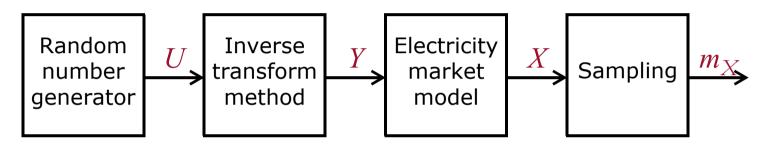


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Result variable

TOC LOLO ENS System index ETOC LOLP EENS

SIMPLE SAMPLING OF ELECTRICITY MARKETS





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- Generate random numbers from uniform distribution
- Transform random numbers into appropriate probability distributions of the scenario parameters
- Determine how electricity market behaves in the scenario
- Sample the result variables

RANDOM NUMBER GENERATION



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- Pseudorandom number generators are mathematical function which given a seed generates a sequence of numbers.
- A good pseudorandom number generator produces a sequence which closely mimics the properties of a U(0, 1)-distribution.
 Without knowledge of the pseudorandom number generator and the seed it is hardly possible to predict the next number in the sequence.
- Pseudorandom number generators are available in most programming languages.

TRANSFORMATION OF RANDOM NUMBER



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It is not likely that the scenario parameters are U(0, 1)-distributed; hence, the output of the random number generator must be transformed to the appropriate probability distribution.

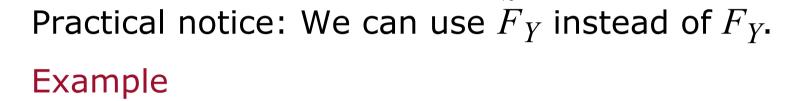
This can be done using the inverse transform method:

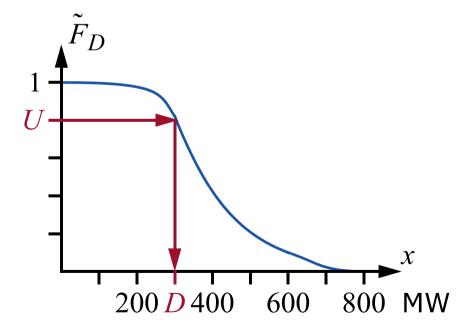
Theorem E.1. If a random variable U is U(0, 1)-distributed then the random variable $Y = F_Y^{-1}(U)$ has the distribution function $F_Y(x)$.

TRANSFORMATION OF RANDOM NUMBER

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TRANSFORMATION OF RANDOM NUMBER



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The inverse of the distribution function of the normal distribution, $\Phi(x)$, does not exist!

 \Rightarrow Use an approximation of $\Phi^{-1}(x)$ instead.

This method is called the approximate inverse transform method and is described in theorem E.2 in the compendium.

ELECTRICITY MARKET MODEL

• A Monte Carlo simulation is not restricted to a specific electricity market model.



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 The complexity of the electricity market model is only limited by the computation time.



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ELECTRICITY MARKET MODEL

• In mathematical terms, the electricity market model is a function

 $x_i = g(y_i),$

where

 x_i = result variables for scenario i,

 y_i = scenario parameters of scenario i,

• In most cases the function g cannot be formulated explicitly, but must be indirectly defined from the solution to an optimisation problem.

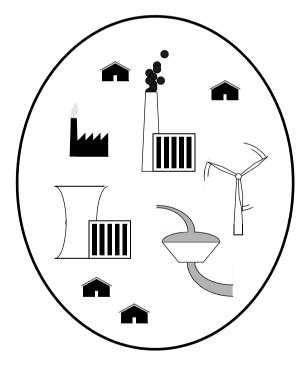
ELECTRICITY MARKET MODEL - PPC model



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Assume

- Perfect competition
- Perfect information
- Load is not price sensitive
- Neglect grid losses and limitations
- All scenario parameters can be treated as independent



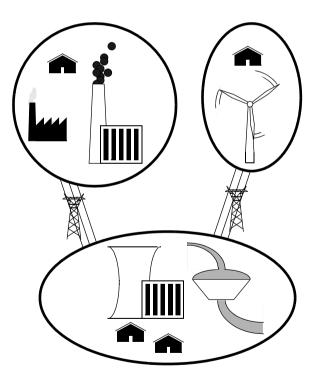
ELECTRICITY MARKET MODEL - Multi-area model



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Assume

- Perfect competition
- Perfect information
- Load is not price sensitive
- Transmission grid losses and limitations included
- Distribution grid losses and limitations neglected



System data



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- Thermal units:
 - Oil condensing, 300 MW, 280 ×/MWh, 95% availability, located in North
 - Nuclear, 1 000 MW, 100 ×/MWh, 90% availability, located in South
 - Bio mass condensing, 400 MW, 180 ×/MWh, 95% availability, located in *South*

System data (cont.)



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- Non-dispatchable units:
 - Run-of-the-river hydro, 2 000 MW (80%), 1 900 MW (10%), 1 800 MW (10%), negligible operation cost, located in *North*
 - Wind farm, 100 MW (10%), 80 MW (5%), 60 MW (10%), 40 MW (15%), 20 MW (25%), 0 MW (35%), negligible operation cost, available capacity 0 MW (35%), located in *Isle*

System data (cont.)



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- Transmission lines:
 - AC line between *North* and *South*, 1 200 MW, 4% losses, 100% availability
 - HVDC link from *South* to *Isle* (one direction only!), 200 MW, 2% losses, 100% availability
- Load:
 - North: N(600,100)
 - South: N(2000,300)
 - *Isle*: *N*(100,20)

(No correlations, no price sensitivity, no compensation paid for disconnected load.)

Problem



Formulate a multi-area model for the system and show how the result variables *TOC*, *LOLO* and *ENS* are calculated.

Solution

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Parameters

 $D_n =$ load in area n (scenario parameter—will be randomised during simulation),

Solution (cont.)

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- \overline{G}_g = available generation capacity in thermal unit g (scenario parameter—will be randomised during simulation),
- $\overline{P}_{n, m}$ = maximal transmission

from area n to area m =

 $=\begin{cases} 1\ 200 & n = 1, m = 2, \\ 1\ 200 & n = 2, m = 1, \\ 200 & n = 2, m = 3, \end{cases}$

Solution (cont.)



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 \overline{W}_n = available non-dispatchable generation capacity in area n (scenario parameter—will be randomised during simulation),

 β_{Gg} = operation cost in thermal unit g =

$$=\begin{cases} 280 & g = 1, \\ 100 & g = 2, \\ 180 & g = 3, \end{cases}$$

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Solution (cont.)

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 $\beta_{Ln, m} =$ loss coefficient for transmission from area n to area m =

$$=\begin{cases} 0.04 & n = 1, m = 2, \\ 0.04 & n = 2, m = 1, \\ 0.02 & n = 2, m = 3, \end{cases}$$

 β_{Un} = penalty for unserved load in area n = 500, n = 1, 2, 3.

Solution (cont.)

Optimisation variables

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 G_g = generation in thermal unit g, g = 1, 2, 3,

 $P_{n, m}$ = transmission from area *n* to area *m*, (*n*, *m*) = (1, 2), (2, 1), (2, 3),

 U_n = unserved load in area n, n = 1, 2, 3, W_n = generation in non-dispatchable unit n, n = 1, 3.

3

Solution (cont.)

Objective function



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Constraints

Load balance in *North*:

3

$$G_1 + W_1 + 0.96P_{2,1} = D_1 - U_1 + P_{1,2}$$

minimise $\sum \beta_{Gg}G_g + \sum \beta_{Un}U_n$.

g = 1 n = 1

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Solution (cont.)

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Load balance in *South*: $G_2 + G_3 + 0.96P_{1,2} = D_2 - U_2 + P_{2,1} + P_{2,3}$. Load balance in *Isle*:

 $W_3 + 0.98P_{2,3} = D_3 - U_3.$

Solution (cont.) Variable limits



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$$\begin{split} & 0 \leq G_g \leq \overline{G}_g, \qquad g = 1, 2, 3, \\ & 0 \leq P_{n,m} \leq \overline{P}_{n,m}, (n,m) = (1,2), (2,1), (2,3), \\ & 0 \leq U_n \leq D_n, \qquad n = 1, 2, 3, \\ & 0 \leq W_n \leq \overline{W}_n, \qquad n = 1, 3. \end{split}$$

Solution (cont.)



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The result variables are calculated by solving the optimisation problem for the specific values of the scenario parameters and then calculate

$$TOC = \sum_{\substack{g = 1 \\ 3}} \beta_{Gg} G_{g'}$$
$$g = 1$$
$$3$$
$$ENS = \sum_{n=1}^{3} U_{n'}$$
$$n = 1$$

1

Solution (cont.)



$$LOLO = \begin{cases} 0 & \text{if } ENS = 0, \\ 1 & \text{if } ENS > 0. \end{cases}$$

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HOME ASSIGNMENTS PART IV - Hints



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Problem 22

Define multi-area model.

- State probability distribution of scenario parameters.
- State value of model constants.
- Formulate optimisation problem.
- Show how the result variables *TOC* and *LOLO* are calculated from the solution to the optimisation problem.

MONTE CARLO SIMULATION - Example system



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- Run-of-the-river hydro, 150 kW, 100% availability, negligible operation cost
- Diesel generator set, 40–100 kW, 100% availability, 1 ×/kWh
- Diesel generator set, 0–50 kW, 100% availability, 2 ×/kWh
- Load N(180, 40)-distributed [kW]
- Dummy load (water heater) can absorb surplus generation

Example 6.22 (simple sampling)

In our example system, we need to consider

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- One scenario parameter, D (the load), i.e., Y = [D].
- One result variable, TOC (operation cost),
 i.e., X = [TOC].

Example 6.22 (cont.)



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• The electricity market model is the explicit function X = g(Y), where

$$g(Y) = \begin{cases} 0 & Y \le 150, \\ 2(Y-150) & 150 < Y \le 170, \\ 40 & 170 < Y \le 190, \\ Y-150 & 190 < Y \le 250, \\ 100+2(Y-250) & 250 < Y \le 300, \\ 200 & 300 < Y. \end{cases}$$

Example 6.22 (cont.)



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To randomise a scenario, we generate a U(0, 1)distributed random number and transform it to an N(180, 40)-distribution.

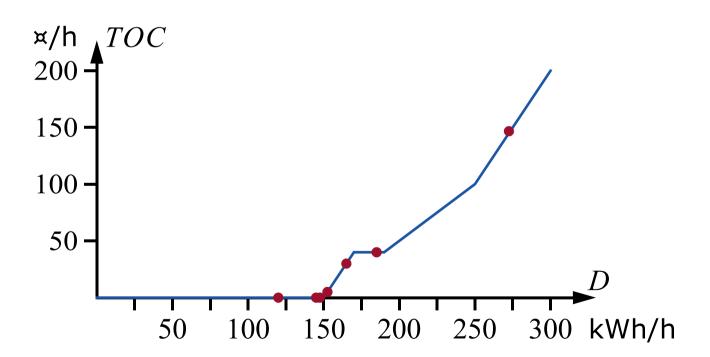
Scenario, i	1	2	3	4	5	6	7	8	9	10
<i>D</i> [kWh/h]	165	273	144	147	185	147	225	120	147	152
TOC [¤/h]	30	146	0	0	40	0	75	0	0	4

$$m_{TOC} = \frac{1}{10} \sum_{i=1}^{10} toc_i = \dots = 29.50$$

Example 6.22 (cont.)



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Example 6.22 (cont.)

- True value: ETOC = 39.66 x/h.
- Estimate from simple sampling: $m_{TOC} = 29.50 \text{ x/h.}$



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HOME ASSIGNMENTS PART IV - Hints



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Problem 23

Apply simple sampling.

- Analyse scenarios using the multi-area model from problem 22.
- Estimate *ETOC* and *LOLP*.

MONTE CARLO SIMULATION - Efficiency



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- A huge number of samples might be necessary to obtain a reasonable accuracy ⇒ long computation time.
- However, we might have some information about the simulation results already before we start sampling.
- Sometimes the information can be used to improve the accuracy (i.e., reduce $Var[m_X]$).

MONTE CARLO SIMULATION - Efficiency



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 Methods to reduce Var[m_X] are referred to as variance reduction techniques.

In this course we will consider three variance reduction techniques:

- Complementary random numbers
- Control variates
- Stratified sampling



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- Assume that m_{X1} and m_{X2} are two separate estimates of μ_{X} , i.e., $E[m_{X1}] = E[m_{X2}] = \mu_X$.
- The mean of these two estimates, i.e., $(m_{X1} + m_{X2})/2$, is also an estimate of μ_X , because

$$E\left[\frac{m_{X1} + m_{X2}}{2}\right] = \frac{1}{2}(E[m_{X1}] + E[m_{X2}]) = \frac{1}{2}(\mu_X + \mu_X) = \mu_X.$$



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• How good is the new estimate? Study

$$\begin{aligned} &Var\left[\frac{m_{X1}+m_{X2}}{2}\right] = \frac{1}{4}Var[m_{X1}+m_{X2}] = \\ &= \frac{1}{4}(Var[m_{X1}]+Var[m_{X2}]+2Cov[m_{X1},m_{X2}]). \end{aligned}$$



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If m_{X1} and m_{X2} are obtained from two separate simulations using simple sampling with n samples in each simulation, then Var[m_{X1}] = Var[m_{X2}] and Cov[m_{X1}, m_{X2}] = 0 ⇒

$$Var\left[\frac{m_{X1}+m_{X2}}{2}\right]=\ldots=\frac{Var[m_{X1}]}{2}.$$

Cf. theorem 6.22: Twice as many samples should cut the variance of the estimate in half.



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• However, if m_{X1} and m_{X2} are negatively correlated, the variance of the estimate can be lower than for simple sampling. If we have n samples in each simulation, then $Var[m_{X1}] = Var[m_{X2}]$ and $Cov[m_{X1}, m_{X2}] < 0 \Rightarrow$

$$Var\left[\frac{m_{X1} + m_{X2}}{2}\right] = \dots =$$
$$= \frac{Var[m_{X1}]}{2} + \frac{1}{2}Cov[m_{X1}, m_{X2}]$$



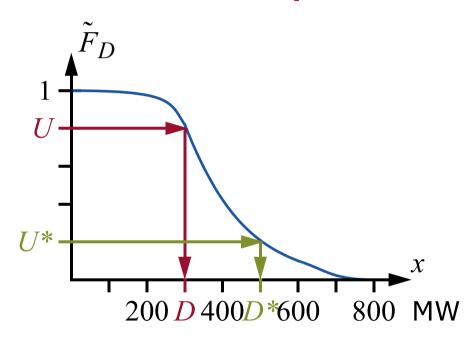
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How do we get negatively correlated estimates?

- Let *U* (the original random number) be U(0, 1)-distributed.
- Then U* = 1 U (the complementary random number) is also U(0, 1)-distributed.
- U and U* are negatively correlated $(\rho_{U, U^*} = -1)$.
- $Y = F_Y^{-1}(U)$ and $Y^* = F_Y^{-1}(U^*)$ will also be negatively correlated ($\rho_{Y, Y^*} \ge \rho_{U, U^*}$).



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- X = g(Y) and $X^* = g(Y^*)$ will also be negatively correlated ($\rho_{X, X^*} \ge \rho_{Y, Y^*} \ge \rho_{U, U^*}$).
- If m_{X1} is based on observations of X and m_{X2} is based on observations of X^* then m_{X1} and m_{X2} will also be negatively correlated.



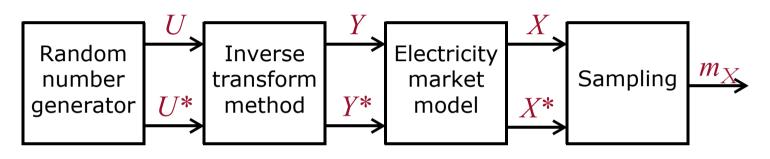
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Practical observation:

$$m_{X1} = \frac{1}{n} \sum_{i=1}^{n} x_i, m_{X2} = \frac{1}{n} \sum_{i=1}^{n} x_i^*$$

$$\Rightarrow \frac{m_{X1} + m_{X2}}{2} = \frac{1}{2n} \sum_{i=1}^{n} (x_i + x_i^*).$$

Hence, there is no need to differentiate between samples based on original and complementary random numbers respectively.





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- Generate random numbers from uniform distribution (original and complementary)
- Transform all random numbers into appropriate probability distributions of the scenario parameters
- Determine how electricity market behaves in original and complementary scenarios
- Sample the result variables



If there are S scenario parameters then we can create in total 2^S scenarios on various combinations of original and complementary random numbers.

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Example

Two scenario parameters, G and D:

- Original scenario: \overline{G} , D
- Complementary scenarios: \overline{G} , D^* , \overline{G}^* , D, \overline{G}^* , D^*



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- Generating too many complementary scenarios might be inefficient.
- Hence, we should only generate complementary random numbers for those scenario parameters where the negative correlation between Y and Y* will be detectable in the result variables!



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COMPLEMENTARY RANDOM NUMBERS - Implementation

Example: Complementary random numbers for multi-area model

- The total load, $D_{tot} = \Sigma D_n$, has a stronger correlation to TOC than the individual area loads, D_n .
- Randomise the total load D_{tot} and its complementary random number D^*_{tot} .
- Randomise two sets of preliminary loads in the areas, D_n^i and D_n^{ii} respectively.

COMPLEMENTARY RANDOM NUMBERS - Implementation



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Example (cont.)

 Finally, scale the preliminary area loads so that they match the total load, i.e.,

T

Scenario 1:
$$D_n = \frac{D_{tot}}{\sum_{m \in \mathcal{N}} D_m^i} D_n^i$$

Scenario 2: $D_n = \frac{D_{tot}^*}{\sum_{m \in \mathcal{N}} D_m^{ii}} D_n^{ii}$

COMPLEMENTARY RANDOM NUMBERS - Example

Example 6.26



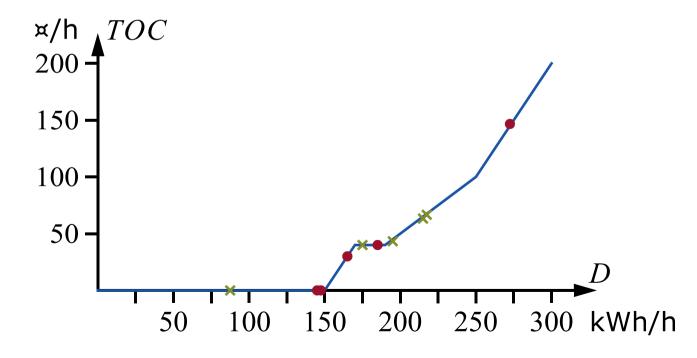
Scenario, i	1	2	3	4	5
<i>D</i> [kWh/h]	165	273	144	147	185
TOC [¤/h]	30	146	0	0	40
Scenario, i	6	7	8	9	10
<i>D</i> * [kWh/h]	195	87	216	213	175
<i>TOC</i> * [¤/h]	45	0	66	63	40

$$m_{TOC} = \frac{1}{10} \sum_{i=1}^{10} toc_i = \dots = 43.00$$

COMPLEMENTARY RANDOM NUMBERS - Example

Example 6.26 (cont.)





COMPLEMENTARY RANDOM NUMBERS - Example



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Example 6.26 (cont.)

- True value: ETOC = 39.66 x/h.
- Estimate from simple sampling: $m_{TOC} = 29.50 \text{ x/h}.$
- Estimate using complementary random numbers: $m_{TOC} = 43.00 \text{ x/h}$.



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- Assume that we have two electricity market models: a detailed model X = g(Y) and a simplified model $Z = \tilde{g}(Y)$. The results of the simplified model are referred to as control variates.
- Assume that we want to calculate the system indices for the detailed model (i.e., estimate E[g(Y)]) and that we already know the system indices for the simplified model, $E[\tilde{g}(Y)] = \mu_Z$.
- Sample the difference between the result variables and the control variate, i.e., X-Z!

 An estimate of the system indices for the detailed model is obtained by adding the system indices of the simplified model to the estimated difference between the two models, because

$$E[m_{(X-Z)} + \mu_Z] = E[X-Z] + \mu_Z = E[X] - E[Z] + \mu_Z = E[X].$$



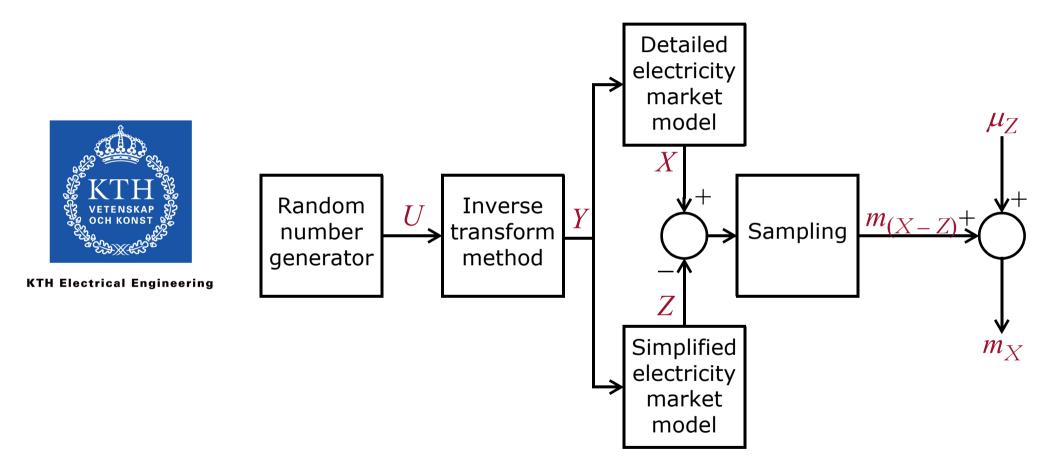
How good is the new estimate?



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$$Var[m_{(X-Z)} + \mu_{Z}] = \frac{1}{n}Var[X-Z] + 0 =$$
$$= \frac{1}{n}(Var[X] + Var[Z] - 2Cov[X, Z]).$$

• X and Z are results from models of the same system \Rightarrow X and Z should be positively correlated \Rightarrow Var[$m_{(X-Z)} + \mu_Z$] < Var[m_X], i.e., sampling using a control variate can be more efficient than using simple sampling!

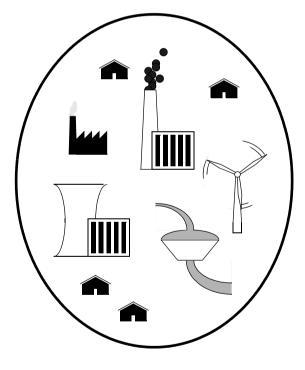




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Assume

- Perfect competition
- Perfect information
- Load is not price sensitive
- Neglect grid losses and limitations
- All scenario parameters can be treated as independent



Parameters



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 $D_{tot} =$ total load (scenario parameter—will be randomised during simulation),

 \overline{G}_g = available generation capacity in thermal unit g (scenario parameter—will be randomised during simulation),

 β_{Gg} = operation cost in thermal unit g,

 β_{Un} = penalty for unserved load.



Optimisation variables \tilde{G}_g = generation in thermal unit g, \tilde{U} = unserved load.

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Objective function

$$\sum_{g \in G} \beta_{Gg} \tilde{G}_g + \beta_U \tilde{U}.$$

Load balance constraint

$$\sum \tilde{G}_g = D_{tot} - \tilde{U}.$$

$$g \in G$$

Variable limits

$$0 \leq \tilde{G}_g \leq \overline{G}_{g'}$$
$$0 \leq \tilde{U} \leq D_{tot}.$$





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The control variates are calculated by solving the optimisation problem for the specific values of the scenario parameters and then calculate

$$\tilde{TOC} = \sum_{\substack{g \in G \\ ENS = \tilde{U},}} \beta_{Gg} \tilde{G}_{g},$$
$$\tilde{ENS} = \tilde{U},$$
$$\tilde{U}, \qquad \text{if } \tilde{ENS} = 0,$$
$$\tilde{U} = \begin{cases} 0 & \text{if } \tilde{ENS} = 0, \\ 1 & \text{if } \tilde{ENS} > 0. \end{cases}$$



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The expectation values of the control variates are calculated by running a probabilistic production cost simulation, i.e.,

$$\mu_{\tilde{TOC}} = ETOC_{PPC},$$
$$\mu_{\tilde{ENS}} = EENS_{PPC},$$
$$\mu_{\tilde{LOLO}} = LOLP_{PPC}.$$

Example 6.27



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In the simplified model we ignore the lower generation limit on the larger diesel generator set, i.e.,

$$\tilde{g}(Y) = \begin{cases} 0 & Y \le 150, \\ Y - 150 & 150 < Y \le 250, \\ 100 + 2(Y - 250) & 250 < Y \le 300, \\ 200 & 300 < Y. \end{cases}$$

Example 6.27 (cont.)



Scenario, i	1	2	3	4	5	6	7	8	9	10
<i>D</i> [kWh/h]	165	273	144	147	185	147	225	120	147	152
TOC [¤/h]	30	146	0	0	40	0	75	0	0	4
<i>TÕC</i> [¤/h]	15	146	0	0	35	0	75	0	0	2

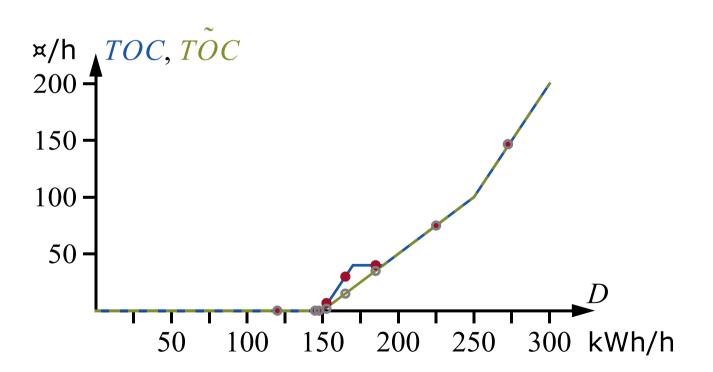
$$ETOC_{PPC} = 36.27.$$

$$m_{TOC} = \frac{1}{10} \sum_{i=1}^{10} (toc_i - t\tilde{o}c_i) + \mu_{T\tilde{OC}} = \dots =$$

= 2.20 + 36.27 = 38.47.

Example 6.27 (cont.)





Example 6.27 (cont.)

- True value: ETOC = 39.66 x/h.
- Estimate from simple sampling: $m_{TOC} = 29.50 \text{ x/h.}$
- Estimate using complementary random numbers: $m_{TOC} = 43.00 \text{ x/h}$.
- Estimate using a control variate: $m_{TOC} = 38.47 \text{ x/h}.$



then we must have



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- Assume that a population is divided in separate parts, strata, so that each unit belongs to exactly one stratum.
 If X_h is the set of units belonging to stratum h
 - $X_h \cap X_k = \emptyset, h \neq k$ (no overlapping strata)
 - $\bigcup_{h} X_{h} = X$ (the strata should include the entire population)



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• Each stratum is assigned a stratum weight corresponding to the size of the stratum, i.e.,

$$\omega_h = \frac{N_h}{N} = P(X \in X_h).$$

 N_h is the number of units in stratum h and N is the number of units in the population.



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- Assume that we have determined estimates of E[X_h] for each stratum.
 - Estimate using simple sampling:

$$m_{Xh} = \frac{1}{n_h} \sum_{i=1}^{n_h} x_{h,i}.$$

- Analytical value: $m_{Xh} = \mu_{Xh}$.



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 The weighted mean of the estimated stratum expectation values, m_{Xh}, is an estimate of E[X], because

$$E\begin{bmatrix} L \\ \sum_{h=1}^{L} \omega_h m_{Xh} \end{bmatrix} = \sum_{h=1}^{L} \omega_h \mu_{Xh} =$$
$$= \sum_{h=1}^{L} \frac{N_h}{N} \cdot \frac{1}{N_h} \sum_{i=1}^{N_h} \chi_i = \frac{1}{N} \sum_{i=1}^{N} \chi_i = E[X]$$



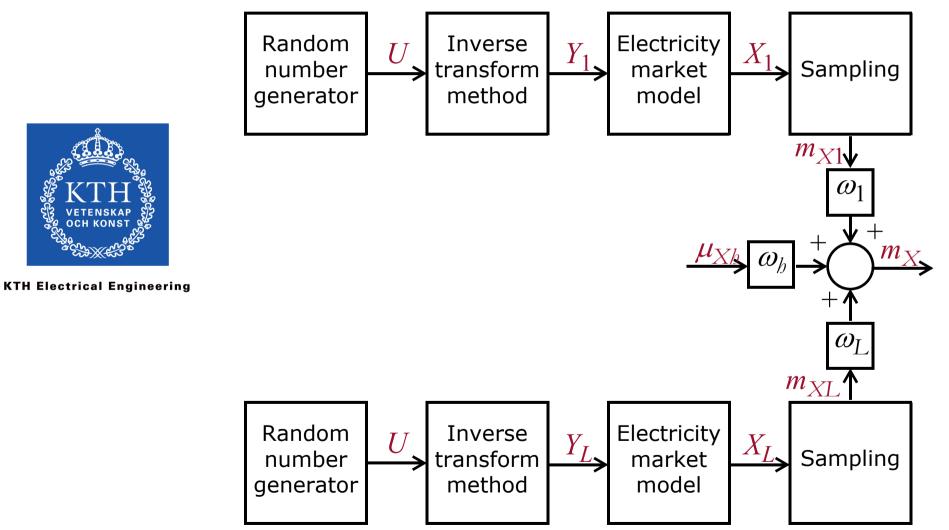
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 How good is the new estimate? It can be shown that

$$Var\left[\sum_{h=1}^{L}\omega_{h}m_{Xh}\right] = \sum_{h=1}^{L}\omega_{h}^{2}Var[m_{Xh}].$$

 Well chosen strata can result in a lesser variance than for simple sampling! However, the opposite is also possible!





STRATIFIED SAMPLING - Implementation



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- Strata cannot be defined based on the values of the result variables, as these values are unknown until we calculate x = g(y).
- A stratum must therefore be defined in terms of possible values for the scenario parameters.
- Hence, we must be able to generate random numbers which belong to a specific part of a probability distribution.

STRATIFIED SAMPLING

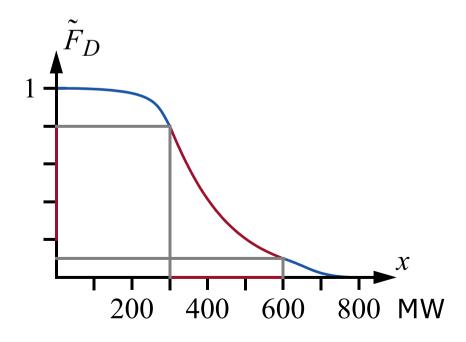
- Implementation

Generate $D \in (300, 600)$.

Example:







Example 6.28

Introduce the following strata:

- **1.** All scenarios such that $D \le 150$
- **2.** All scenarios such that $150 < D \le 250$
- **3.** All scenarios such that 250 < D



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Example 6.28 (cont.)

Calculate the stratum weights:

$$\begin{split} \omega_1 &= P(D \le 150) = \varPhi(-0.75) \approx 0.23, \\ \omega_2 &= P(150 < D \le 250) = \\ &= \varPhi(1.75) - \varPhi(-0.75) \approx 0.73, \\ \omega_3 &= P(250 < D) = 1 - \varPhi(1.75) \approx 0.04 \end{split}$$

Example 6.28 (cont.)



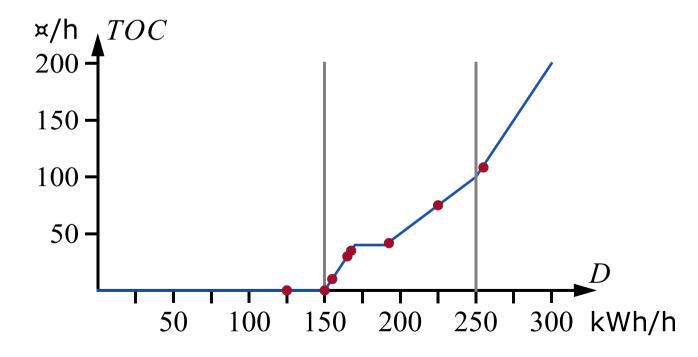
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Stratum, h]	l	2					3		
Scenario, i	1	2	1	2	3	4	5	6	1	2
D [kWh/h]	124	150	166	168	193	167	224	156	254	255
TOC [¤/h]	0	0	33	36	43	34	74	12	108	110
$m_{TOC} = \omega_1 \frac{1}{2} \sum_{i=1}^{2} x_{1,i} + \omega_2 \frac{1}{6} \sum_{i=1}^{6} x_{2,i} + \omega_3 \frac{1}{2} \sum_{i=1}^{2} x_{3,i}$ $= \dots = 32.72.$										

Example 6.28 (cont.)



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Example 6.28 (cont.)

- True value: ETOC = 39.66 x/h.
- Simple sampling: $m_{TOC} = 29.50 \text{ x/h}$.
- Complementary random numbers: $m_{TOC} = 43.00 \text{ x/h}.$
- Control variate: $m_{TOC} = 38.47 \text{ x/h}$.
- Stratified sampling: $m_{TOC} = 32.72 \text{ x/h}$.

Example 6.29



Stratum, h	1		3		
Scenario, i	1	1	2	3	1
D [kWh/h]	124	166	168	193	254
<i>TÕC</i> [¤/h]	0	16	18	43	108
TOC [¤/h]	0	32	36	43	108
Scenario, i	2	4	5	6	2
<i>D</i> * [kWh/h]	138	217	215	185	276
<i>TÕC</i> * [¤/h]	0	67	65	35	152
<i>TOC</i> * [¤/h]	0	67	65	40	152

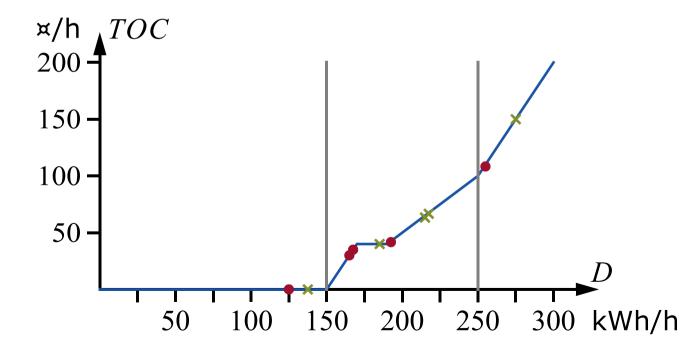


Example 6.29 (cont.)

$$m_{TOC} = \mu_{TOC} + \omega_1 \frac{1}{2} \sum_{i=1}^{2} (toc_{1,i} - t\tilde{o}c_{1,i}) + \omega_2 \frac{1}{6} \sum_{i=1}^{6} (toc_{2,i} - t\tilde{o}c_{2,i}) + \omega_3 \frac{1}{2} \sum_{i=1}^{2} (toc_{3,i} - t\tilde{o}c_{3,i}) + \dots = 43.44.$$

Example 6.29 (cont.)







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Example 6.29 (cont.)

- True value: ETOC = 39.66 x/h.
- Simple sampling: $m_{TOC} = 29.50 \text{ x/h}$.
- Complementary random numbers: $m_{TOC} = 43.00 \text{ x/h}.$
- Control variate: $m_{TOC} = 38.47 \text{ x/h}$.
- Stratified sampling: $m_{TOC} = 32.72 \text{ x/h}$.
- Combined method: $m_{TOC} = 43.44 \text{ x/h}$.

COMPARISON OF SIMULATION METHODS

Results from 1 000 simulations with different seeds for the random number generator.

Simulation method	Lowest ETOC estimate	Average ETOC estimate	Highest ETOC estimate
Simple sampling	6.33	39.78	81.65
Complementary random numbers	31.48	39.85	64.22
Control variate	36.27	40.03	46.08
Stratified sampling	19.44	39.78	59.74
Combination	36.95	40.03	43.30



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How should strata be defined in order to achieve the largest variance reduction? Consider that

$$Var[m_X] = \sum_{h=1} \omega_h^2 Var[m_{Xh}].$$

 \Rightarrow If all $Var[m_{Xh}]$ are small then $Var[m_X]$ will be small.

L



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- It is preferable if all scenarios belonging to a stratum give the same or very similar values for the result variables.
- To define efficient strata, we must be able to predict the results of the scenarios (without actually calculating the result variables).
- The strata tree is a tool to systematically categorise the scenarios.



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A strata tree is a tree structure with the following properties:

- The root of the tree contains no information.
- All other nodes specify a number of possible outcomes for one or more scenario parameters.
- Each node has a node weight, which is given by the probability to get the specified outcome for the scenario parameters.



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- The node weight of the root is 1.
- The scenario parameters along a branch of the tree should be independent of each other.
- Each branch will include a part of the total population, i.e., each branch corresponds to a stratum. The stratum weight is obtained by multiplying the node weights along the branch.

Strata with similar properties can be merged, i.e., one stratum may consist of several branches.



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The strata tree should include all possible scenarios. This requirement is guaranteed to be fulfilled if

- all children of a certain node specify outcomes for the same scenario parameters,
- the sum of the node weights of the children is equal to 1.



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The possible values of TOC and LOLO can be predicted if we know the total available generation capacity, \overline{G} (thermal) and \overline{W} (non-dispatchable), as well as the total load, D.

- One node for each possible state of the available generation capacity should be in an upper level of the strata tree.
 Requires discrete probability distributions!
- One node for each interesting load interval in a lower level of the strata tree.



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- In a multi-area model, we need to consider that there are some load intervals for which it is more difficult to predict *TOC* and *LOLO*.
- Assume that we know the maximal losses, \overline{L} , and the maximal unused generation capacity due to transmission congestion, \overline{U}_W (renewable) and \overline{U}_{WG} (total).



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• $D \le \overline{W} - \overline{U}_W \Longrightarrow TOC = 0, LOLO = 0$

The load can be covered using only nondispatchable units.

•
$$\overline{W} - \overline{U}_W < D \le \overline{W} - \overline{L} \implies TOC \ge 0, LOLO = 0$$

It is possible that the load can be covered using only non-dispatchable units, but other units might have to be dispatched due to transmission congestion.



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• $\overline{W} - \overline{L} < D \le \overline{W} \Longrightarrow TOC \ge 0, LOLO = 0$

It is possible that the load can be covered using only non-dispatchable units, but other units might have to be dispatched due to transmission losses.

• $\overline{W} < D \le \overline{W} + \overline{G} - \overline{U}_{WG} \Longrightarrow TOC > 0, LOLO = 0$

The load cannot be covered using only nondispatchable units, but the generation capacity is sufficient thanks to the other units.



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• $\overline{W} + \overline{G} - \overline{U}_{WG} < D \le \overline{W} + \overline{G} - \overline{L} \implies TOC > 0$, LOLO = 0 or 1

It is possible that the generation capacity is sufficient, but load shedding might become necessary due to transmission congestion.

• $\overline{W} + \overline{G} - \overline{L} < D \le \overline{W} + \overline{G} \Longrightarrow TOC > 0$, LOLO = 0 or 1

It is possible that the generation capacity is sufficient, but load shedding might become necessary due to transmission losses.



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• $\overline{W} + \overline{G} < D \implies TOC > 0, LOLO = 1$ Load shedding is unavoidable.

Notice that other combinations of *TOC* and *LOLO* are also possible, for example if $\overline{G} = 0$.



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Example 6.30 — System data

Generation

- Wind power, available capacity 0 kW (50%) or 150 kW (50%), negligible operation cost.
- Diesel generator set, 250 kW, 80% availability, operation cost 10 ×/kWh.

Load

- Evenings: Mji *N*(175,48), Kijiji *N*(75,20).
- Other time: Mji *N*(120,24), Kijiji *N*(30,7).



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Example 6.30 — System data

Transmission

• The maximal losses on the line between Mji and Kijiji are 3 kW.

Example 6.30 — Problem

Suggest an appropriate strata tree and calculate the stratum weights!



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Example 6.30 — Solution

Suitable strata tree

- Level 0: Root
- Level 1: Time of day
- Level 2: Available generation capacity
- Level 3: Load

	Time l	Fime level		Generation level		Load level		um ht	()	0	Ð
KTH KTH VETENSKAP OCH KONST	Period	Node weight	\overline{W}	\overline{G}	Node weight	D	Node weight	Stratı weig	TOC	TOT	Type
KTH Electrical Engineering			0	0	0.1	≥ 0	1	0.075	0	1	*
						≤ 147	0.452	0.034	0	0	Ι
	Day/		150	0	0.1	147–150	0.048	0.004	0	0/1	*
	Night	0.75				> 150	0.5	0.038	0	1	*

	Time l	evel	Ge	nera leve		Load le	vel	ht L	۲)	0	ل۵
KTH VETENSKAP OCH KONST OF	Period	Node weight	\overline{W}	\overline{G}	Node weight	D	Node weight	Stratu weig	TOC	TOL	Type
KTH Electrical Engineering						≤ 247	0.452	0.034	>0	0	IV
	Day/ Night	0.75	0	250	0.4	247–250	0.048	0.004	>0	0/1	VI
						> 250	≈ 0	≈ 0	>0	1	VII

KTH Elastical Engineering	Time level		Generation level			Load level		um Jht	C	0	e
	Period	Node weight	\overline{W}	\overline{G}	Node weight	D	Node weight	Stratum weight	TOC	TOT	Type
KTH Electrical Engineering	Day/	0.75				≤ 147	0.452	0.136	0	0	Ι
	Night		150	0 250	50 0.4	147–150	0.048	0.014	≥ 0	0	III
						150–397	0.5	0.15	>0	0	IV
						397–400	≈ 0	≈ 0	>0	0/1	VI
						>400	≈ 0	≈ 0	>0	1	VII

	Time l	evel	Generation level		Load level		um ht	()	0	Ð	
KTH VETENSKAP COCH KONST COCH KONST COCH	Period	Node weight	\overline{W}	\overline{G}	Node weight	D	Node weight	Stratu weig	TOC	TOT	Type
KTH Electrical Engineering			0	0	0.1	≥ 0	1	0.025	0	1	*
						≤ 147	0.024	0.001	0	0	Ι
	Even-		150	0	0.1	147–150	0.003	≈ 0	0	0/1	*
	ing	0.25				> 150	0.973	0.243	0	1	*

	Time level		Generation level		Load level		um ht	5	O`	(D	
KTH VETENSKAP OCH KONST WE	Period	Node weight	W	\overline{G}	Node weight	D	Node weight	Stratu weig	TOC	TOT	Type
KTH Electrical Engineering	-					≤ 247	0.452	0.034	>0	0	IV
	Even- ing	0.25	0	250	0.4	247–250	0.048	0.004	>0	0/1	VI
						> 250	0.5	0.05	>0	1	VII

KTH VETENSKAP OCH KONST	Time level		Generation level			Load level		um Jht	C	0	в
	Period	Node weight	\overline{W}	\overline{G}	Node weight	D	Node weight	Stratum weight	OOL	TOI	Type
KTH Electrical Engineering	Even-	0.25				≤ 147	0.024	0.002	0	0	Ι
	ing		150 25	250	50 0.4	147–150	0.003	≈ 0	≥ 0	0	III
						150–397	0.970	0.097	>0	0	IV
						397–400	≈ 0	≈ 0	>0	0/1	VI
						>400	0.002	≈ 0	>0	1	VII

HOME ASSIGNMENTS PART IV - Hints



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Problem 24

Define strata using a strata tree.

- Calculate the maximal losses.
- Identify interesting load intervals.
- Calculate node and stratum weights.

Recommended exercise: 6.16a

HOME ASSIGNMENTS PART IV - Hints



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Problem 25

Perform a small Monte Carlo simulation to estimate *ETOC* and *LOLP*.

- Randomise a scenario (norminterval will generate both an original and complementary random number from the normal distribution of your choice).
- Analyse the scenario using the multi-area model (problem 22) and a PPC model.
- Calculate estimates according to (6.46).

Recommended exercises: 6.14, 6.15, 6.16b

HOME ASSIGNMENTS PART IV - Hints



Problem 26

Compare probabilistic production cost simulation and Monte Carlo simulation.

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Theorem (Neyman allocation): $Var[m_X]$ for *n* samples is minimised if the sample are distributed between the strata according to

$$n_{h} = \frac{\omega_{h}\sigma_{Xh}}{\sum_{k=1}^{L}\omega_{k}\sigma_{Xk}}n,$$

where $\sigma_{Xh} = \sqrt{Var[X_{h}]}.$



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The Neyman allocation corresponds to a flat optimum, i.e., it is possible that we get a $Var[m_X]$ which is close to the optimal value, even if we do not use the best sample allocation.



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Problem 1:

 $Var[X_h]$ are unknown.

• Estimate σ_{Xh} by

$$s_{Xh} = \sqrt{\frac{1}{n_h} \sum_{i=1}^{n_h} (x_{h,i} - m_{Xh})^2}.$$

• Notice that σ_{Xh} cannot be estimated unless $n_h > 0!$



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STRATIFIED SAMPLING - Sample allocation

Procedure

- Run a pilot study where the number of scenarios per stratum is determined in advance.
- Calculate an appropriate allocation.
- Run a **batch** of scenarios.
- Test convergence criteria.
- If more scenarios are needed, update the sample allocation, run the next batch, etc.



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Problem 2:

We are simultaneously sampling several result variables and a sample allocation that is optimal for one result variable might not be optimal for another.

- Calculate the optimal sample allocation with respect to each result variable.
- Use a compromise allocation (for example the mean of the allocations).



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Stratum	Optimal all TOC	ocation for LOLO	Compromise allocation
1	0	0	0
2	1 028	0	514
3	388	0	194
4	4	1 420	712
5	0	0	0
Σ	1 420	1 420	1 420

Example:



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Problem 3:

It might not be possible to achieve the target sample allocation.

• Try to get as close as possible!

(Cf. algorithm described in the compendium, page 144.)



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Stratum	Allocation										
Stratum	Compromise	So far	Next batch	Total							
1	0	94	0	94							
2	514	530	0	530							
3	194	68	77	145							
4	712	512	123	635							
5	0	16	0	16							
Σ	1 420	1 220	200	1 420							

Example: